

STRESS PATHS AND COLLAPSING SOILS

A Thesis presented to the

DEPARTMENT OF CIVIL ENGINEERING

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In partial* fulfilment of the requirements for
the degree of Master of Science in Engineering.

by

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* This candidate has successfully completed five postgraduate courses (24 credit points) in partial fulfilment of the requirements for the M.Sc.Eng. degree, and therefore this thesis represents approximately one half of the value of an M.Sc. thesis submitted in complete fulfilment of the requirements for the degree. (For details of courses taken, see page C1 in last Appendix.)

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A C K N O W L E D G E M E N T S

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D E C L A R A T I O N

The writer hereby declares that except where otherwise stated, the content of this thesis is substantially his own work and has not been submitted to any other university.

Signed by candidate

L.A. ERRERA

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CHAPTER 1

BRIEF INTRODUCTION TO THESIS

The design of footings and the accurate prediction of settlements is inherently difficult as the parameters involved vary considerably.

The initial stage of the design consists of three steps. The first step is to define all the parameters required. The second step is to give quantitative values to these parameters by performing tests and calculations. The third and last step should be the investigation of changes in external or local conditions on these parameters. The importance of this step is brought to the fore when considering collapsing soils and heaving clays.

The next stage of the design would be to consider the stress changes at either an average point or a grid of points below the footing within the soil mass. To do this the engineer makes use of conventional methods of analysis. Factors such as horizontal strata and variations of properties with depth must be considered.

Once the engineer has defined all the stress changes he must then decide which method of settlement prediction would be appropriate. The deformations of the soil mass do not only depend on the change in stress, but also on the previous stress-strain history of the soil and the actual variation of stresses with time during the settlement process. (e.g. see the error involved when considering the Skempton-Bjerrum method. Refer to Chapter 7). As the stress path accurately reflects all the stress changes the stress path method is an excellent tool for describing the stress and strain variations. There are numerous methods all of which have their merits and disadvantages. These will be discussed, and the influence of the stress path on settlement prediction is also analysed. Although a stress path method of settlement prediction might not always be essential, an analysis of a typical stress path for the particular problem would appear to be an excellent initial approach to deciding on the validity of any method of settlement prediction.

The final stage is the accumulation of data and the prediction of the settlement value using one or more of the following methods:

- 1) Find the field penetration using the Dutch Cone Penetrometer (or any accepted penetrometer). This value is then used in conjunction with predetermined design curves to find the settlement.
- 2) Make use of settlement formulae which are directly derived from elastic theory. These do not take into consideration any of the variations of properties within the soil mass (see Chapter 7).
- 3) Define an average point or a number of grid points below the foundation (see Chapter 5). For each point evaluate a stress variation and hence calculate a corresponding strain value. The settlement of the footing is then calculated using the strain values.

The above estimated settlement values are also to be regarded with caution, as foundation size and rigidity do influence predicted values. There are however methods to diminish these inaccuracies (see Chapters 3 and 7).

The engineer should be able to predict the stress variations with reasonable accuracy if he has a knowledge of the influences of all these factors on the idealised elastic case (e.g. foundation size, rigidity, existing horizontal stresses etc). It therefore becomes apparent that the predicted settlement is not a 'wild estimate', but a carefully analysed value which can be forecast with confidence, providing the proper tests have been made.

C H A P T E R 2

COLLAPSING SOILS

2.1 Introduction to the phenomenon of collapsing soils

The problem of collapsing soils is a world wide phenomena. On these soils excessive settlements can be experienced by footings carrying only a fraction of the safe bearing capacity according to current theories.

After investigation of case histories (Knight, Ref. 28 and Kantey, Ref. 29) it was found that if a particular type of soil was subjected to a load greater than the past overburden pressure and the collapsing soil was simultaneously wetted, then excessive settlement would occur. This sudden excessive settlement has been defined as 'settlement due to collapse' (Knight, Ref. 28). Collapse is a rapid decrease in void ratio and refers to the altering of the packing of the grains.

The amount of water necessary to produce this collapse phenomena is related to the clay content as well as the type of clay present. In the case of a collapsing decomposed granitic residual soil this statement is justified, providing the proportion of clay is expressed as a percentage by mass of the material below 1 mm. If the moisture content is too high, the soil settles fully under the loading, and no further collapse occurs due to further wetting while the soil carries this load. Critical moisture contents above which no more collapse settlement occurs have been observed by the writer. These are shown in Table 2.1 for three soils.

2.2 Collapsing soils in South Africa

Collapsing soils fall into two main categories i.e. decomposed in situ residual soils or transported decomposed silty sands. The transported material is silty sand because the prime mode of transportation is wind.

Clay content & soil description	Field void ratio	Moisture content after which no further collapse settlement occurs	Degree of saturation after which no further collapse settlement occurs	Source of sample
	e_o	(Constant load 110 kN/m ²) i.e. 1 ton/ft ²	(Constant load 110 kN/m ²) i.e. 1 ton/ft ²	
19% Clay Berea Road Collapsing sand	0,712	16,5 %	69,4 %	Via Prof Sparks
10% Clay Sishen Collapsing sand	0,802	5,2 %	20,7 %	Via Mr Stern
5% Clay Feathers Decomposed Granite	0,915	13,7 %	52,0 %	Via Mr Butters

TABLE 2.1 Comparison of Collapsing Properties of Undisturbed Samples Tested

2.2.1 Physical properities of collapsing aeolian sands

The deposited sands rest unconformably on rock systems (Knight, Ref. 28). They usually have a grey or orange colour. The colouring depends on whether the oxide present is one of Iron (orange) or Aluminium (grey). The darkness of the colour depends on the percentage of the oxide present in the soil.

All the sands display a uniformity of size. This is a direct result of the aeolian mode of transportation (Knight, Ref. 28, Allen, Ref. 30 and Way, Ref. 31). Way and Allen define the sizes of saltating (i.e. bouncing) grains in wind as varying between 0,5 and 0,15 mm. Results of sieve analyses substantiate this (see Figure 2.1).

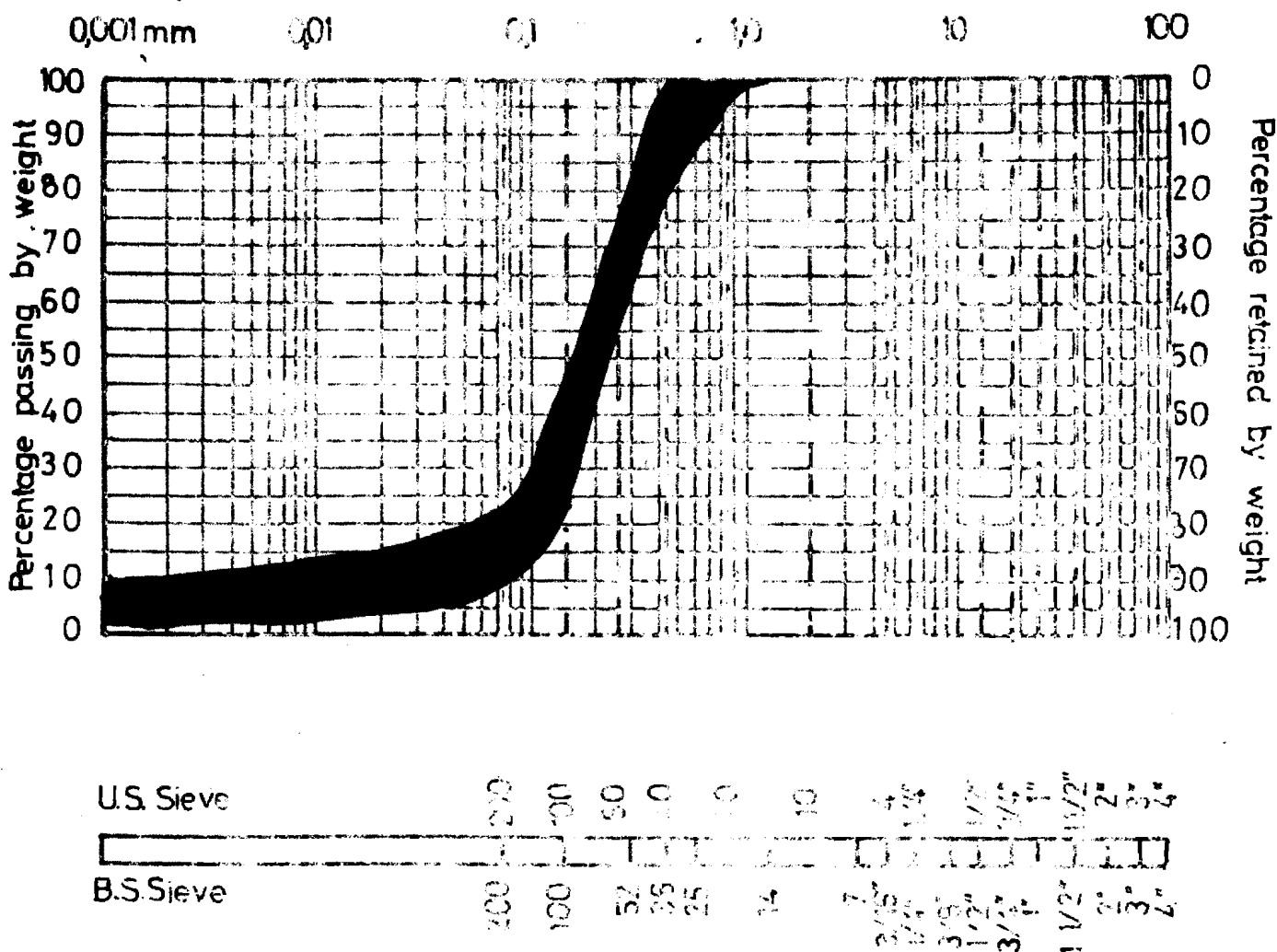


FIGURE 2.1 Sieve Analysis of Collapsing Soils
Investigated by the Writer

Particles which are larger and finer than the usual wind-blown sizes are also present in the windblown sands. These larger sizes can arise from a process defined as creep (Way, Ref. 31, and Allen, Ref. 30). The finer sizes may be deposited after travelling in suspension, or from in situ weathering after deposition of larger saltating grains. In collapsing sands the latter can be the cause of the finer portion of the sand (Knight, Ref. 28).

The envelope of eight collapsing aeolian sands is shown in Figure 2.2. Jennings (Ref. 32) and Knight (Ref. 28) emphasize that all collapsing sands have a characteristic gap grading. The writer however feels that the characteristic grading curve of collapsing sands should rather be described as uniformly graded with relatively low clay content. For this thesis clay content is defined as the proportion by mass of the sample below a grain size diameter of 0,074 mm.

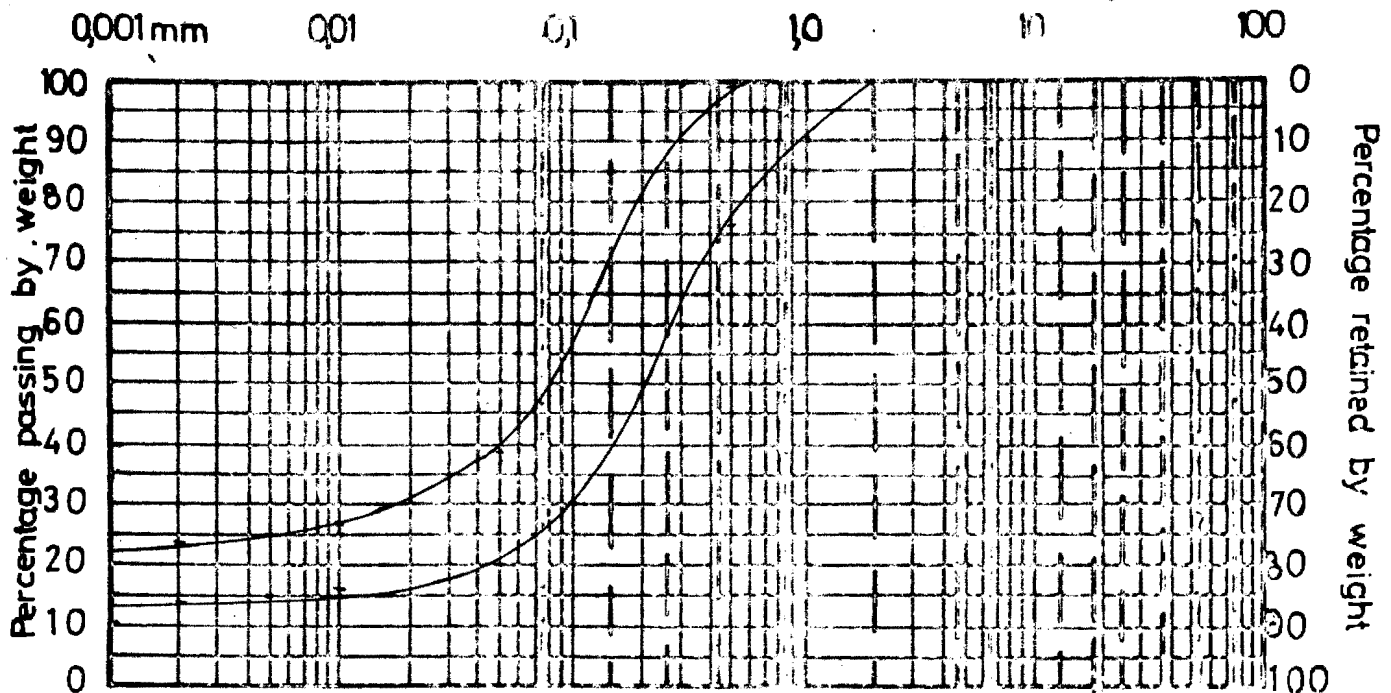


FIGURE 2.2 *Envelope of Eight Collapsing Sands*
(Knight, Ref. 28 and Jennings, Ref. 32)

2.2.2 Sequence of events resulting in the formation of collapsing aeolian sands

Initially in areas of arid climatic conditions rocks are broken down. The breaking down process is caused by the action of temperature, wind and water. When the process has continued long enough for the material to be transported, the sands will either be transported by wind for long distances, or they may be deposited locally. Local deposition is a result of local dustbowl conditions. In the Transvaal these local dustbowl conditions are known to exist (Knight, Ref. 28).

In the areas where the sands are deposited the climatic conditions may be different. The map in Figure 2.3 describes the recent deposition of windblown sands (Knight, Ref. 28 and Kantey, Ref. 29) and areas where precipitation of water exceeds evapo transpiration. (Knight, Ref. 28, Kantey, Ref. 29 and Van der Merwe, Ref. 33).

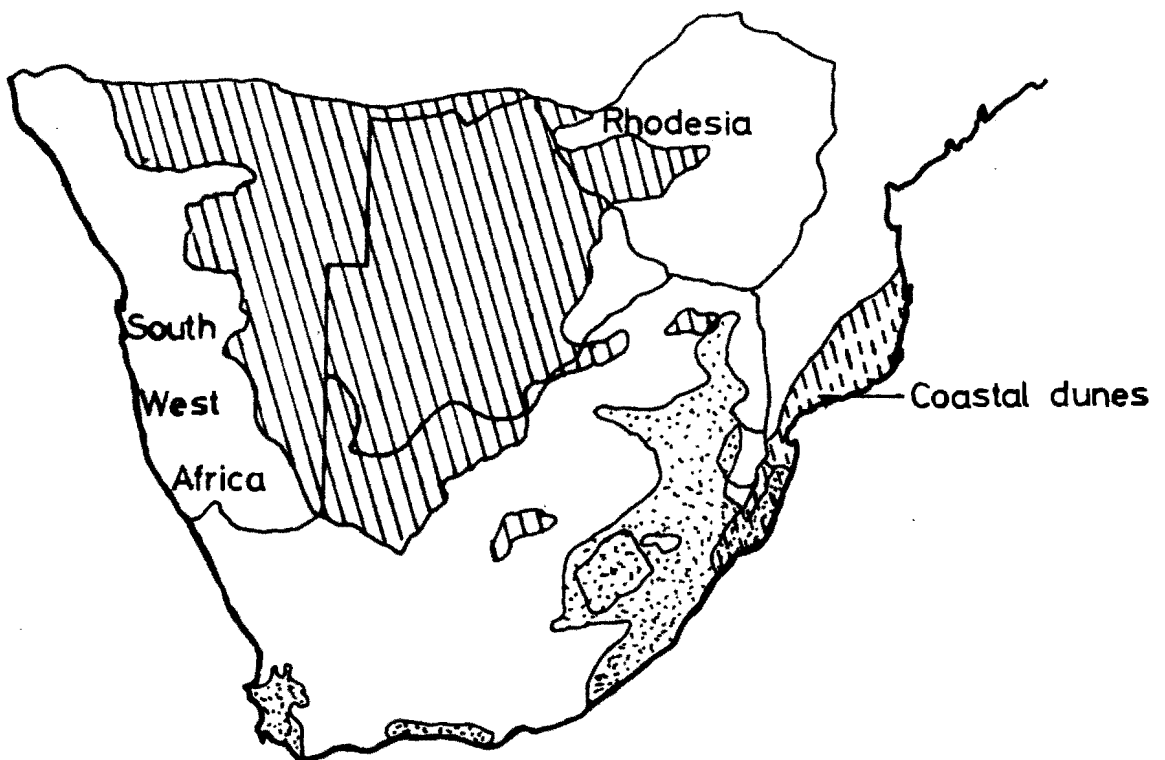


FIGURE 2.3 *Areas of Recent Windblown Sheets and of Annual Water Surplus*

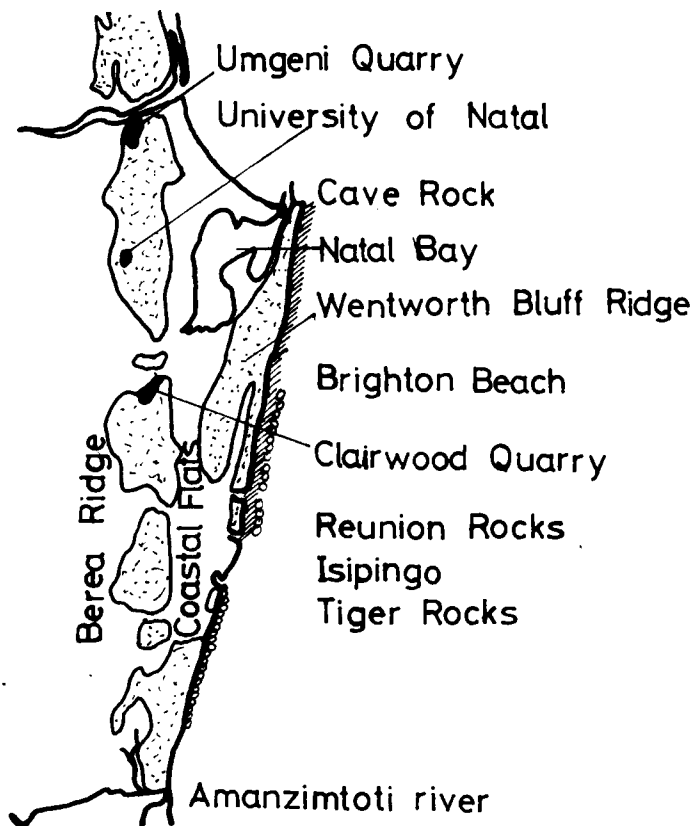


FIGURE 2.4 *The Distribution of the Bluff Beds, the Berea Red Sandstone (Weathered Bluff Beds) and raised beach deposits in the Durban area.*

Kaolinite bridges are formed between the hard quartz grains. The iron oxide present covers the quartz grains and assists in the cementing together of the grains. The end result is a weakly cemented loosely packed soil mass. See Figure 2.5.

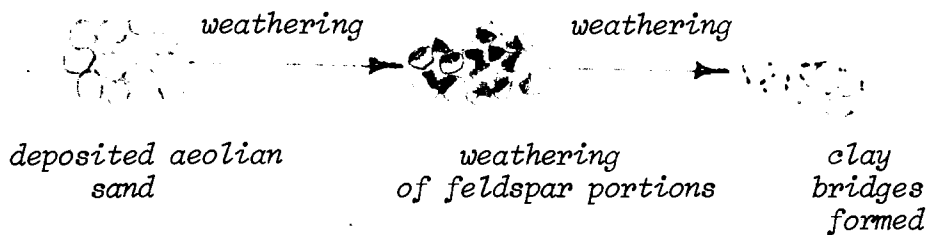


FIGURE 2.5 *Schematic Representation of Insitu Weathering*

2.2.3 Composition and source of collapsing sands

The parent rock is usually granite. The sands are predominantly quartz. Small percentages of heavy minerals (e.g. ilmenite and tourmaline) are present. Knight (Ref. 28) shows that it is this small percentage of heavy minerals which can be used to define the origin of the transported sands. Variable quantities of feldspar are present.

The hard grains are chiefly quartz and chert. Microscopic examination of windblown quartz grains shows them to have a frosted texture. (Knight, Ref. 28).

The clay content of the sands vary. Knight (Ref. 28) quotes an average value of 20 per cent for the clay content of collapsing sands. The sample from Sishen, tested by the writer, has a much lower clay content. The clay fractions of most collapsing sands consists mainly of kaolinite with minor amount of illite. The clay is formed as a by-product of feldspar weathering.

Adhering to the grains is a fine layer of iron oxide. The colours of soils tested by the writer varied from a brick red (Berea Road, Durban) through a dull brown (Sishen) to a orange (Yellowood Parkway, Durban). The iron oxide is a weathering product of the mafic minerals present in the wind deposited soil mass.

2.2.4 Conditions surrounding collapsing sands

Aeolian or windblown sands were deposited mainly during the Pleistocene times. Pleistocene times are associated with arid climatic conditions. Areas where collapsing soils have been found have rainfalls varying from 41 cm to 82 cm per annum.

Underlying all transported collapsing sands a pebble-marker layer has been found. The weathering of the rock formations underlying the pebble-marker indicates the weathering that has occurred in the collapsing sand (Knight, Ref. 28).

The rapidity of in situ weathering is dependent upon climatic conditions and internal soil drainage. In humid climates and under good internal soil drainage conditions the weathering process is accelerated.

Figure 2.6 illustrates the distribution of collapsing sands in South Africa (Knight, Ref. 28 and Van der Merwe, Ref. 33). Comparison of Figures 2.3 and 2.6 shows a definite correlation between areas of recent transported sands, rainfall surplus and known sites of collapsing sands. Subsequent areas where collapsing sands were found are Sishen and Durban. The Sishen area however does not lie in a zone of rainfall surplus.

2.2.5 The structure of collapsing sands

The structure of collapsing sands consists of the stable quartz grains weakly cemented by clay bridges. These clay bridges display strength parameters which are highly dependent upon moisture content. In cases when the degree of saturation is low, the collapsing soil seems to have much higher strength parameters than a pure sand. The addition of water appears to lubricate the coated quartz particles. This reduces both the angle of internal friction and the cohesive strength of the collapsing sand. This reduction in the strength parameters must be related to the percentage of clay present in the collapsing sand. This would seem to be the reason for the main difference between the Southern African sands and collapsing sands in the other areas throughout the world. The difference is that collapsing sands in America (Knight, Ref. 28) will not support their own weight when inundated whereas the Southern African sands do not collapse under normal overburden pressures due to self weight.

The sands have relatively high void ratios which may differ in any one location. Differences in void ratio in any one location arise from occurrences such as failure near the toe of a dune (Knight, Ref. 28). Within the voids are uncompacted fine portions of the soil mass. When collapse of the soil mass takes place these portions are compacted.

Figure 2.7(a) shows the structure of the undisturbed deposited sand while Figure 2.7(c) shows the collapsed structure (Knight, Ref. 28, Knight and Jennings, Ref. 34, and Jennings, Ref. 32). Figure 2.8 shows a typical $e-\bar{p}$ collapse curve for a collapsing sand. The method and description of the test as used at the University of Cape Town is described in Chapter 9.

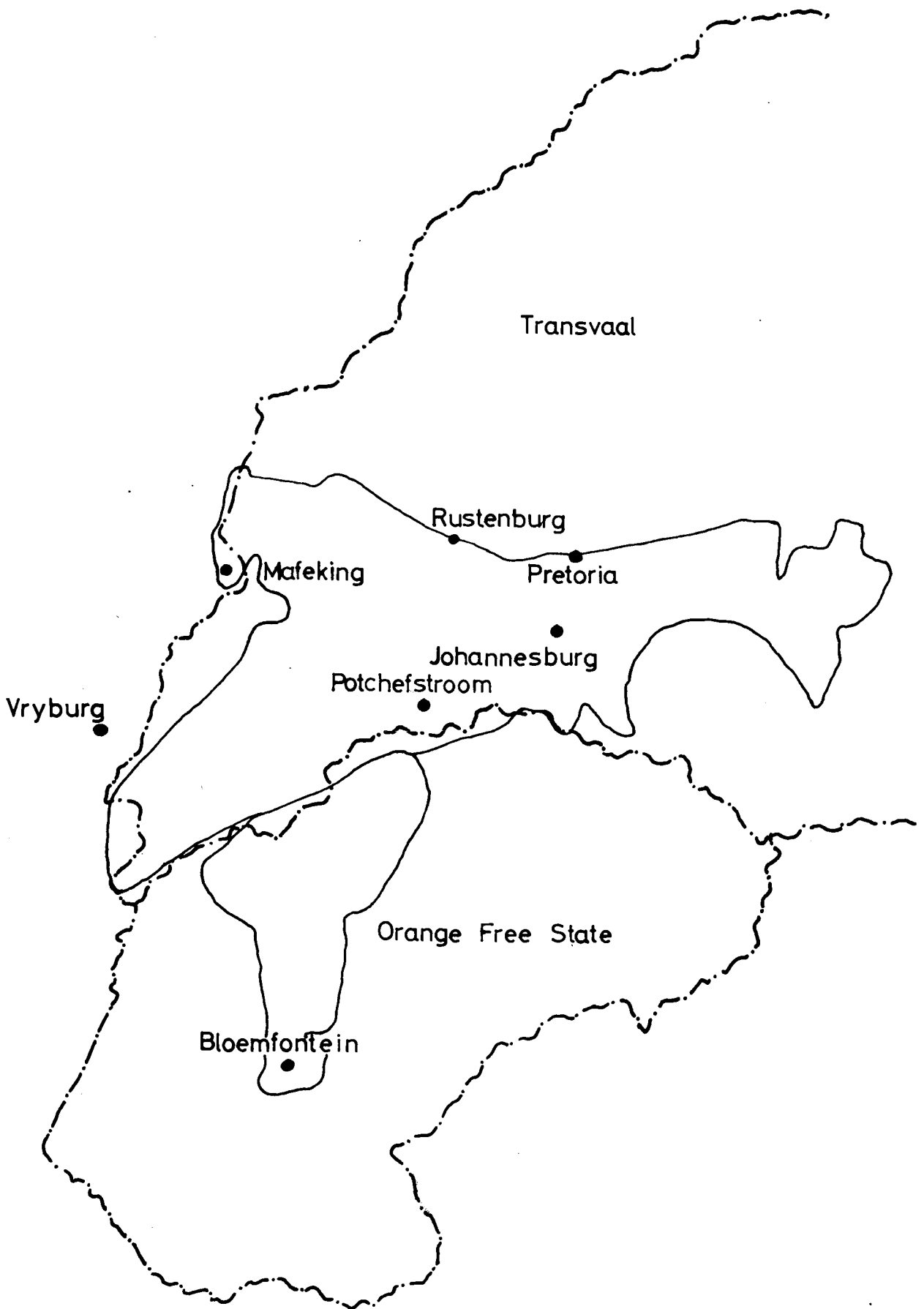


FIGURE 2.6 *Distribution of Commonly known Areas of Collapsing Sands in South Africa*

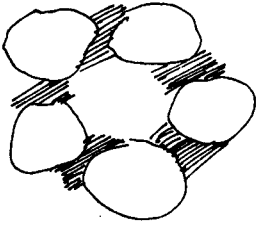


FIGURE 2.7(a) ORIGINAL FIELD STRESS STATE

Low moisture content

High void ratio

Subjected to self weight pressures only

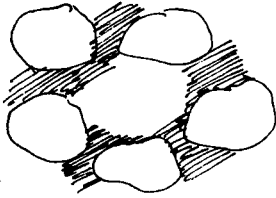


FIGURE 2.7(b) LOADED STATE (without wetting)

Low moisture content

Relatively high void ratio

*Subjected to self weight overburden pressure
plus design loads*

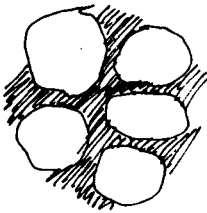


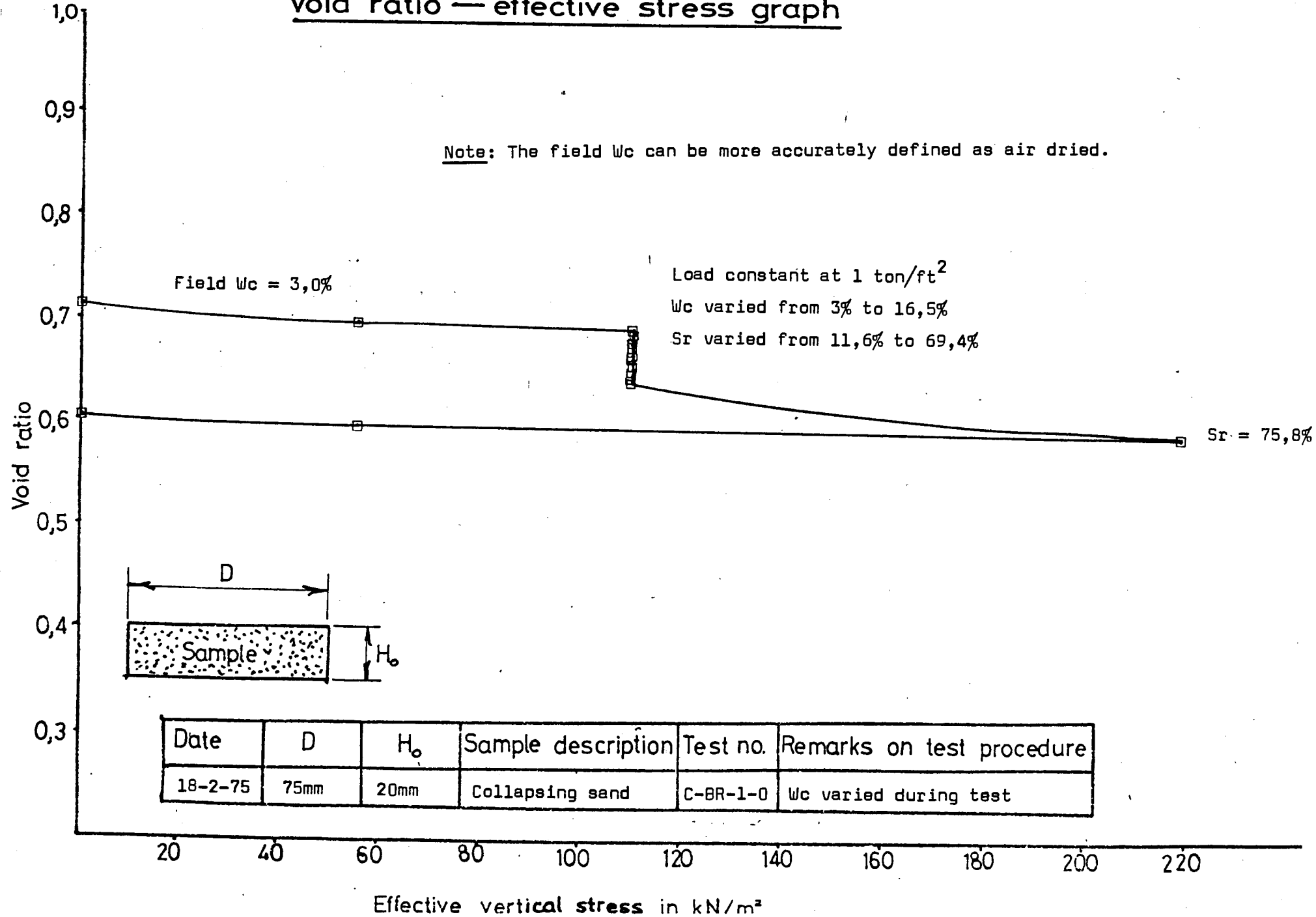
FIGURE 2.7(c) LOADED STATE (after further wetting)

Relatively high moisture content

Low void ratio

Subjected to overburden pressure plus design loads

FIGURE 2.8 e - p Collapse Curve for Berea Road Sample



2.2.6 Physical properties of collapsible residual granitic soils

This soil type is formed when the feldspars and the mafic minerals of the parent rock are weathered in situ. The resulting soil consists of a large percentage of quartz particles surrounded by finer material.

The finer material consists of fine sand particles with a thin layer of either iron oxide or aluminium oxide adhering to them. As with the collapsing sands, clay bridges also link the larger sized particles in the collapsing residual granitic soils.

The results of a grading analysis done on this soil type is shown in Figure 2.9(a). In Figure 2.9(b) a comparison of grading curves for the collapsing sands and for the granitic soil is shown. The curve for the collapsing sands is an average curve derived directly from Knight (Ref. 28). Only the finer section of the grading curve for the granitic soil is used. This section of the curve is adjusted to represent a complete sample.

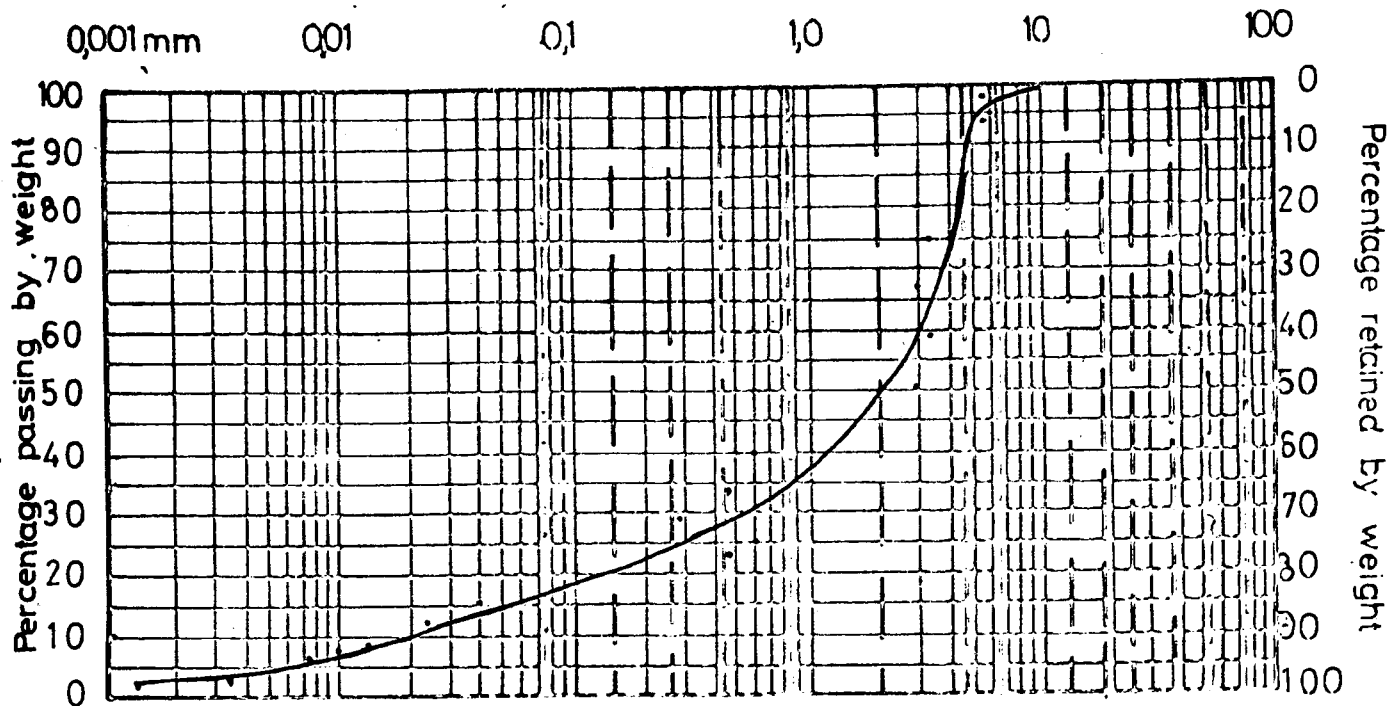


FIGURE 2.9(a) Grading Curve for Feathers Sample

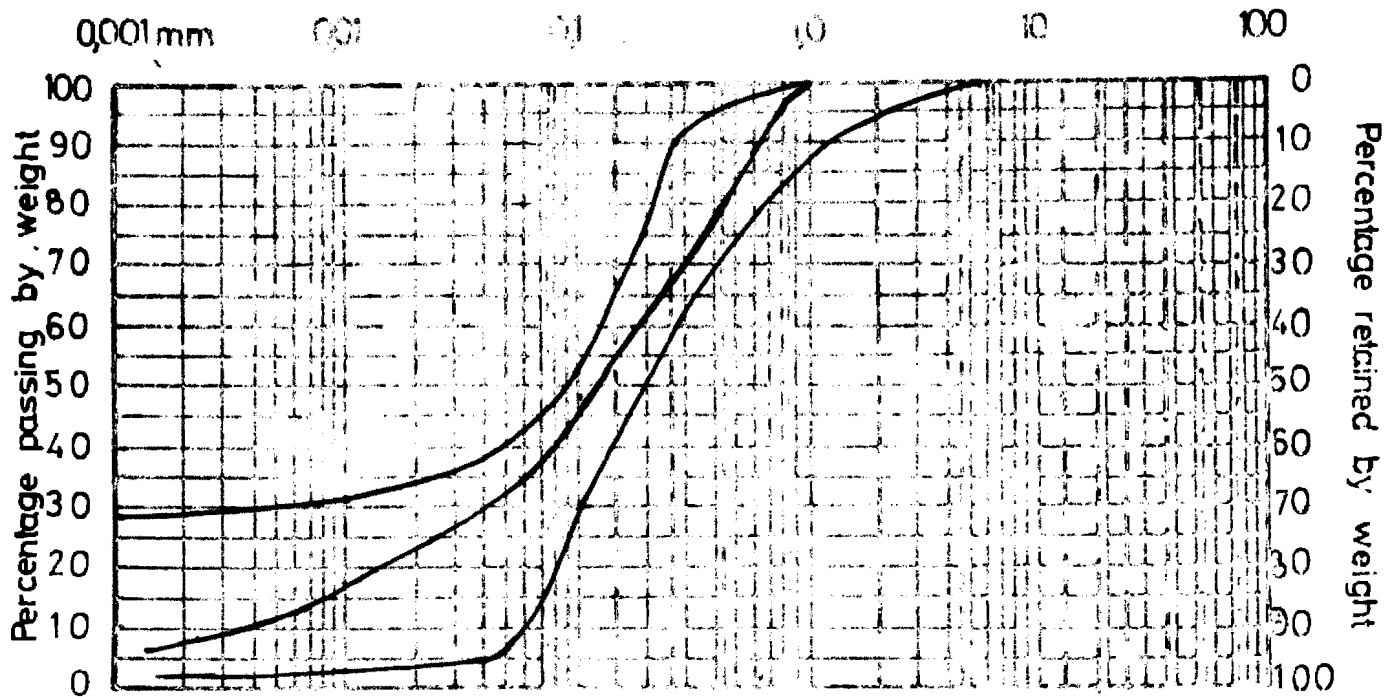
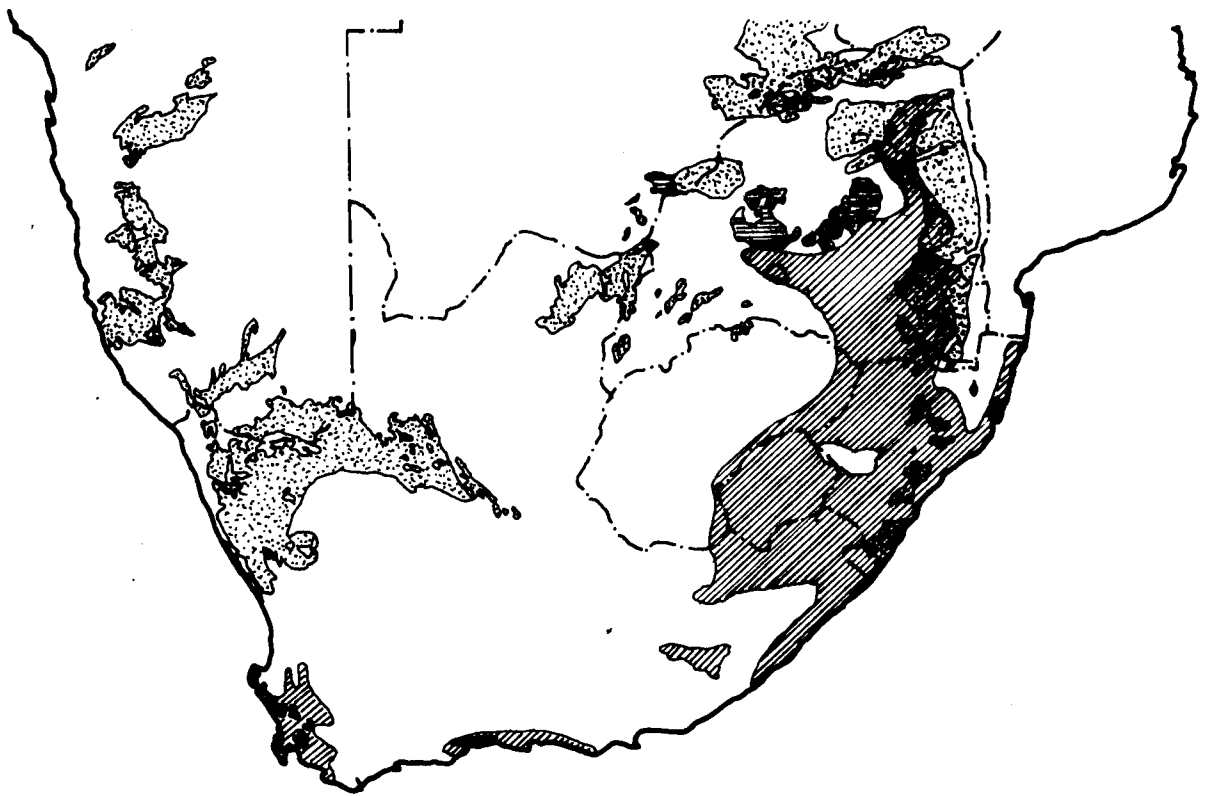


FIGURE 2.9(b) Comparison of Grading Curves

According to other workers (e.g. Knight, Kantey, Holmes) the two main climatic factors associated with the collapse structure of the soil are that precipitation must exceed evapo-transpiration and the existence of arid conditions see Figure 2.10. Seasonal climatic variations and the presence of slopes or large angles of dip accelerate the process of the formation of the collapse structure.

The colouring of granitic residual soils is either reddish brown or grey. The cause and variations in colouring is the same as for the collapsing sands.



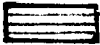



-  *Distribution of Red Bushveld Granite*
-  *Distribution of younger Cape Granite*
-  *Distribution of Old Granite*
-  *Areas of annual water surplus*

FIGURE 2.10 *Granite Areas and Areas of Net Excess Rainfall in S.A.*

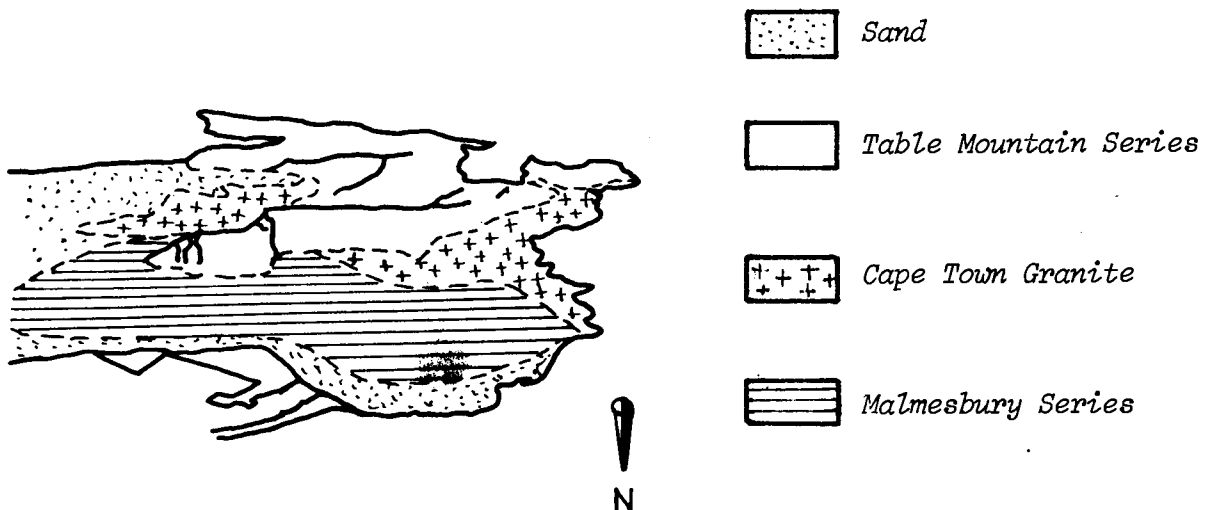


FIGURE 2.11 *Detailed Geographical View of the Cape Peninsula*

2.2.7 Sequence of events resulting in the production of collapsible granitic soils in South Africa

The parent rock consists mainly of quartz (25% to 40%), feldspar (orthoclase, plagioclase up to 50%) and mica (light or dark).

The weathering process is divided into two main categories, mechanical weathering and chemical weathering. The weathering process usually leaves a loosely packed skeleton of unweathered products. The unweathered products are chiefly quartz and muscovite (Holmes, Ref. 27).

Mechanical weathering is the breaking down of the parent rock into smaller particles. Agents of this process are rain, frost and wind. Sudden temperature changes will cause flaking of the parent rock.

Chemical weathering is the breaking down of minerals into new components by the action of chemical agents. Representative of these chemical agents are acids in the air, in rain water and in river water.

A. Horizon Top Soil	high void ratio	Decreasing organic content
	high porosity	
	quantities of inorganic particles and vegetable humus	
	Mixture of soil and rock fragments	
B. Horizon	Weathered Rock	
Sub Soil	Unweathered Rock	

FIGURE 2.12 *Typical Cross-section Through weathered layers down to Parent Rock (Holmes, Ref. 27)*

The weathered material may either remain in position as residual deposits or be removed by the action of wind and/or water.

The voids in the B Horizon are filled with air together with water from rainfall. Some of this water percolates down into the rock. The jointing of the granite increases the depth of penetration. This groundwater can become acidic in passing through the soil and can under certain conditions reduce the granite to a relatively porous weak soil mass.

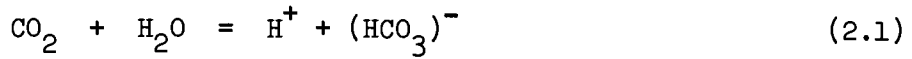
Denudation also accelerates weathering. A reduction in loading will cause a vertical expansion within the rock mass. This gives rise to the formation of sheets of rock due to the opening of joints parallel to the ground surface. This occurrence is a characteristic of granites. The frequency of the existence of the sheets diminishes with depth into the granite.

Once the weathering process has been completed the products that are in colloidal form are transported to other areas. The transportation process can either be due to the flow of water down a slope or by the upward movement of water. The upward flow of water occurs mainly in areas where there are heavy rainfalls followed by hot dry seasons during which evaporation is rapid. The top soil water is removed by plants and evaporation. The water below the surface is then drawn upwards. The weak solutions produced by the leaching of the rocks during the wet season, then become concentrated. Dissolved materials such as the hydroxides of aluminium and iron are then deposited (Holmes, Ref. 27). Kantey, (Ref. 29) states that slopes are essential for the formation of this soil type whereas Holmes, (Ref. 27) quotes flat areas where decomposed granite to depths of 10 metres and more have been found.

2.2.8 The processes involved in the chemical weathering of rock

Rain water acts as a carrier for dissolved oxygen and carbon dioxide and for various acids and organic products derived from the soil. Natural water is slightly dissociated into H^+ and OH^- ions. The pH of rain water varies between

four and seven (i.e. it is acidic). The acidity is formed mainly from dissolved carbon dioxide which ionises the water (see equation 2.1). The very low pH values might be due to a lightening discharge. The discharge produces nitric and other acids in small amounts. The effect of carbon dioxide (without lightning) is shown by the following equation:

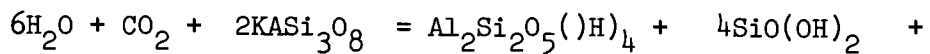


(Holmes, Ref. 27)

The main chemical changes which occur in the soil are:

- a) Solution of solubles by water
- b) Oxidation of certain substances
- c) Hydration or hydrolysis
- d) Formation of carbonates

The feldspars break down under the hydrolysing action of slightly carbonated waters. The main residual products of decomposition of feldspars are clay minerals and silicic acid.



orthoclase clay minerals silicic 'acid'



removed in solution

(Holmes, Ref. 27)

Most of the clay mineral initially exists in colloidal solution. Colloid particles are larger than ions, but smaller than can be seen by the microscope. The particles eventually congregate into tiny scales or flakes which coat the residual grains. These clay minerals form the clay bridges.

2.3 Conclusion

In areas where climatic conditions favour the formation of collapsing soils, consideration should be given to the behaviour of soils due to varying the moisture content of a load-bearing soil.

There are various methods to control the collapse phenomena of these soils (Knight, Ref. 28, Kantey, Ref. 29, Tschebotarioff, Ref. 22 and Robert Leslie and Partners). The most common method of inducing collapse before construction is the simultaneous inundation and loading of the soil.

CHAPTER 3

BRIEF OUTLINE OF THESIS WORK

3.1 Brief outline of thesis

At this stage of this thesis, it seems advisable to provide a brief guide to the major steps which were followed in planning and setting out the work of this thesis.

The fold-out flow chart in Figure 3.1 shows the main steps of the thesis. In some cases there might be a slight overlap of ideas between the conclusions discussed in the final Chapter of the thesis and Figure 3.1.

3.2 Comments concerning the flow chart in Figure 3.1

It will be noticed that Figure 3.1 is not a description of the conventional stress path method used for settlement prediction by Simons, Lambe and others. Instead Figure 3.1 can be regarded as one possible plan for investigating certain background assumptions which are implied in the use of a stress path method for settlement prediction.

Particular attention has been given to the comparison between the stress paths (for soil elements under footings) which follow either the K_0 stress path, or a more correct stress path in which Boussinesq type equations are used to find the stress increases due to the surface loading.

As a result of these comparisons it was found that the K_0 condition might be suitable for use even in a stress path approach to the settlement prediction for collapsing soils. A modification to the K_0 stress path occurs during collapse, in that the soil stress moves to another K_0 stress path line. However this would also occur in a consolidometer if a collapsing soil is wetted under loading. Hence the consolidometer is still a good instrument for the laboratory studies of collapsing soils, even if one wishes to simulate the field stress path.

The method used to find the extra stresses in a soil due to a uniform surface loading, is not necessarily the only method, nor the best method. It was however a convenient technique based on the principle of superposition for elastic medium.

Although soil is not a true elastic medium, it has been assumed that the stresses calculated for a surface load on an elastic medium will be approximately correct for the soil; even if the resulting strains for a soil may differ from those of an elastic medium.

Investigating possible stress paths

Comparing stress paths

Tests using the K_0 approximation to the stress path.

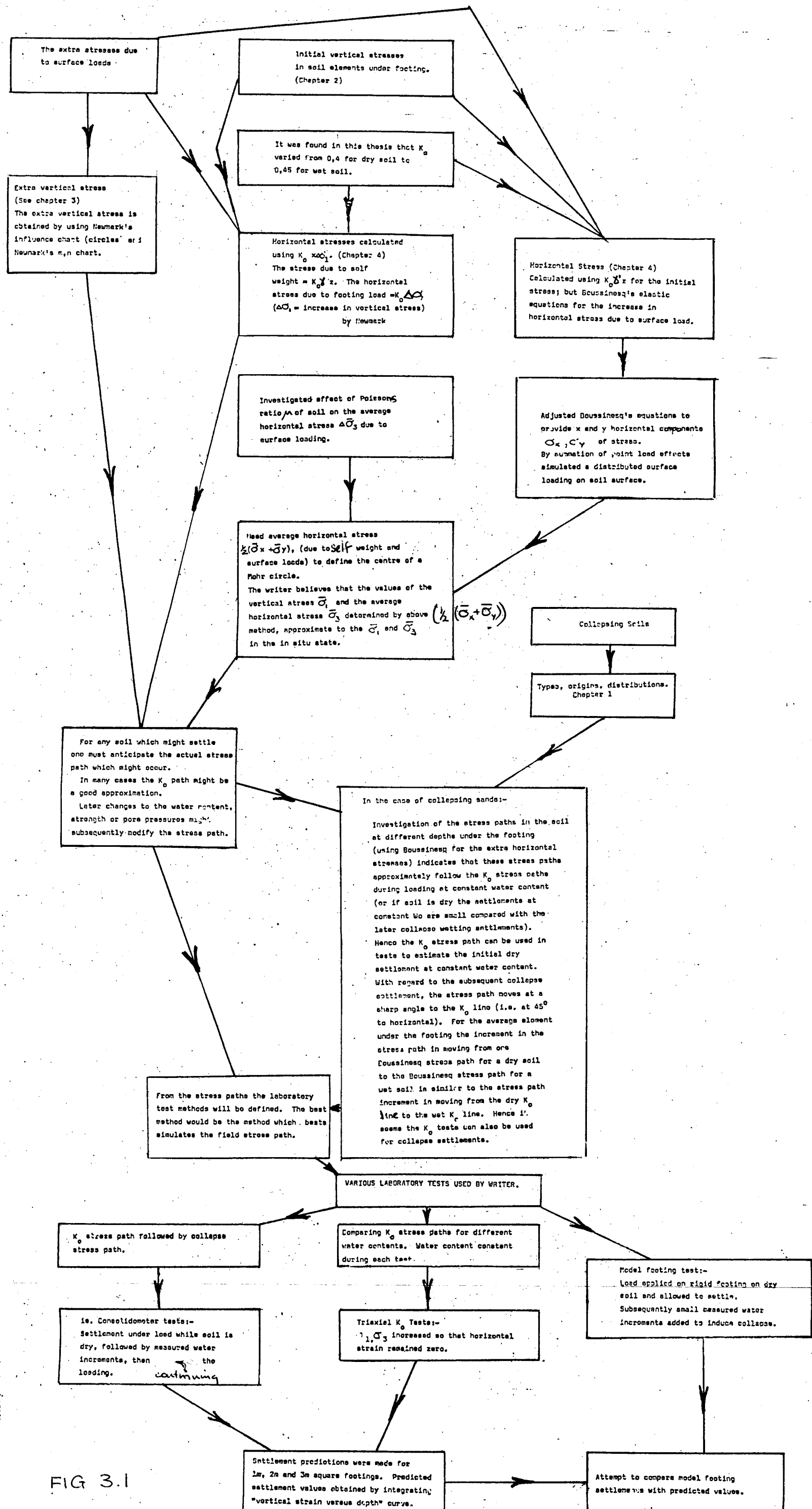


FIG 3.1

C H A P T E R 4

VERTICAL STRESSES WITHIN A SOIL MASS

4.1 Introduction to the boundary conditions of elastic formulae

When designing a foundation system the engineer must determine whether the given soil mass will support the load imposed on it by the foundation. The term 'support' implies that both the bearing capacity and the settlement criteria are satisfied. It is therefore necessary to be able to define the magnitude and distribution of the stresses produced under the action of the design load. Formulae are usually based upon the assumptions of:

- a) elasticity
- b) homogeneity
- c) semi-infinite soil mass
- d) isotropy

Isotropy is defined as identical elastic properties in every direction through a certain point of the solid. Homogeneity is defined as involving identical elastic properties at every point of the solid (Lambe and Whitman, Ref. 2 and Terzaghi, Ref. 1).

4.2 Dry soil

The measuring of the stresses within a soil mass is difficult as the presence of a stress gauge disrupts the stress field that would otherwise exist if the stress gauge were not present. This effect would depend upon the type of soil, the average grain size and the size of the loaded area. 'In a dry soil, stress may be thought of as the force in the mineral skeleton per unit of area' (Lambe and Whitman, Ref. 2). To define this Lambe considers a plane through a soil mass.

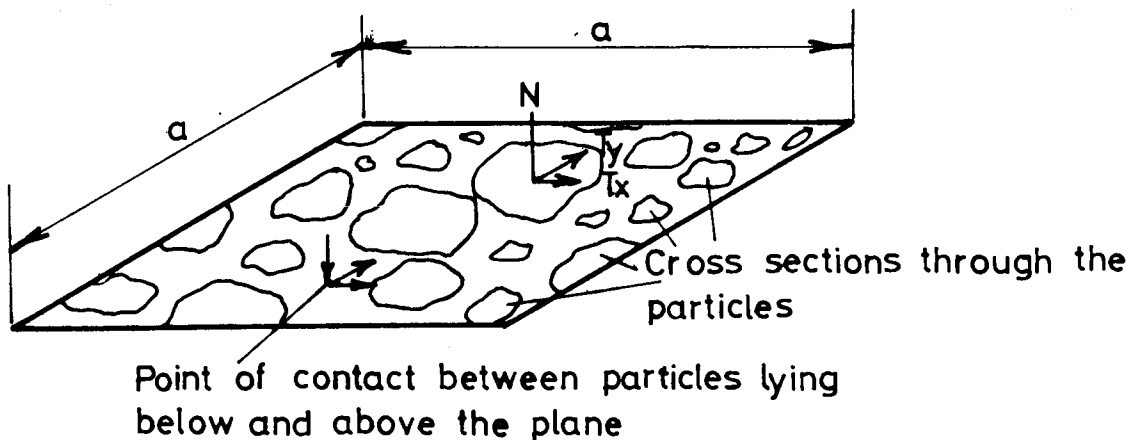
This plane passes through pore space as well as through mineral matter. At each point where this plane passes through mineral matter, the forces on these faces can be resolved into components normal and tangential to the plane. These forces are

then resolved further to fit into some global coordinate system. The summation of the forces along the vertical axis divided by the area of the plane will define the vertical stress (see Figure 3.1). The shear stresses and the horizontal stresses are similarly defined.

It is important to note that the macroscopic stresses as described above are different from the stresses existing at points of contact between particles. The above definition allows the forces acting at a point to be defined as the forces acting against the sides of an infinitesimally small cube of typical soil.

4.3 Geostatic stresses

Geostatic stresses exist when there are no shear stresses acting on vertical and horizontal planes within a soil mass. The stress is also due to self weight of the soil mass alone.



$$\sigma_v = \frac{\sum N}{a \times a}$$

FIGURE 4.1 *Definition of Stress within a Soil Mass*

4.3.1 Equations based on elastic theories

Most soil mechanics formulae are based on the assumption that the soil strictly follows Hooke's law. (Ratio between a linear stress, σ , and the corresponding linear strain, ϵ , is constant (Terzaghi, Ref. 1).

$$\frac{\sigma}{\epsilon} = E \quad (4.1)$$

The value of E is derived from the results of the unconfined compression test.

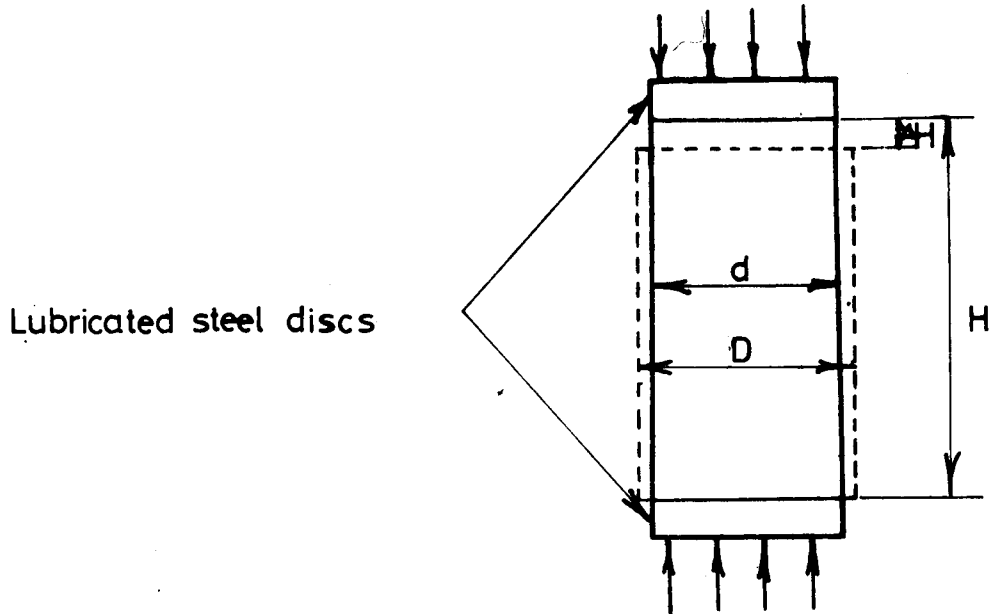


FIGURE 4.2 *Deformations which Occur During the Unconfined Compression Test (Lambe, Ref. 5 and Terzaghi, Ref. 1)*

The vertical load applied will produce both a positive vertical strain and a negative horizontal strain.

$$\epsilon_v = \frac{\Delta H}{H} \quad (4.2)$$

$$\epsilon_h = \frac{\Delta d}{d} \quad (4.3)$$

where $D-d = \Delta d$

The absolute value of the strain ratio ϵ_h/ϵ_v is termed Poisson's Ratio (μ). The reciprocal of this ratio is called Poisson's number (m).

4.3.2 The upper and lower limits of Poisson's ratio

Poisson's ratio has been defined as either the ratio of lateral extension to longitudinal contraction for a cylindrical specimen in compression or the ratio of lateral compression to longitudinal extension for a specimen in tension. Therefore by definition if μ were to be negative one of the following situations would have to occur.

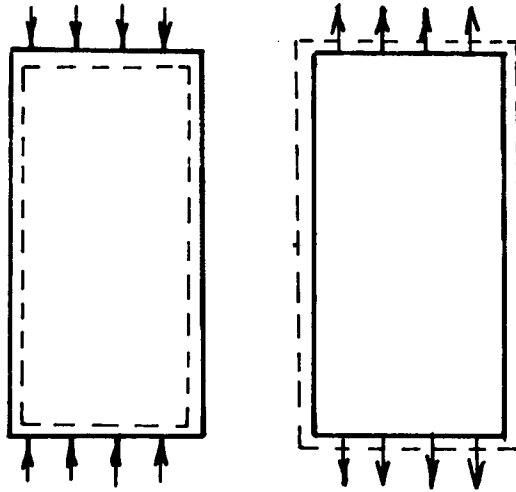
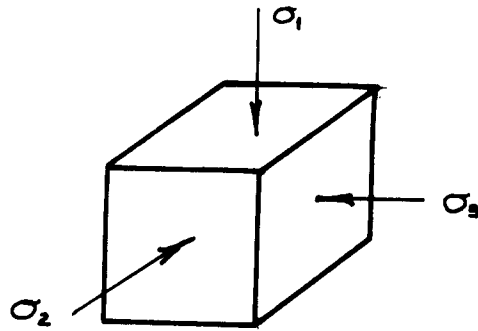


FIGURE 4.3 *Deformations Associated with Negative Values of μ*
(Rauch, Ref. 17)

For all truly elastic materials the situations in Figure 4.3 are unknown. These conditions therefore define the lower limit of Poisson's ratio, i.e. μ must be positive. However the writer believes that if the void ratio changes during shear (e.g. from a dense packing to a looser packing), care must be exercised in defining μ .



$$\sigma_1 = \sigma_2 = \sigma_3$$

FIGURE 4.4 *Isotropic Stress Application*

If a sample is subjected to an isotropic stress system and if equations (4.1), (4.2) and (4.3) are satisfied then the strain in any one of the three principal directions is $\frac{\sigma}{E} - 2\mu \frac{\sigma}{E}$

$$\text{The volumetric strain} = \frac{\Delta V}{V}$$

$$= 3 \frac{\sigma}{E} (1 - 2\mu) \quad (4.4)$$

(if a small strain occurs)

From equation (4.4) it is evident that for μ equal to 0,5 the material is incompressible. The range of μ therefore is zero to 0,5.

Terzaghi (Ref. 1) also states that for dense soils and solid granular materials μ varies considerably in magnitude between relatively low stresses and failure stresses. In most formulae applied to soil mechanics μ is considered to remain constant. It is therefore necessary to view this assumption with caution when considering the behaviour of collapsing soil types as the stresses approach failure values.

4.3.3 The relationship between vertical and horizontal stresses

The ratio of the horizontal effective stress to the vertical effective stress is defined by the coefficient of lateral pressure, K , where

$$K = \frac{\sigma_3}{\sigma_1} \quad (4.5)$$

If a prism of material with unit weight γ kN/m³ is placed on a perfectly frictionless base, the stresses caused by the self weight will produce a vertical compression and a lateral expansion (see Figure 4.5).

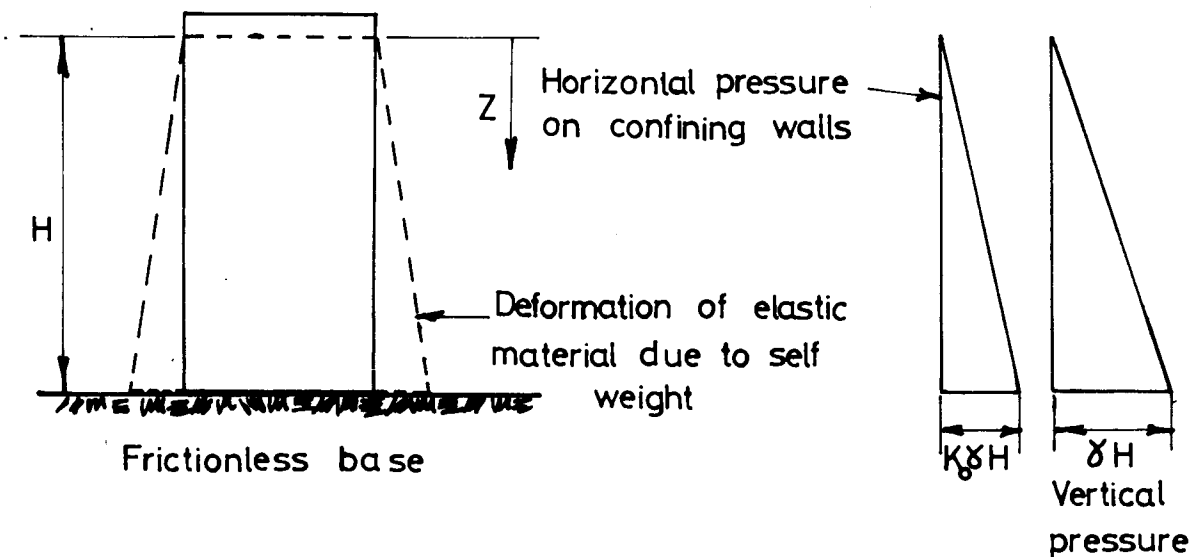


FIGURE 4.5 *Deformations and Stresses Associated with a Prism of Soil acted upon by Self Weight Alone (Terzaghi, Ref. 1)*

In Figure 4.5, any depth z the vertical stress is equal to γz kN/m². Applying equations (4.3) and (4.4) an expression of lateral strain in terms of vertical stress for any depth z is obtained.

The soil prism (cross section) can now be considered to be laterally confined in both horizontal directions between walls of exactly the same soil material, and to rest on a rough base.

A horizontal pressure σ_3 will then be developed along the vertical walls. When compared with the unconfined case in Figure 4.5 this horizontal stress will cause horizontal strains ϵ'_3 due to σ_3 . i.e.

$$\begin{aligned}\epsilon'_3 &= \frac{\sigma_3}{E} - \mu \frac{\sigma_3}{E} \\ &= \frac{\sigma_3}{E} (1 - \mu)\end{aligned}$$

The absolute values of this strain must be equal to the strain which existed in Figure 4.5 for the unrestrained case.

$$\frac{\mu \gamma z}{E} = \frac{\sigma_3}{E} (1 - \mu)$$

$$\therefore \sigma_3 = \frac{\mu}{1 - \mu} \gamma z$$

Therefore

$$\sigma_3 = \left(\frac{\mu}{1 - \mu} \right) \sigma_1 = K_o \sigma_1 = K_o \gamma z \quad (4.6)$$

where

$$K_o = \frac{\mu}{1 - \mu}$$

Where K_o is defined as the coefficient of lateral pressure at rest i.e. when no horizontal deformation is permitted.

(Compare K_o with the general notation for K in equation (4.5)).

4.4 Stresses and displacements produced in a semi-infinite solid, with a horizontal surface, due to an imposed loading system

In Figure 4.6 let N' be any point on the surface of a soil mass distance r away from the point of application of a point load Q . N is a point directly below N' , at depth z below ground

level. The stresses and strains (See Figure 4.6) that exist at point N are described by Boussinesq's equations (see equations (4.7) to (4.12)).

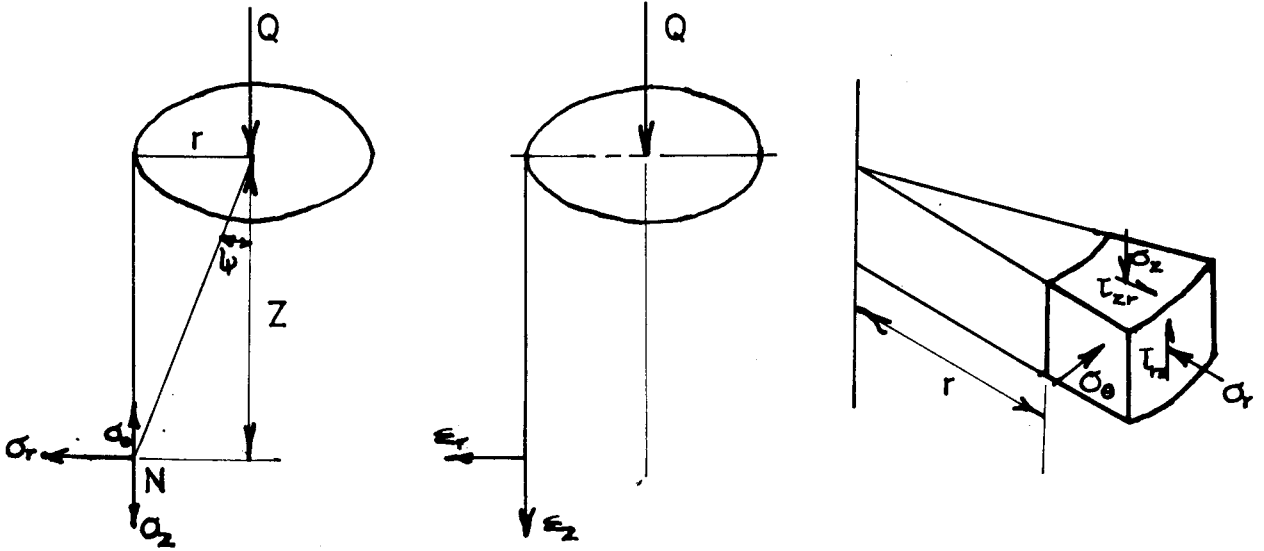


FIGURE 4.6 Definition of the Stresses and Strains Described by Boussinesq's Equations (Terzaghi, Ref. 1 & Zeevaert, Ref. 14)

Boussinesq's equations as stated below strictly satisfy the boundary conditions described in the beginning of this Chapter and as such are only within the acceptable limits of accuracy where these conditions are approximated.

The equations of stress according to Boussinesq are as follows:

$$\sigma_z = \frac{3Q}{2\pi z^2} \cos^5 \psi \quad (4.7)$$

$$\sigma_r = \frac{Q}{2\pi z^2} \left[3 \cos^3 \psi \sin^2 \psi - (1 - 2\mu) \frac{\cos^2 \psi}{1 + \cos \psi} \right] \quad (4.8)$$

$$\sigma_\theta = - (1 - 2\mu) \frac{Q}{2\pi z^2} \left[\cos^3 \psi - \frac{\cos^2 \psi}{1 + \cos \psi} \right] \quad (4.9)$$

$$\tau_{rz} = \frac{3Q}{2\pi z^2} \cos^4 \psi \sin \psi \quad (4.10)$$

Displacement equations:

$$\epsilon_z = \frac{Q}{2\pi r} \frac{1 + \mu}{E} \left[2(1 - \mu) + \cos^2 \psi \right] \sin \psi \quad (4.11)$$

$$\epsilon_r = \frac{Q}{2\pi r} \frac{1 + \mu}{E} \left[- (1 - 2\mu) + \cos \psi + \cos^2 \psi \right] \sin \psi \tan \frac{\psi}{2} \quad (4.12)$$

where

- Q = the concentrated load on the surface
- r = the horizontal radial distance between an arbitrary point N below the surface and a vertical axis through the point of application of Q
- ψ = the angle between N and the vertical axis through the point of application of Q
- z = the depth below the surface of N
- σ_z = the vertical normal stress
- σ_r = the horizontal radial normal stress
- σ_θ = the horizontal circumferential normal stress
- τ_{rz} = the shear stress in the directions of r and z
- μ = Poisson's ratio for the solid
- ϵ_z = the vertical displacement of the point N, taken as positive for a downward displacement
- ϵ_r = the horizontal radial displacement, taken as positive for an outward displacement

These equations all assume that the unit weight of the material is zero. The stress obtained is therefore only due to the imposed surface load Q . The determination of the stresses due to self weight has already been described (see equation (4.6)). The summation of these two stress systems will define a stress state for a point within the soil (due to self weight and the load Q).

4.4.1 Vertical stresses due to uniformly distributed loads

The formulae available to the engineer for the determination of stresses due to distributed loads apply only to stresses produced by a flexible area load (i.e. surface loading intensity q is constant). A flexible area load implies that there is no rigid structure such as a footing between the load and the soil surface. To determine the effect of the uniformly distributed load, the load is divided into an infinite number of discrete point loads $q dA$ (see Figure 4.7). Where A is the flexible loaded area and q is the intensity of the uniformly distributed load.

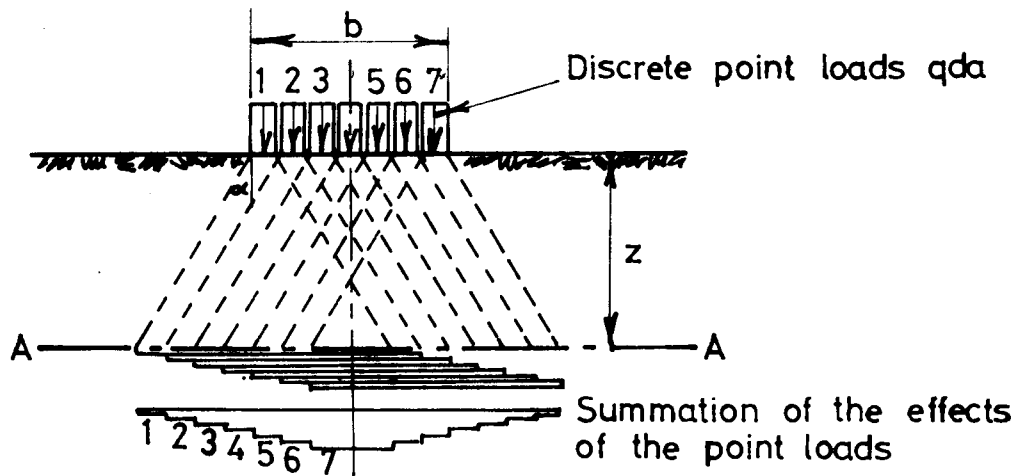


FIGURE 4.7 *Illustration of the Division of an Uniformly Distributed Load into a Number of Point Loads (Tschebotarioff, Ref. 22)*

Terzaghi (Ref. 1) quotes formulae applying to line loads, strip loads and circular loads.

For a line load (see Figure 4.8)

$$\sigma_1 = \frac{2q'}{\pi z} \cos^4 \psi \quad (\text{vertical}) \quad (4.13)$$

$$\sigma_3 = \frac{2q'}{\pi z} \cos^2 \psi \sin^2 \psi \quad (\text{horizontal}) \quad (4.14)$$

$$\tau_{13} = \frac{2q'}{\pi z} \cos^2 \psi \sin \psi \quad (4.15)$$

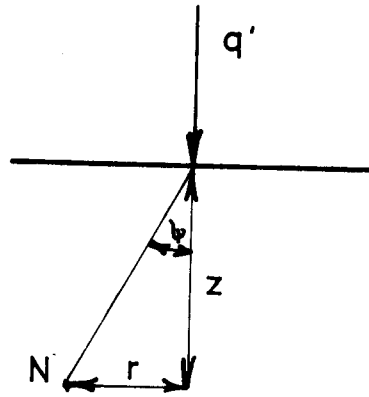


FIGURE 4.8 Stresses at N due to Line Load q' are Described by Equations 4.13 and 4.15

For a strip load (see Figure 4.9 and 4.10)

$$\sigma_1 = \frac{q}{\pi} \left[\sin\psi \cos\psi + \psi \right]_{\psi_1}^{\psi_2} \quad (\text{vertical}) \quad (4.16)$$

$$\sigma_3 = \frac{q}{\pi} \left[-\sin\psi \cos\psi + \psi \right]_{\psi_1}^{\psi_2} \quad (\text{horizontal}) \quad (4.17)$$

$$\tau_{13} = \frac{q}{\pi} \sin^2\psi \quad (4.18)$$

For a uniform loading on a circular area (see Figure 4.11)

$$\sigma_z = q \left[1 - \left\{ \frac{1}{1 + (R/z)^2} \right\}^{\frac{3}{2}} \right] \quad 4.18b.$$

(under the centre of the loaded circle)

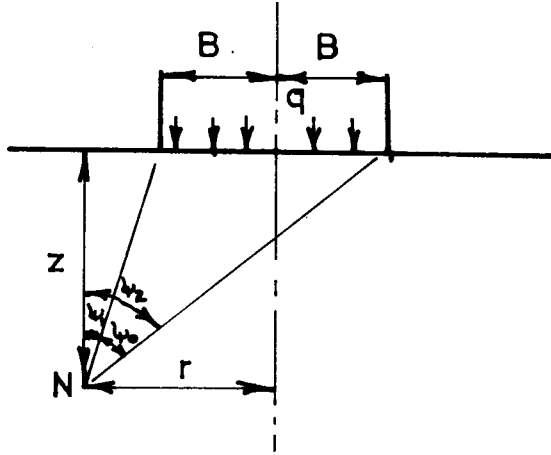


FIGURE 4.9 Stresses at N due to a Strip Load q are Described by Equations 4.16 and 4.18

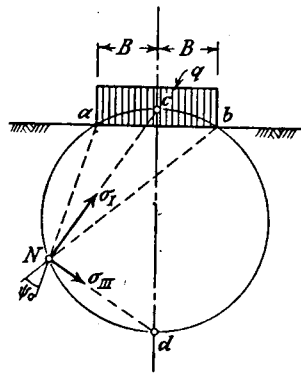


FIGURE 4.10 Illustration of a Simple Construction to Determine the orientation of the Principal Stresses at N due to a uniformly distributed Strip Load (Terzaghi, Ref. 1)

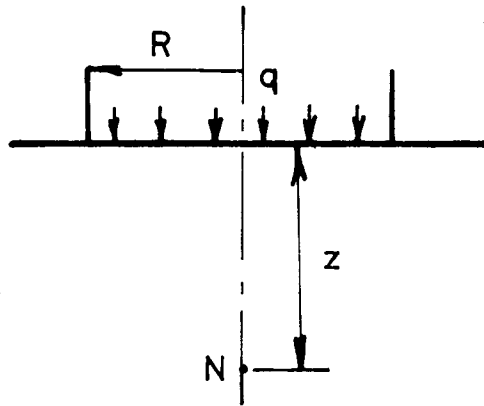


FIGURE 4.11 Stress at Point N, due to Loading q on a Circular Flexible Footing, is defined by Equation 4.18b

4.4.2 Influence values

An influence value (see Figure 4.14) is a dimensionless quantity that enables the stress at any point within a soil mass to be determined merely by multiplying this value by Q/z , or q'/z where q' is a line load causing a pressure at depth z . The parameters used for multiplication depend on whether the load is uniformly distributed, a line load or a concentrated load.

Newmark, in 1935, obtained from integration of Boussinesq's formula for a concentrated load the following:

$$\frac{\Delta\sigma}{q} = \frac{1}{4\pi} \left[\frac{2mn}{m^2 + n^2 + 1 + m^2 n^2} \frac{\sqrt{m^2 + n^2 + 1}}{m^2 + n^2 + 1} + \sin^{-1} \frac{2mn}{m^2 + n^2 + 1 + m^2 n^2} \right] \quad (4.19)$$

where

$$m = B/z$$

$$n = L/z$$

B = the breadth of the footing

L = the length of the footing

$\Delta\sigma_1$ = the change in stress at any point N , depth z below the corner of a rectangle

The increase in vertical stress at N (see Figure 4.12) can be calculated for the loaded area $dehi$ by addition and subtraction of various rectangles (Terzaghi, Ref. 1).

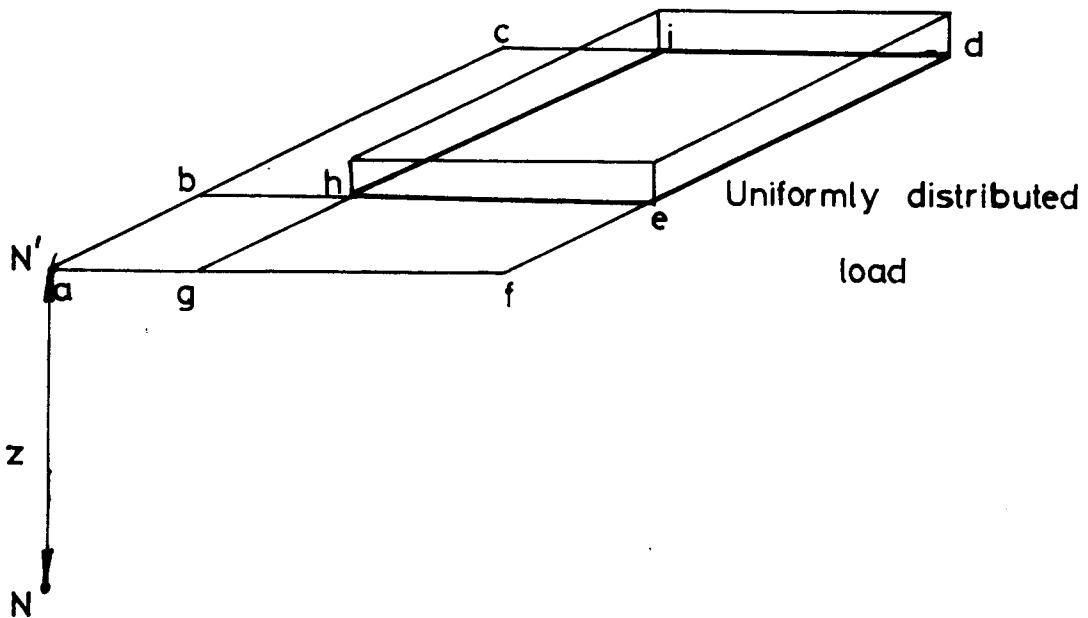


FIGURE 4.12 Point N at which Stress is to be Calculated

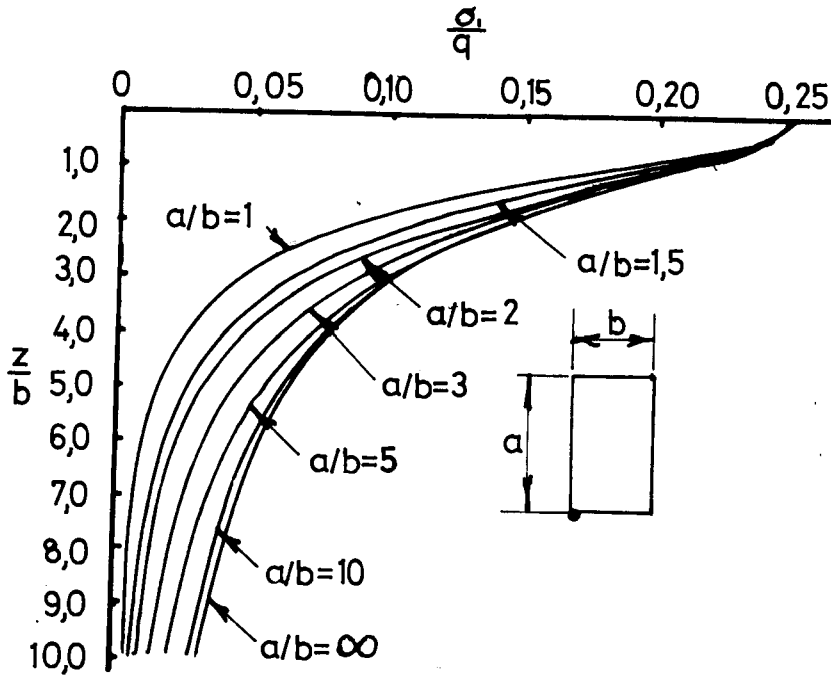


FIGURE 4.13 Chart of Stress Values for Point at Depth z below Corner of Footing (Tschebotarioff, Ref. 22)

Equation (4.19) can be rewritten as

$$\Delta\sigma_1 = q f(m,n) \quad (4.20)$$

For the direct solution to equation (4.20) a chart (see Figure 4.14) has been drawn. This chart defines $f(m,n)$ for particular values of m and n .

Another form of equation (4.20) is

$$\Delta\sigma_1 = q I_\sigma \quad (4.21)$$

From the curves shown in Figure 4.15 values of I_σ can be found for any value of z/B and L/B . I_σ is called an influence value (for stress).

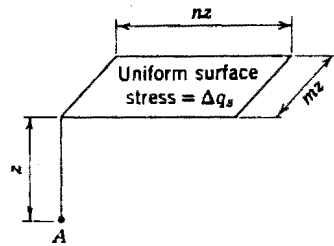
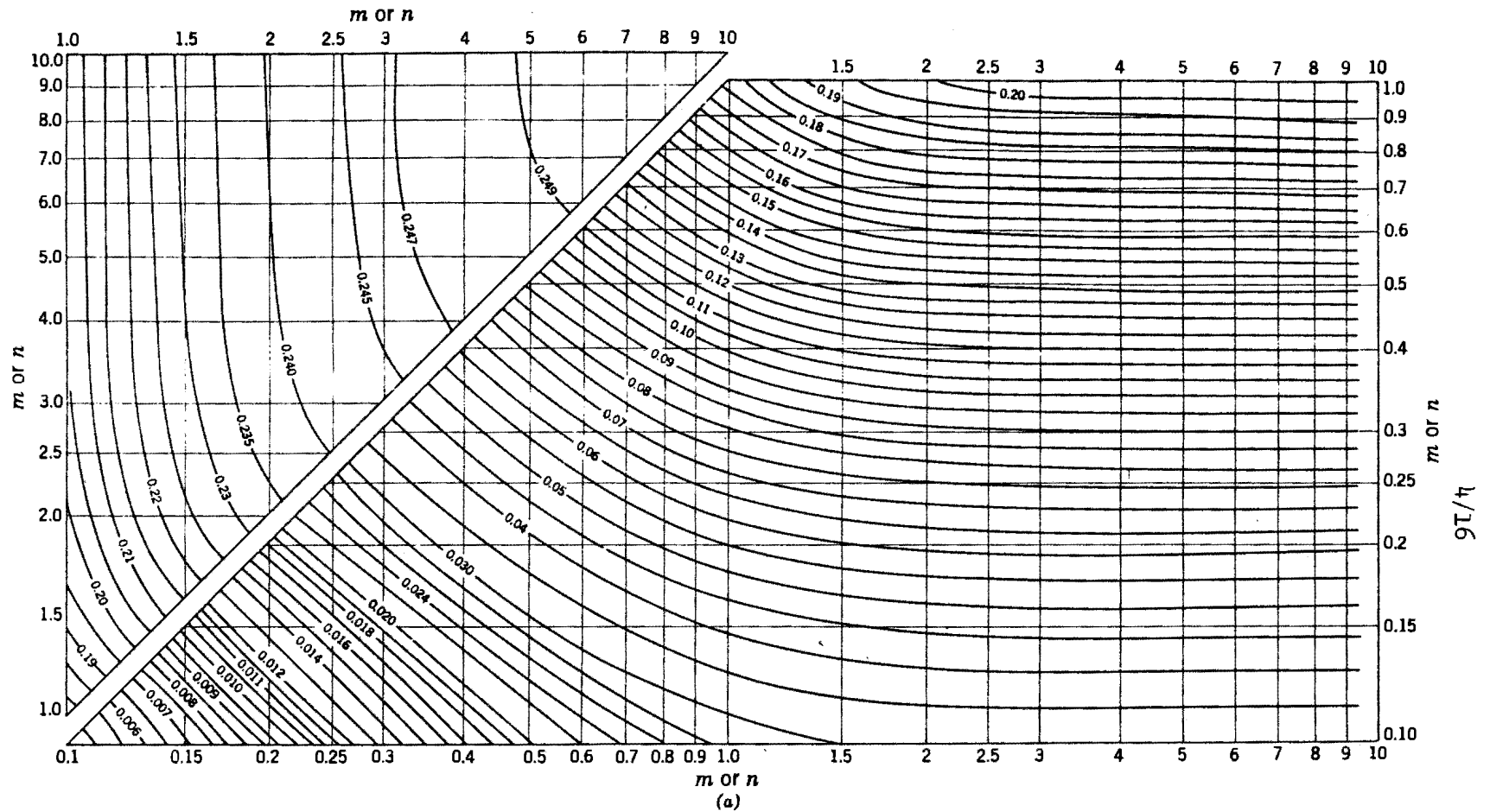


FIGURE 4.14

Chart for Determining the Stress Factor at a Point N
Situated at Depth z below the Corner of a footing

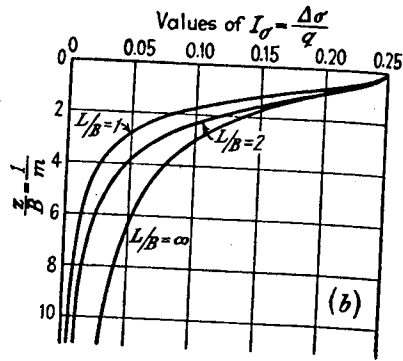


FIGURE 4.15 Stress Influence Value at Depth z under a Corner of a Rectangular Loaded Area (Terzaghi, Ref. 1)

4.4.3. Newmark influence chart

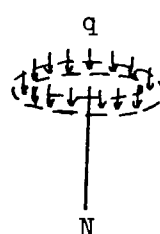
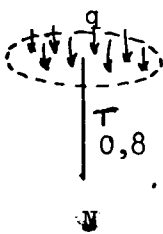


FIGURE 4.16(a)

4.16(b)

4.16(c)

4.16(d)

Suppose that in Figure 4.16(a) r is such that the stress at N due to the loaded area is $0,8 q$. If r in Figure 4.16(b) is chosen so that the stress caused is $0,7 q$, then the stress caused due to Figure 4.16(c) is $0,1 q$. Similarly in Figure 4.16(d) the stress at N is $0,1 \times 0,1 q$ for each of the loaded portions.

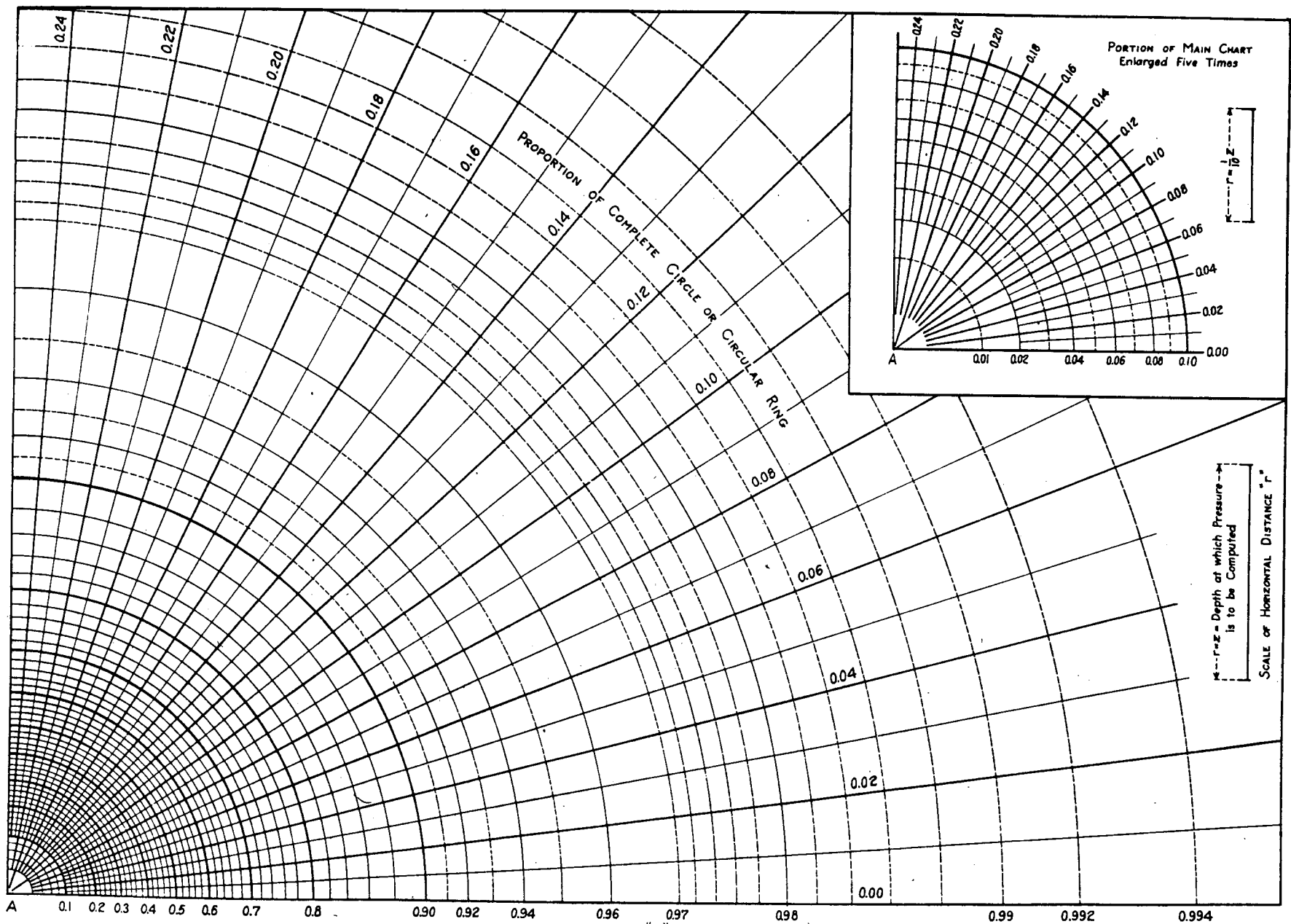
Newmark's influence chart (see Figure 4.17) is used to find the extra stress at any point within a soil mass due to a surface loading. To evaluate the stress, the footing is drawn to a scale dependent upon the depth below founding level of the point at which the stress must be determined. The scale is determined by equating OA to the depth of the point considered. Then the number of elemental areas covered by the drawn footing is counted. The number of elemental areas counted multiplied by the chart constant and the uniformly distributed loading will produce the required vertical pressure. The chart constant will depend only on the number of elemental areas that the chart contains. Note that the self weight effect of the soil must be added to the above vertical stress caused by the footing load.

4.5 Conclusion

For a footing which causes a uniformly distributed load on the soil, the increase in vertical stress at a point in the soil can be calculated. In practice however rigid footings are a common occurrence.

Rigid footings tend to prevent the uniform distribution of contact pressures to the soil. The contact pressures can vary considerably across a rigid footing. The contact pressure distribution depends on the stress parameters E and μ for the footing and for the subgrade. For the prediction of settlements, the contact pressure is considered to be uniform and the settlement results are then modified to allow for non-uniform contact pressures (see Chapter 7).

FIGURE 4.17 Neumark Influence Chart (Plummer, Ref. 37)



In 1936 Borowicka (Ref. 2) established a formula to describe the contact pressure distribution. The formula defines a subgrade reaction K_r value for given stress parameters of the soil and the footing and for a given footing size. For a circular footing Borowicka stated that K_r has the following value.

$$K_r = \frac{1}{6} \frac{1 - \mu_s^2}{1 - \mu_p^2} \frac{E_p}{E_s} \left(\frac{H}{R} \right)^3 \quad (4.22)$$

where

- μ_s = Poisson's ratio for subgrade reaction
- μ_p = Poisson's ratio for the footing
- E_s = Young's modulus for the subgrade
- E_p = Young's modulus for the footing
- H = Thickness of footing
- R = Radius of circular footing

For an infinite strip load K_r has the following value

$$K_r = \frac{1}{6} \frac{1 - \mu_s^2}{1 - \mu_p^2} \frac{E_p}{E_s} \left(\frac{H}{B} \right)^3 \quad (4.23)$$

A value of K_r equal to zero indicates constant contact pressure (e.g. a perfectly flexible raft carrying a uniform loading).

Figures 4.18(a) and 4.18(b) show various contact pressures for different values of K_r (Terzaghi, Ref. 1 and Lambe and Whitman, Ref. 2).

Figure 4.19 shows lines of equal vertical pressure in sand as measured during the Freiburg tests. The angle ϕ_o is measured between the zero pressure curve (due to Q) and the vertical. As one approaches the footing this angle varies until it reaches the value of 90° at the footing.

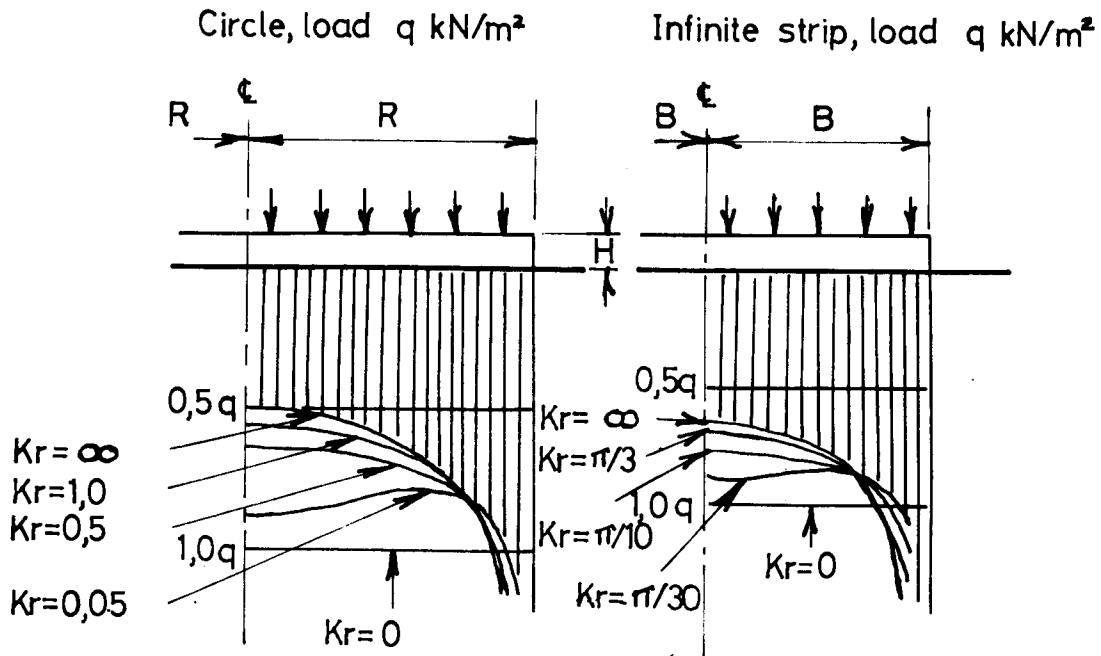


FIGURE 4.18(a)

FIGURE 4.18(b)

Uniform Loadings on Semi-flexible Bases

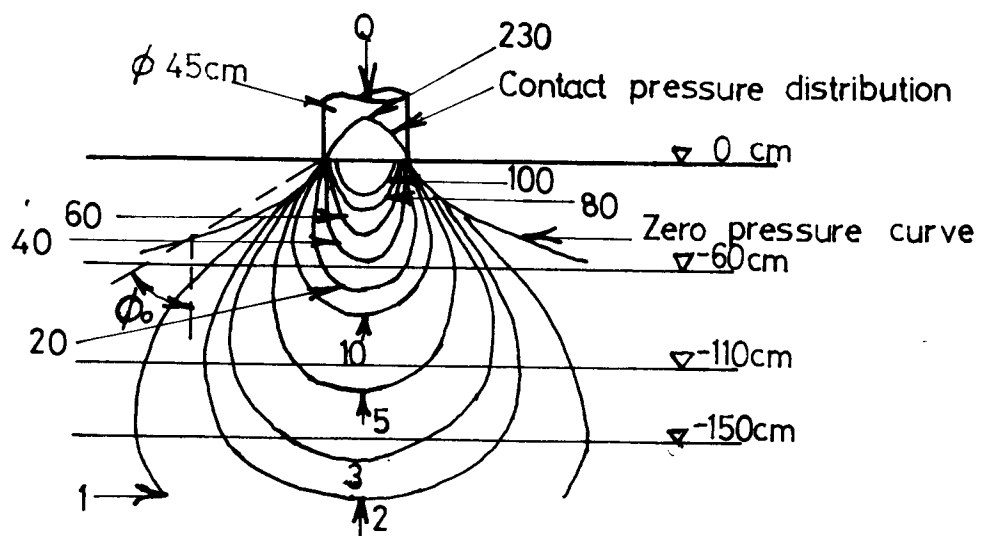


FIGURE 4.19 Lines of Equal Vertical pressure (due to Q) as measured in Sand (Tschebotarioff, Ref. 22)

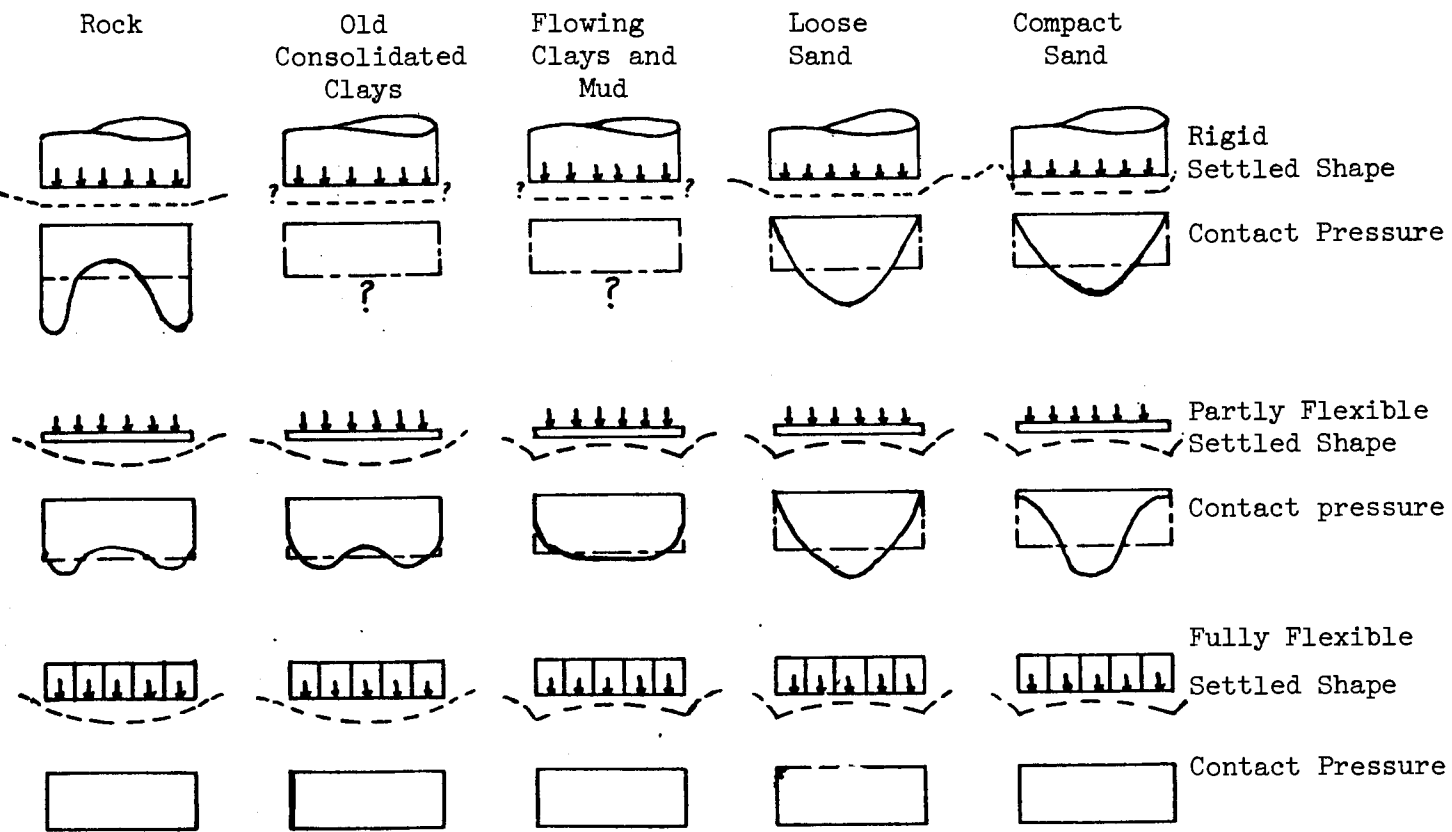


FIGURE 4.20 Shows Different Settlement and Contact Pressure Distributions for Different Types of Footings and Soil Formations (Plummer, Ref. 37)

Because of the variations shown in Figure 4.20 it is the duty of the civil engineer not to merely apply formulae but also to adjust the idealised values he obtains to the problem under consideration.

CHAPTER 5

HORIZONTAL STRESS DISTRIBUTIONS

5.1 Introduction to horizontal stresses due to vertical loads

Horizontal stress distributions can be calculated from elastic formulae or might be approximated by multiplying the vertical stress (due to self weight and surface loading) by the factor K_0 (i.e. assuming zero horizontal strain). The assumption of zero horizontal strain is a simplification and is not always accurate. The variations in the results obtained from the two different methods can become appreciable, especially near the surface. These two methods can cause different stress paths at different points in the soil and therefore the settlement predictions by the two methods will not be identical. In order to decide on the stress path which must be followed in a laboratory test used for settlement prediction, it is necessary to accurately anticipate the stress path which might be followed by a soil element under the proposed foundation. Soil elements at different positions under the footing will follow different shapes of stress paths. Stress paths are defined and discussed in Chapter 6.

5.2 Using Boussinesq's equations to approximate horizontal stresses due to a concentrated surface load

At this stage we will neglect the self weight effect of the soil. To define stresses within a soil mass a constant coordinate system (see Figure 5.1) is generally used. Boussinesq's equations yield values for radial and tangential horizontal stress. Use can be made of Mohr's circle of stress (see Chapter 7) to find the components of stress in the x and y directions.

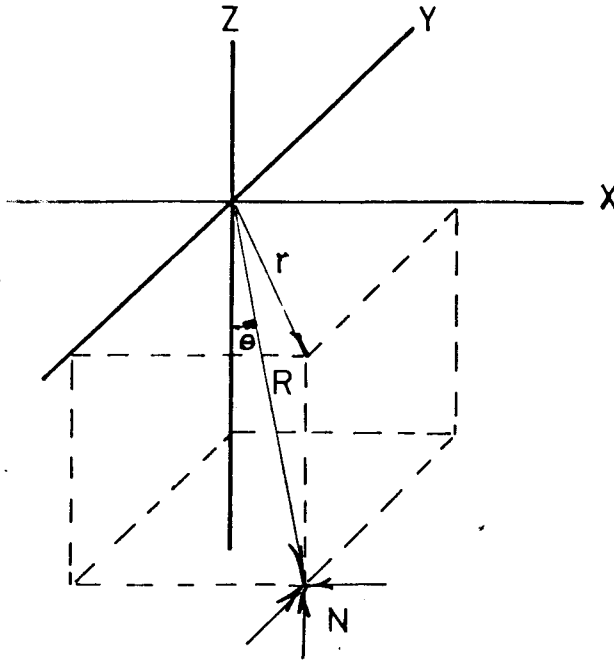


FIGURE 5.1 Definition of the Co-ordinate System

Timoshenko (Ref. 50) shows that the stress normal to any plane (see Figure 5.2) at any point within an elastic medium can be expressed in terms of stresses σ_x , σ_y , σ_z , τ_{yz} , τ_{xz} , τ_{xy} the stresses acting on three mutually perpendicular planes as

$$\begin{aligned} \sigma_n = & \sigma_x \ell^2 + \sigma_y m^2 + \sigma_z n^2 + 2\tau_{yz} mn + 2\tau_{xz} \ell n \\ & + 2\tau_{xy} \ell m \end{aligned} \quad (5.1)$$

where

$$\begin{aligned} \text{Cos}(N_x) &= \ell \\ \text{Cos}(N_y) &= m \\ \text{Cos}(N_z) &= n \end{aligned}$$

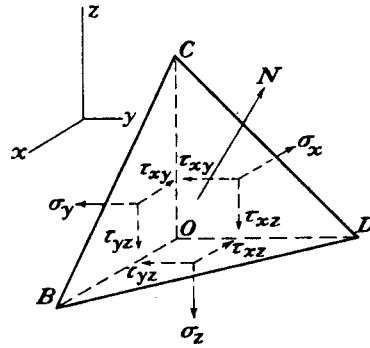


FIGURE 5.2 The Normal Stress σ_n Acting on plane CBD in Direction ON

The stresses obtained from Boussinesq's equations are defined in Figure 5.3. These stresses must now be orientated to yield σ_x and σ_y in the chosen x,y coordinate system (Figure 5.4).

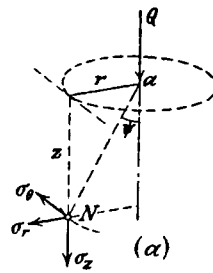


FIGURE 5.3 Stresses Defined by Boussinesq's Equations

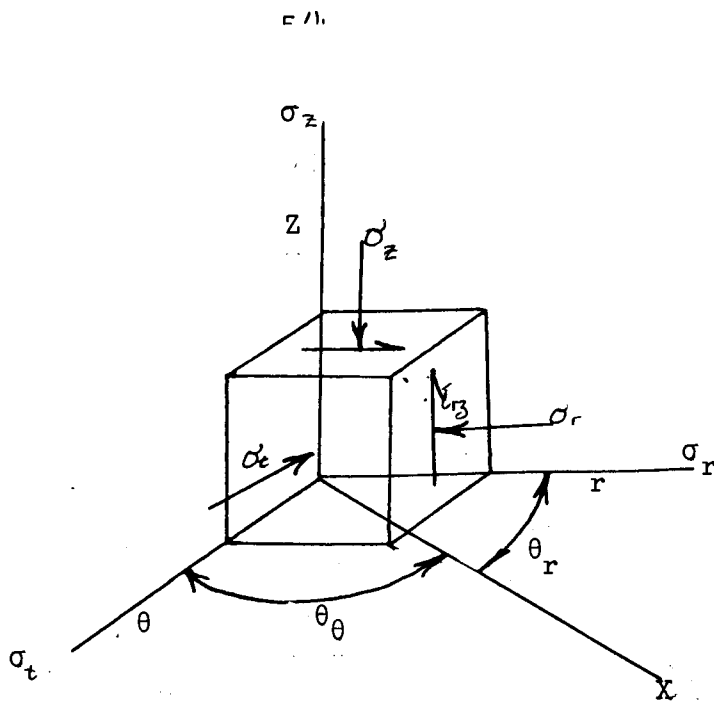


FIGURE 5.4 The Modification of the Boussinesq's Stresses to yield horizontal stresses σ_x, σ_y in the x, y coordinate system

From Figure 5.4 the direction cosines can be defined.

These are:

$$\cos(ZX) = \cos 90^\circ = 0 = n$$

$$\cos(rX) = \cos \theta_r = l$$

$$\cos(\theta X) = \cos \theta_\theta = m$$

Therefore from equation (5.1)

$$\sigma_x = \sigma_z n^2 + \sigma_t m^2 + \sigma_r l^2 + 2\tau_{rz} ln + 2\tau_{tz} mn + 2\tau_{rt} lm$$

Because $n = 0$, $\tau_{tz} = 0$ and $\tau_{rt} = 0$

$$\sigma_x = \sigma_t m^2 + \sigma_r l^2$$

$$= \sigma_t \sin^2 \theta_r + \sigma_r \cos^2 \theta_r \quad (5.2)$$

Similarly

$$\sigma_y = \sigma_t \cos^2 \theta_r + \sigma_r \sin^2 \theta_r \quad (5.3)$$

Substituting Boussinesq values for σ_t and σ_r into equation 5.2 and 5.3 the following is obtained:

$$\begin{aligned}
 \sigma_x &= \frac{y^2}{x^2+y^2} \left[- (1-2\mu) \frac{Q}{2\pi z^2} \right] \left[\frac{z^3}{(x^2+y^2+z^2)^{\frac{3}{2}}} - \frac{z^2}{x^2+y^2+z^2+z} \frac{1}{\sqrt{x^2+y^2+z^2}} \right] \\
 &+ \frac{Q}{2\pi z^2} \frac{x^2}{x^2+y^2} \left[\frac{3x^2z^3 + 3y^2z^3}{(x^2+y^2+z^2)^{\frac{5}{2}}} - (1-2\mu) \frac{z^2}{x^2+y^2+z^2+z} \frac{1}{\sqrt{x^2+y^2+z^2}} \right] \\
 &= \frac{Q}{2\pi} \left[\frac{x^2}{x^2+y^2} \left(\frac{3x^2z + 3y^2z}{(x^2+y^2+z^2)^{\frac{5}{2}}} \right) - \frac{(1-2\mu)y^2}{x^2+y^2} \right. \\
 &\quad \left(\frac{z}{(x^2+y^2+z^2)^{\frac{3}{2}}} - \frac{1}{x^2+y^2+z^2+z} \frac{1}{\sqrt{x^2+y^2+z^2}} \right) \\
 &\quad \left. - \frac{(1-2\mu)x^2}{x^2+y^2} \left(\frac{1}{x^2+y^2+z^2+z} \frac{1}{\sqrt{x^2+y^2+z^2}} \right) \right] \quad (5.4)
 \end{aligned}$$

$$\begin{aligned}
 \sigma_y &= \frac{Q}{2\pi} \left[\frac{y^2}{x^2+y^2} \frac{3x^2z + 3y^2z}{(x^2+y^2+z^2)^{\frac{5}{2}}} - \frac{(1-2\mu)x^2}{x^2+y^2} \right. \\
 &\quad \left(\frac{z}{(x^2+y^2+z^2)^{\frac{3}{2}}} - \frac{1}{x^2+y^2+z^2+z} \frac{1}{\sqrt{x^2+y^2+z^2}} \right) \\
 &\quad \left. - \frac{(1-2\mu)y^2}{x^2+y^2} \left(\frac{1}{x^2+y^2+z^2+z} \frac{1}{\sqrt{x^2+y^2+z^2}} \right) \right] \quad (5.5)
 \end{aligned}$$

where

$$r = x^2 + y^2$$

$$R = x^2 + y^2 + z^2$$

$$\sigma_r = \frac{Q}{2\pi z^2} \left[3 \frac{z^3 (\sqrt{x^2 + y^2})^2}{(x^2 + y^2 + z^2)^{5/2}} - (1-2\mu) \frac{z^2}{x^2 + y^2 + z^2 + z \sqrt{x^2 + y^2 + z^2}} \right]$$

$$\sigma_t = -(1-2\mu) \frac{Q}{2\pi z^2} \left[\frac{z^3}{(x^2 + y^2 + z^2)^{3/2}} - \frac{z^2}{x^2 + y^2 + z^2 + z \sqrt{x^2 + y^2 + z^2}} \right]$$

$$\sin^2 \theta_r = \frac{y^2}{(\sqrt{x^2 + y^2})^2}$$

$$\cos^2 \theta_r = \frac{x^2}{x^2 + y^2}$$

5.3 Approximation of horizontal stresses due to uniformly distributed surface loads

Equations 5.4 and 5.5 were expressly derived to facilitate the application of Boussinesq's equations to determine horizontal stresses within a soil mass subjected to a uniformly distributed surface load.

The effect of the uniformly distributed load can once more be considered as a large number of concentrated loads with their effects summated. The major difference between determining horizontal and vertical stresses is that for the calculation of the horizontal stresses the summation by formula of the effects of a finite number of concentrated surface loads has been considered. However the Newmark chart and the effective weight of the soil is used to calculate the vertical stresses at each point in the soil.

The formulae derived (equations 5.4 and 5.5) orientate the σ_t and σ_r to a chosen σ_x, σ_y system for each of the concentrated loads of an elemental area. A finite number of point loads was considered because a mechanical form of integration was used. (see Figure 5.5)

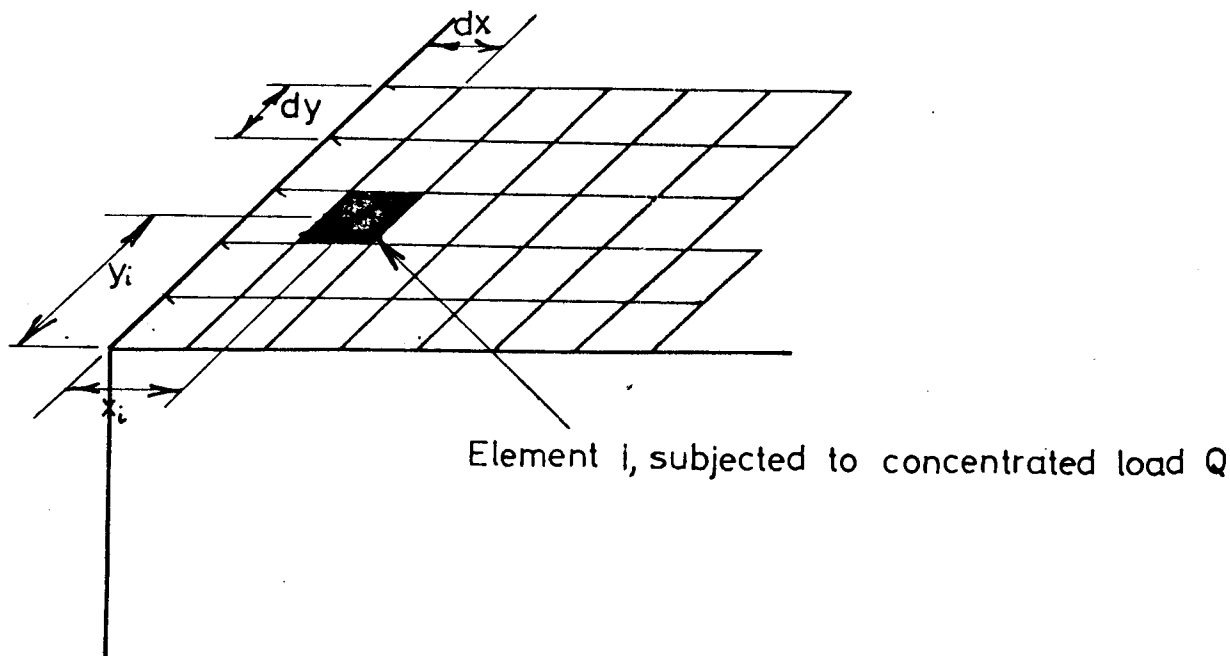


FIGURE 5.5 An Elemental Area a_i Subjected to Load Q

Although the footing sizes are 1 m, 2 m and 3 m square the dimensions of each element are 10 cm x 10 cm. The computer program used to determine values for σ_x and σ_y is shown after the next paragraph. At a point in the soil the program calculates values of σ_x and σ_y for each surface element. From the tabulated data (Appendix 1) stress distributions under odd shaped footings can be determined. (see Figure 5.6)

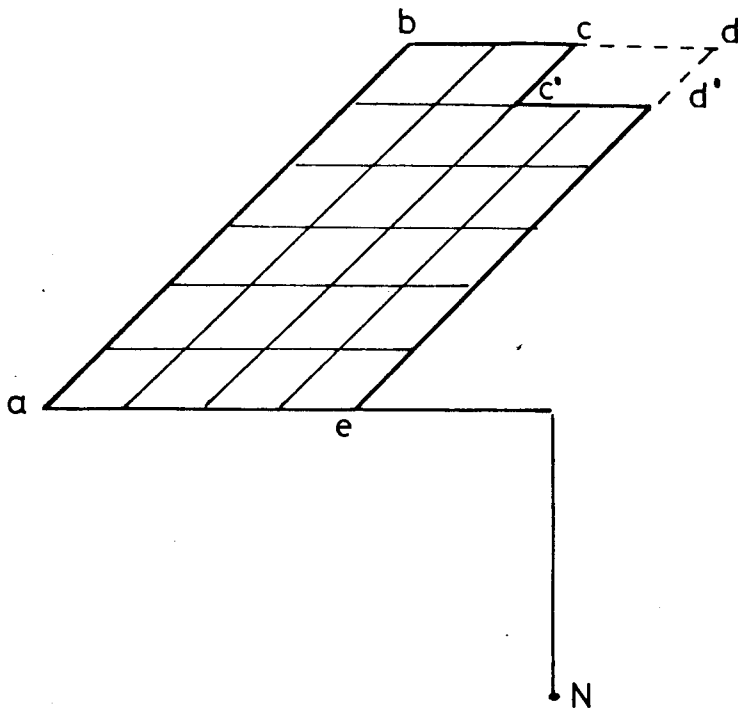


FIGURE 5.6 Stress at N = (Effect of elements of $abde$) -
 (Effects of elements of $cc'd'd$)

[illegible]

QHDG ERRERA HORIZONTAL STRESSES IN SOILS USING ELASTIC FORMALAE

ORFOR, IS

RFOR 5.106 09/13-14:23-

COU1	Q101:	DIMENSION Y(30),K(30),Z(12),COEFA(900),COEFA(900),COEFV(900),
COU2		,COEFV(900),ANSA(900),ANSJ(900),ANSV(900),ANSJ(900),BSTR(900),
COU3		,CSTR(900),USTR(900),ESTR(900),FSTR(900),GSTR(900),RA(30)

```
0004      U102:      WRITE (5,100)
0005      U103:      100 FORMAT (1H,4X,'Y(I)',6X,'X(J)',6X,'Z(K)',6X,'BSTR(N)',1X,
0006      , 'CSTR(N)',1X,'DSTR(N)',1X,'ESTR(N)',1X,'FSTR(N)',1X,'GSTR(N)')
```

0007	0104:	K=1
0008	0105:	Z(K)=0.1
0009	0106:	10 J=1

0010	0107:	L=1
0011	0116:	RA(J)=0.05

```
0012      0111:      9 101
0013      0112:      Y(1)=0.05
```

```
0014          0113:      M=1
0015          0114:      COEFA(M)=0
```

0016	0115:	CQEFB(H)=0
0017	0116:	CQEFV(H)=0

0018	0117:	CDEFW(M)=0
0019	0120:	H=1

0020	0121:	2 R(I)=(R(I
0021	0122:	AMSA(I)=IY

$$C022 \quad , \Delta Z(K) / (R(I) \cdot \Delta t + Z(K) \cdot \Delta t + Y(I) \cdot \Delta t) \cdot \Delta t, 5)$$
$$Z(K) \cdot ((R(I) \cdot 2 + Z(K) \cdot 2 + Y(I) \cdot 2) \cdot 0.5) + (R(I) \cdot 2 / (R(I) \cdot 2 + Y(I) \cdot 2 + Z(K) \cdot 2) \cdot (R(I) \cdot 2 + Z(K) \cdot 2 + Y(I) \cdot 2))$$
$$0027 \quad 2124: \quad \text{ANS}(Y(1) \cdot 0.2 + Z(K) \cdot (N(1) \cdot 0.2 + Z(K) \cdot 0.2 + Y(1) \cdot 0.2) \cdot 0.5))$$
$$Z(K) / ((R(1) \cdot \cdot 2 + Z(K) \cdot \cdot 2 + Y(1) \cdot \cdot 2) \cdot \cdot 2.5)$$

```

0027      U125:      ANSWER=(R(I)*2/(R(I)*2+Y(I)*2)/((R(I)*2+Z(K)*2+Y(I)*2+
0030      ,Z(K)*((R(I)*2+Z(K)*2+Y(I)*2)*D,5))+(Y(I)*2/(R(I)*2+Y(I)*2
0031      ,Z(K)*((R(I)*2+Z(K)*2+Y(I)*2)*D,5))

```

$$+Y(I)*2+Z(K)*(R(I)*2+Z(K)*2+Y(I)*2)*0.5))$$

0033	0126:	COEFB(M+1)=COEFB(M)+ANSB(L)
0034	0127:	COEFD(M+1)=COEFD(M)+ANSB(L)
0035	0128:	COEFC(M+1)=COEFC(M)+ANSB(L)

0035	0130:	COEFV(H+1)=COEFV(H)+ANSV(L)
0036	0131:	COEFH(H+1)=COEFH(H)+ANSW(L)
0037	0132:	

0537 0132: L=L+1

47	0038	0133:	H=H+1
	0039	0134:	GSTR(N)=COEFA(M)-0.34*COEFB(M)
49	0040	0135:	CSTR(N)=COEFA(M)-0.4*COEFB(M)
	0041	0136:	USTR(N)=COEFA(M)-0.5*COEFB(M)
51	0042	0137:	ESTR(N)=COEFV(M)-0.34*COEFW(M)
	0043	0140:	FSTR(N)=COEFV(M)-0.4*COEFW(M)
53	0044	0141:	GSTR(N)=COEFV(M)-0.5*COEFW(M)
	0045	0142:	PRINT 200,(Y(I),RA(J),Z(K),USTR(N),CSTR(N),USTR(N),ESTR(N),
55	0046		FSTR(N),GSTR(N))
	0047	0143:	200 FURMAT (9(F10.3))
57	0048	0144:	N=N+1
	0049	0145:	IF (I-J) 4,3,3
59	0050	0146:	4 Y(I+1)=Y(I)+0.1
	0051	0147:	I=I+1
61	0052	0150:	GO TO 2,
	0053	0151:	3 IF (J-30) 5,6,6
63	0054	0152:	5 RA(J+1)=RA(J)+0.1
65			
67	0055	0153:	J=J+1
69	0056	0154:	GO TO 4
71	0057	0155:	6 IF (K-6) 80,81,82
	0058	0156:	80 Z(K+1)=Z(K)+0.1
73	0059	0157:	K=K+1
75	0060	0160:	GO TO 10
77	0061	0161:	81 Z(K+1)=Z(K)+0.4
79	0062	0162:	K=K+1
81	0063	0163:	GO TO 10
83	0064	0164:	82 Z(K+1)=Z(K)+1.0
85	0065	0165:	K=K+1
87	0066	0166:	IF (K-12) 10,10,7
89	0067	0167:	7 STOP
91	0068	0170:	END
93			
95			
97			
99			
101			
103			
105			
107			
109			
111			
113			
115			
117			
119			
121			
123			
125			
127			
129			

	Y(I)	RA(J)	Z(K)	BSTR(N)	CSTR(N)	DSTR(N)	ESTR(N)	FSTR(N)	GSTR(N)
3									
5	.050	.050	.100	12.410	11.233	9.538	28.441	26.927	24.402
	.150	.050	.100	19.045	18.578	16.466	36.514	34.754	31.821
	.250	.050	.100	22.218	20.098	18.627	38.930	37.106	34.066
	.350	.050	.100	23.190	21.848	19.612	39.905	38.056	34.975
9	.450	.050	.100	23.670	22.318	20.065	40.384	38.523	35.422
	.550	.050	.100	23.940	22.582	20.319	40.652	38.785	35.673
11	.650	.050	.100	24.106	22.744	20.475	40.817	38.946	35.828
	.750	.050	.100	24.215	22.851	20.577	40.925	39.052	35.929
13	.850	.050	.100	24.290	22.924	20.648	41.000	39.125	35.999
	.950	.050	.100	24.344	22.977	20.698	41.054	39.177	36.049
15	1.050	.050	.100	24.384	23.017	20.737	41.094	39.216	36.087
	1.150	.050	.100	24.415	23.046	20.766	41.124	39.246	36.116
17	1.250	.050	.100	24.439	23.070	20.788	41.148	39.269	36.138
	1.350	.050	.100	24.458	23.088	20.806	41.167	39.288	36.156
19	1.450	.050	.100	24.473	23.103	20.821	41.182	39.303	36.170
	1.550	.050	.100	24.486	23.116	20.833	41.195	39.315	36.182
21	1.650	.050	.100	24.496	23.126	20.842	41.205	39.325	36.191
	1.750	.050	.100	24.505	23.135	20.851	41.214	39.334	36.200
23	1.850	.050	.100	24.512	23.142	20.858	41.221	39.341	36.207
	1.950	.050	.100	24.519	23.148	20.864	41.228	39.347	36.212
25	2.050	.050	.100	24.524	23.153	20.869	41.233	39.352	36.218
	2.150	.050	.100	24.529	23.158	20.873	41.238	39.357	36.222
27	2.250	.050	.100	24.533	23.162	20.877	41.242	39.361	36.226
	2.350	.050	.100	24.537	23.165	20.880	41.246	39.364	36.229
29	2.450	.050	.100	24.540	23.169	20.883	41.249	39.368	36.232
	2.550	.050	.100	24.543	23.171	20.886	41.252	39.370	36.235
31	2.650	.050	.100	24.545	23.174	20.888	41.254	39.373	36.237
	2.750	.050	.100	24.547	23.176	20.891	41.256	39.375	36.239
33	2.850	.050	.100	24.549	23.178	20.892	41.258	39.377	36.241
	2.950	.050	.100	24.551	23.180	20.894	41.260	39.379	36.243
35	.050	.150	.100	3.390	3.502	3.689	22.224	21.265	19.721
	.150	.150	.100	7.452	7.569	7.763	28.696	27.475	25.440
37	.250	.150	.100	9.306	9.414	9.593	30.793	29.485	27.305
	.350	.150	.100	10.173	10.273	10.441	31.672	30.330	28.093
39	.450	.150	.100	10.626	10.722	10.882	32.114	30.756	28.492
	.550	.150	.100	10.808	10.981	11.136	32.365	30.999	28.720
41	.650	.150	.100	11.052	11.193	11.294	32.521	31.149	28.862
	.750	.150	.100	11.160	11.250	11.398	32.624	31.249	28.957
43	.850	.150	.100	11.236	11.324	11.471	32.696	31.318	29.022
	.950	.150	.100	11.290	11.377	11.523	32.748	31.369	29.070
45	1.050	.150	.100	11.330	11.417	11.562	32.786	31.406	29.106
	1.150	.150	.100	11.361	11.447	11.591	32.816	31.435	29.133
47	1.250	.150	.100	11.385	11.471	11.614	32.839	31.457	29.154
	1.350	.150	.100	11.405	11.490	11.633	32.857	31.475	29.171
49	1.450	.150	.100	11.420	11.505	11.647	32.872	31.490	29.185
	1.550	.150	.100	11.433	11.518	11.659	32.885	31.502	29.196
51	1.650	.150	.100	11.443	11.528	11.667	32.895	31.511	29.206
	1.750	.150	.100	11.452	11.537	11.678	32.903	31.520	29.214
53	1.850	.150	.100	11.460	11.544	11.685	32.911	31.527	29.220
	1.950	.150	.100	11.466	11.550	11.691	32.917	31.533	29.226
55	2.050	.150	.100	11.472	11.556	11.696	32.922	31.538	29.231
	2.150	.150	.100	11.476	11.561	11.701	32.927	31.542	29.235
57	2.250	.150	.100	11.481	11.565	11.705	32.931	31.546	29.239
	2.350	.150	.100	11.484	11.568	11.708	32.934	31.550	29.243

From the computer program results the horizontal stresses at various depths under the centre of the footing have been computed for various sizes of footings. The results are tabulated in Tables 5.1 to 5.4. The stress paths for these footings have been drawn. (see Figures 5.7 to 5.10). A single curve of Z/B against average horizontal stress σ_h can be drawn. (see Figure 5.11). The effect of μ on horizontal stress distributions is shown in Figure 5.12. The results obtained compared with those shown in Lambe and Whitman (Ref. 2), see Figures 5.13 to 5.16.

5.4 Conclusion

The power of the stress path method is illustrated. One can see from the stress paths that

- a) μ and therefore K_0 definitely have a large effect on the horizontal stress distribution within a soil mass
- b) Smaller footings are much more susceptible to inaccuracies when using settlement prediction methods in which the average increments in horizontal stresses are estimated from vertical stresses by using the K_0 factor (i.e. instead of calculating directly from Boussinesq type theory). The reason for this greater inaccuracy for smaller footings is that the stress paths deviate proportionally more from the K_0 line than in the case of the larger footings. Whenever results with apparent^{ly} good agreement between predictions and measurements are quoted by other workers these are for large footings where the actual average stress paths due to surface loads are approximately on the K_0 line.
- c) The effect of moisture content on collapsing soils can be represented by a 45° line on the $p - q$ diagram.. When considering small footings (e.g. less than 0,5 m by 0,5 m) it might be advisable not to use the K_0 approximation. For larger footings for important structures where accurate settlement must be predicted the K_0 approximation might also be unsuitable.

For collapsing soils the estimated initial settlement based on K_0 might be inaccurate, but the collapse settlement taking into account the change in K_0 due to changes in water content be such that the combined initial and collapse settlement should be accurately predicted. All settlements calculated using the K_0 theory should be less than that of the actual field settlement because in natural foundation soils, horizontal yielding can take place. This is also substantiated by the stress paths (see Figure 5.7 to 5.10) and the knowledge that horizontal deformations do in fact occur.

FIGURE 5.7 Stress Paths for Points Under the Centre of a 3m x 3m Footing (deepwater table)

FIGURE 5.7 Stress Paths for Points Under the Centre of a 3m x 3m Footing (Deep water table)

$q_w = 100 \text{ kN/m}^2$ (gross loading at founding level)

$q_{wn} = 80 \text{ kN/m}^2$ (nett loading, taking into account excavated material)

$K_o = 0,5$

Unit weight of soil = 20 kN/m^3

Founding depth = 1 m

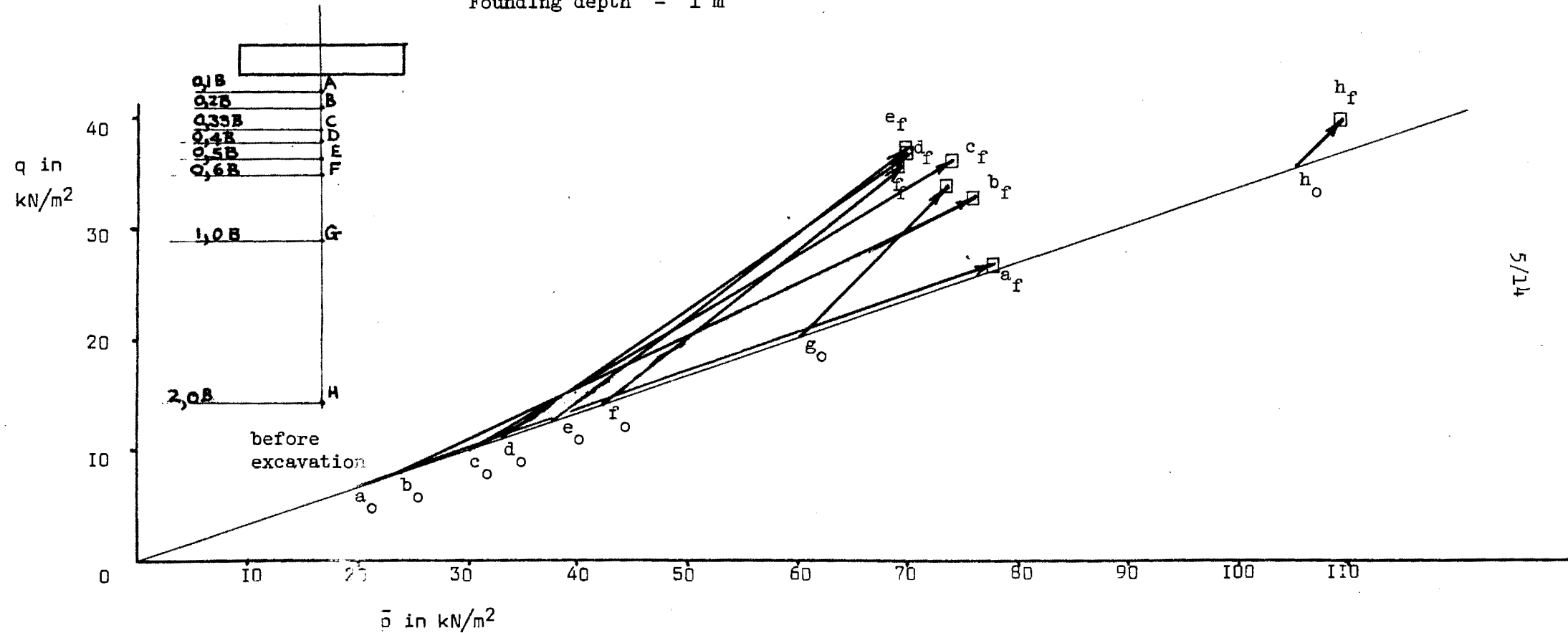


FIGURE 5.8 Stress Paths for Points Under the Centre of a 10m x 10m Footing (Fine sand, deep water table)

$$q_w = 120 \text{ kN/m}^2$$

$$q_{wn} = 100 \text{ kN/m}^2$$

$$K_o = 0,5$$

$$\text{Unit weight of soil} = 20 \text{ kN/m}^3$$

$$\text{Founding depth} = 1 \text{ m}$$

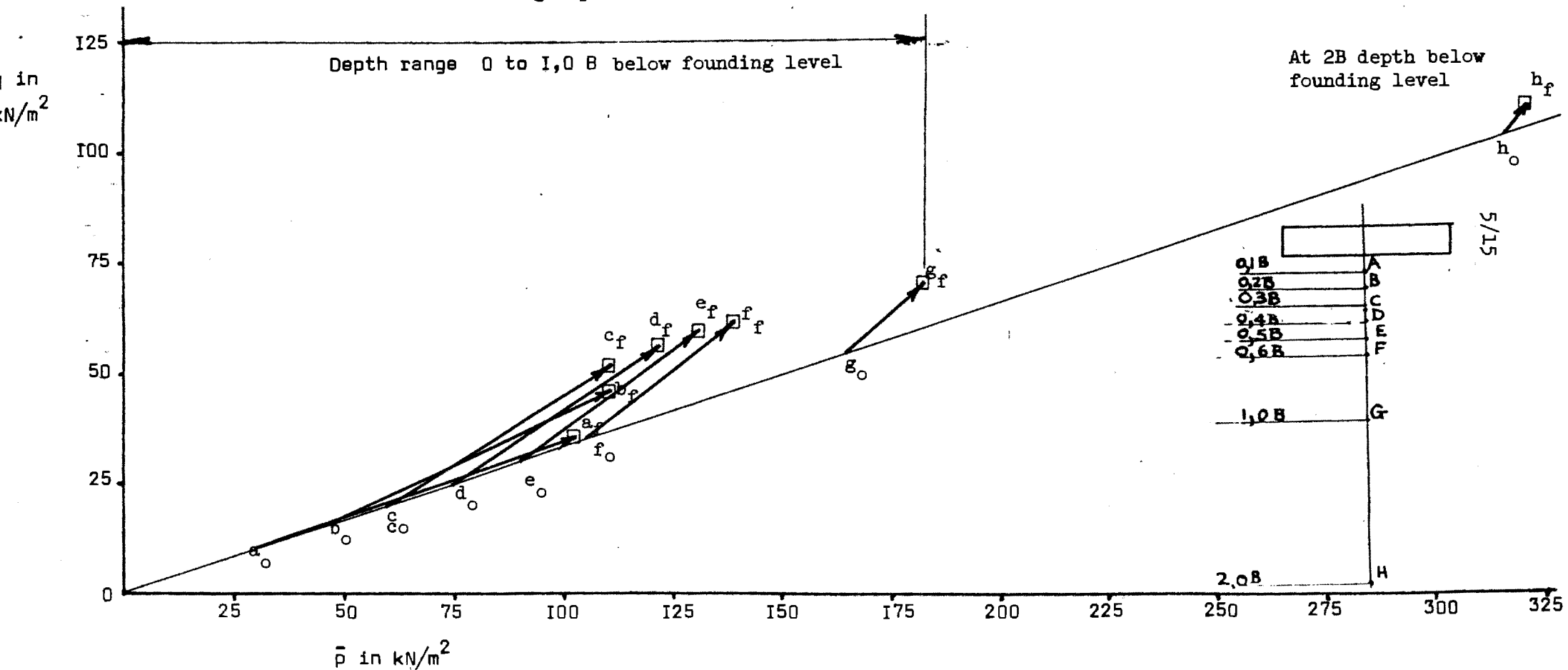


FIGURE 5.9 Stress Paths for Points Under the Centre of a 10m x 10m Footing (Fine sand, deep water table)

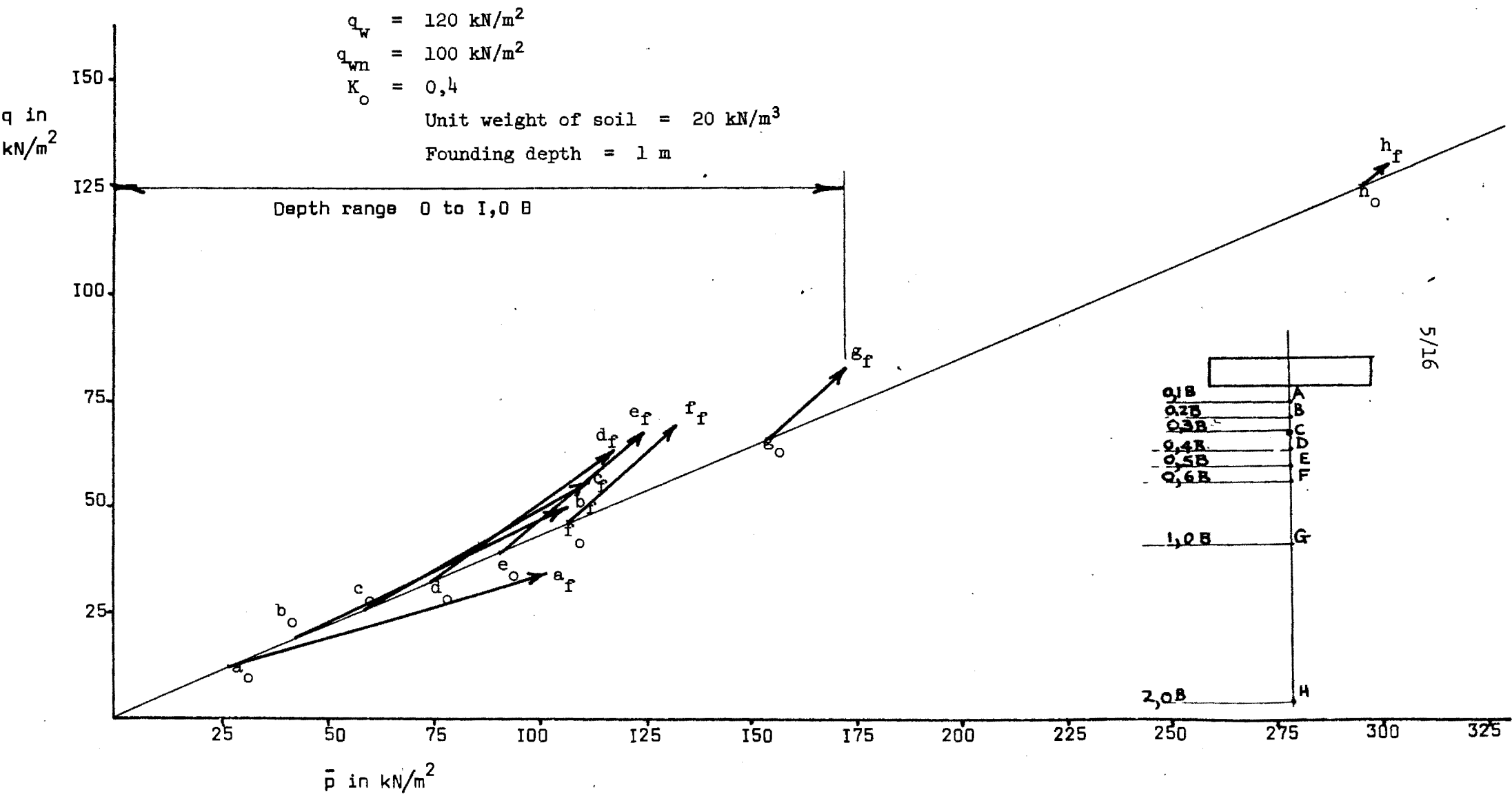


FIGURE 5.10 Stress Paths for Points Under the Centre of a 20m x 20m Footing (Fine sand, deep water table)

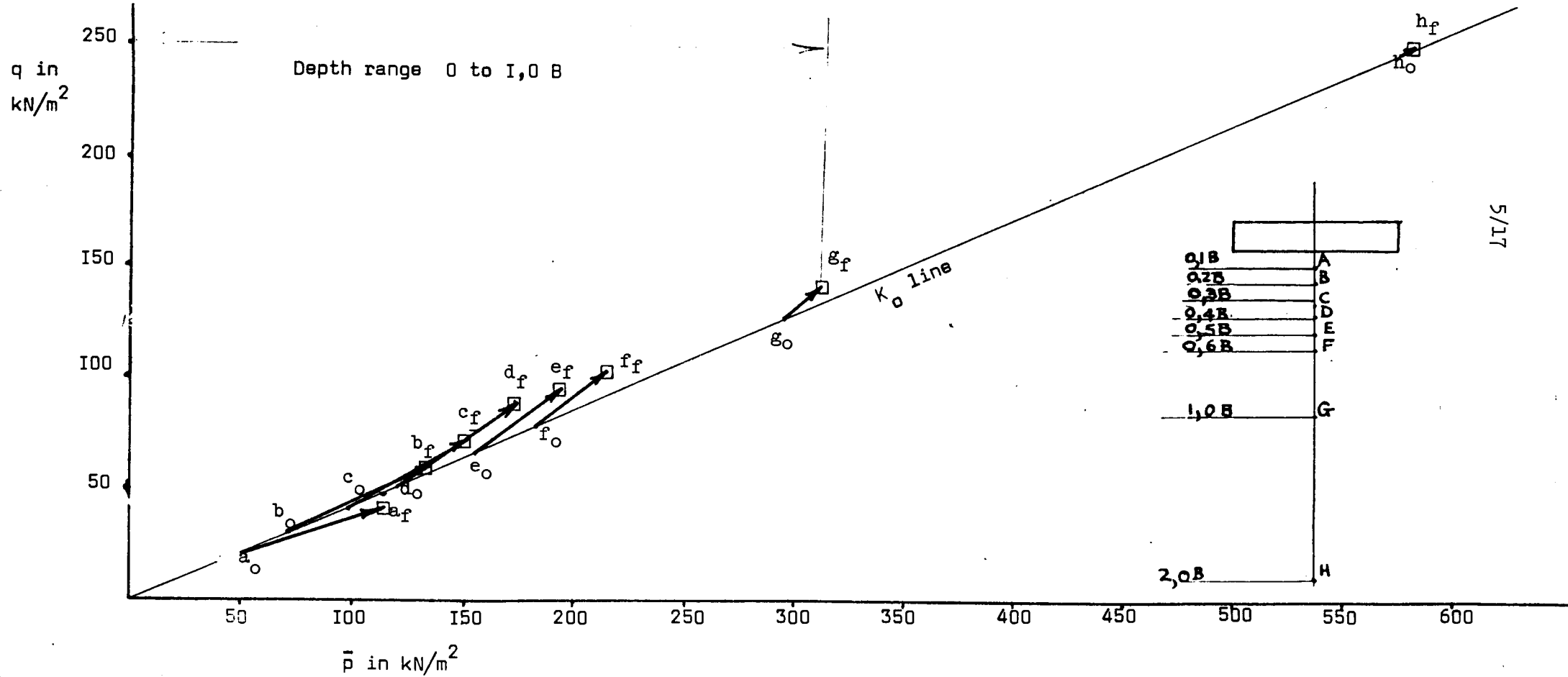
$$q_w = 120 \text{ kN/m}^2$$

$$q_{wn} = 100 \text{ kN/m}^2$$

$$K_o = 0,4$$

$$\text{Unit weight of soil} = 20 \text{ kN/m}^3$$

$$\text{Founding depth} = 1 \text{ m}$$



Change in Stress due to Nett Surface Loading

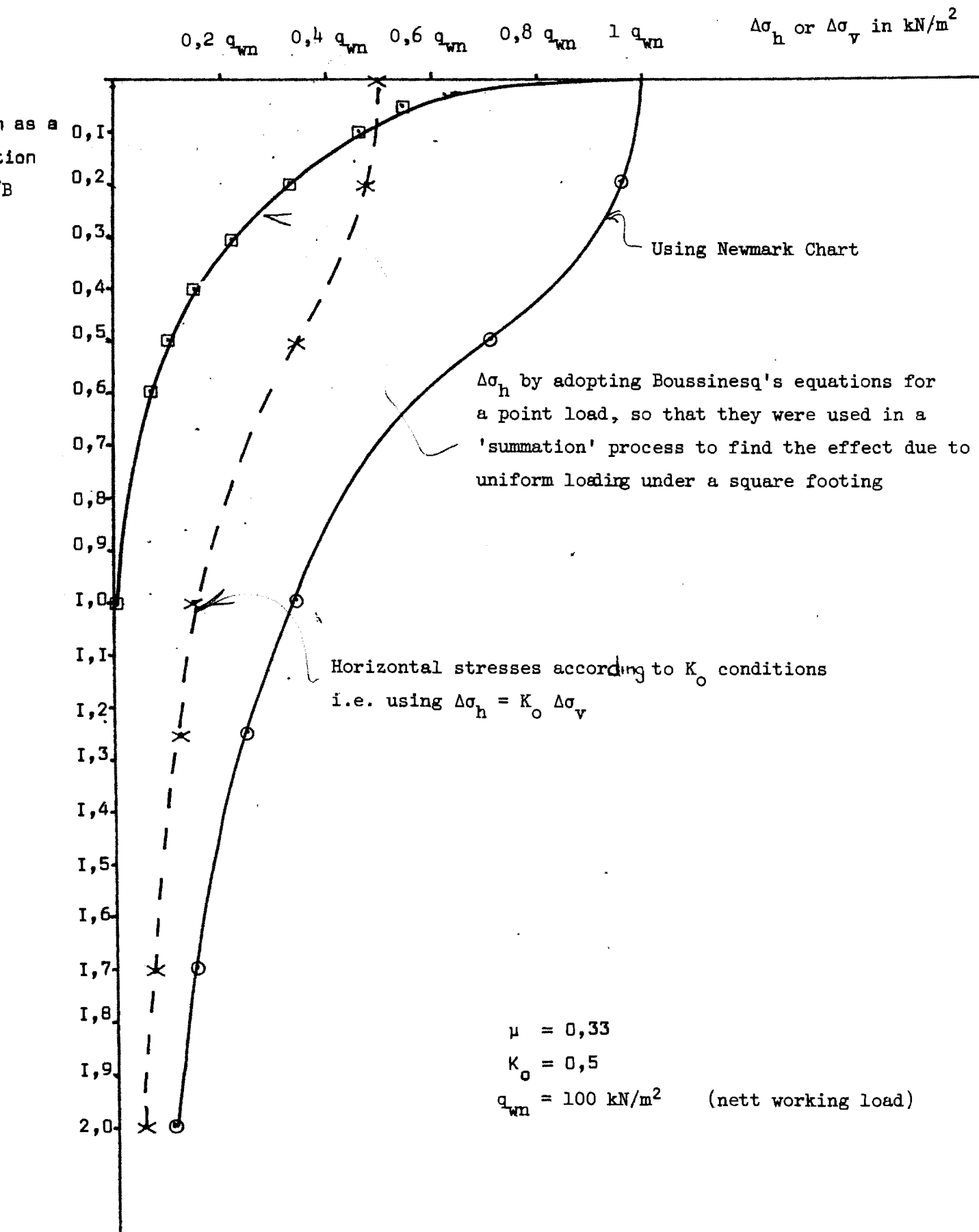


FIGURE 5.11 Stresses under Centre of a Square Footing (width B)
(assumed uniform pressure between footing and soil)

Increase in Average Horizontal Stresses Under Centre of Flexible Footing

$\Delta\sigma_3$ in kN/m^2

0,1 q_{wn} 0,2 q_{wn} 0,3 q_{wn} 0,4 q_{wn} 0,5 q_{wn} 0,6 q_{wn} 0,7 q_{wn} 0,8 q_{wn}

Depth as a
function
Z/B

0,1
0,2
0,3
0,4
0,5
0,6
0,7
0,8
0,9
1,0
1,1
1,2
1,3
1,4
1,5
1,6
1,7
1,8
1,9
2,0

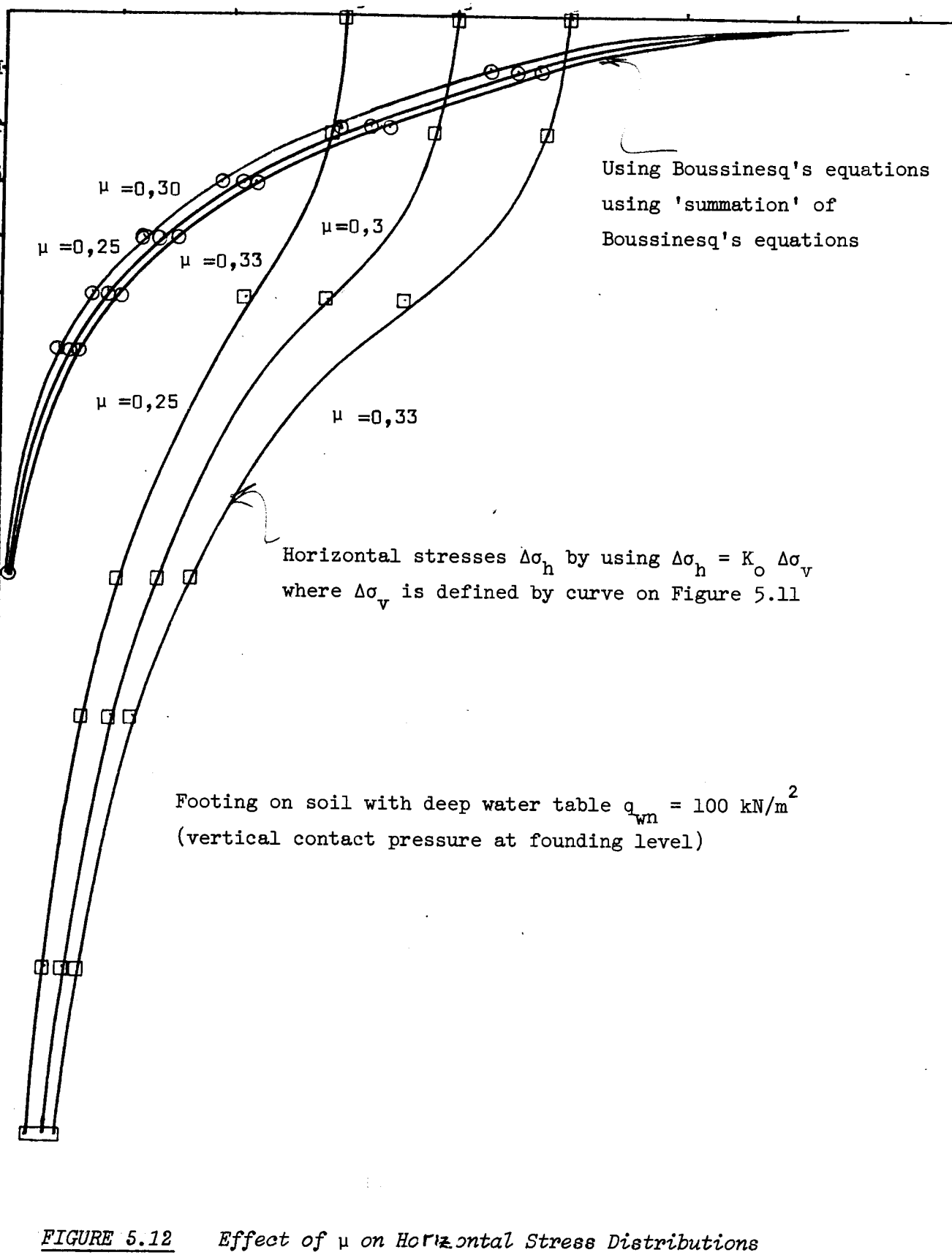


FIGURE 5.12

Effect of μ on Horizontal Stress Distributions
(on vertical centre line under square footing)

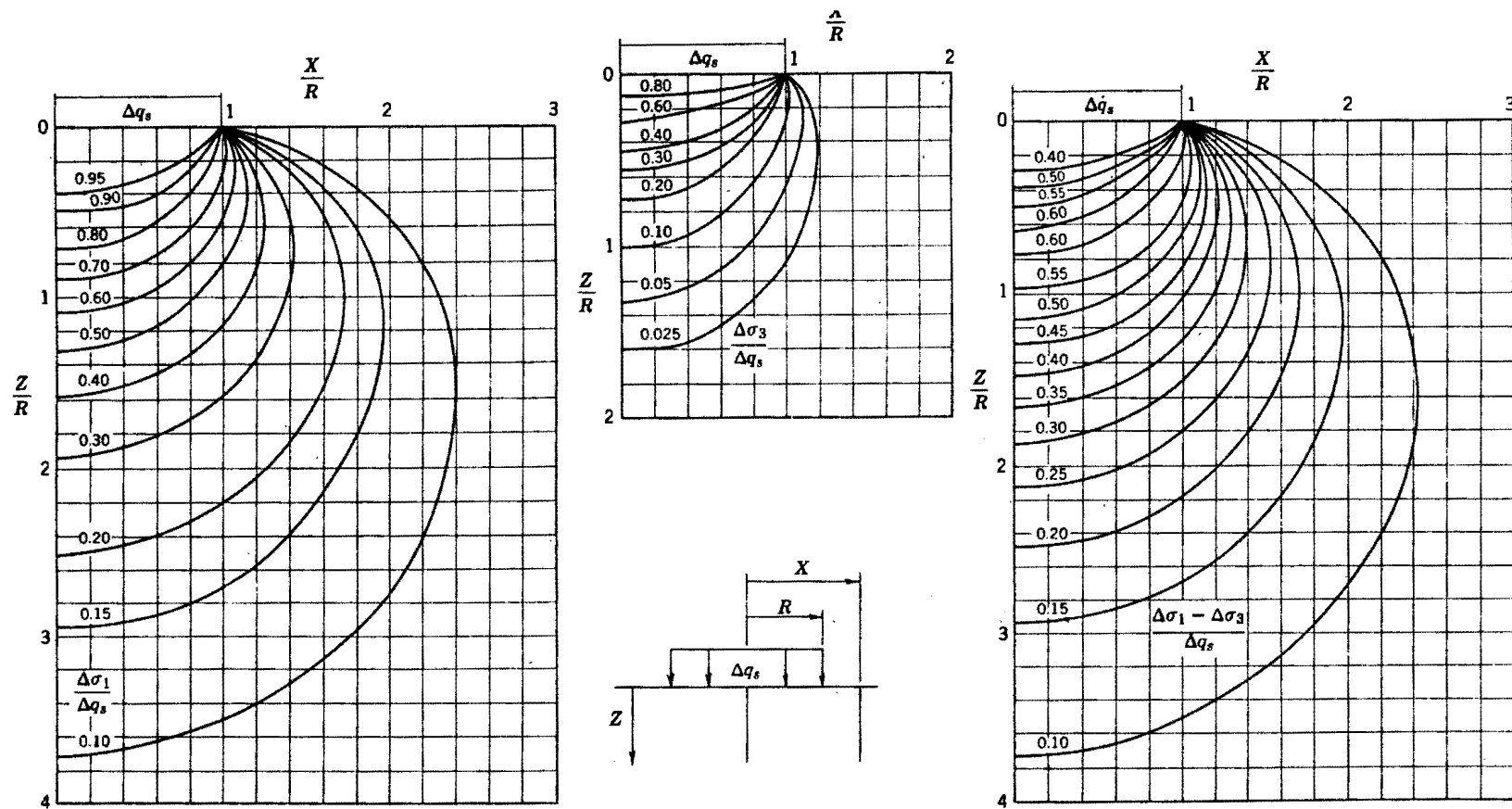


FIGURE 5.13 Stress Distributions under a Circular Footing (Lambe and Whitman, Ref. 2)

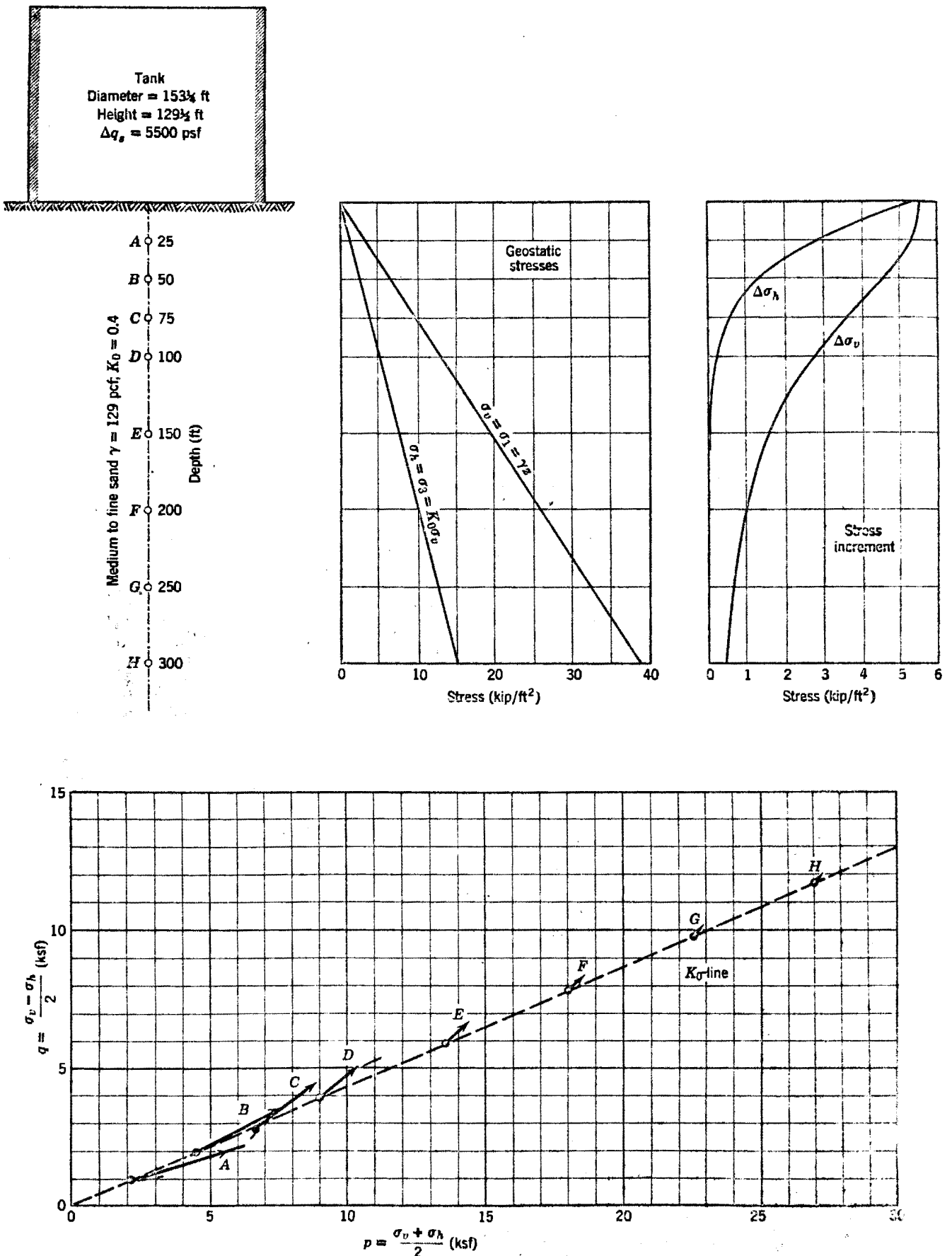


FIGURE 5.14 Stress Distributions and Associated Stress Paths under a Tank (Lambe and Whitman, Ref. 2)

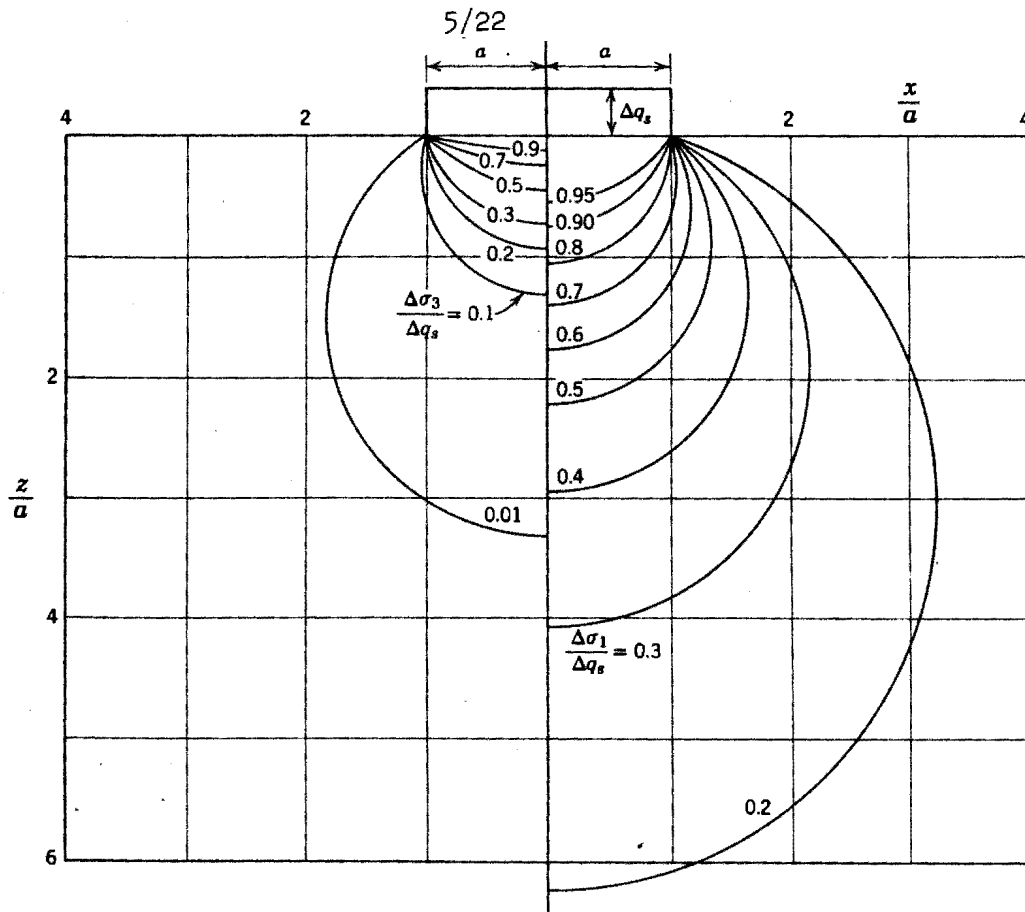


FIGURE 5.15 Stresses Under a Strip Load (Lambe & Whitman, Ref. 2)

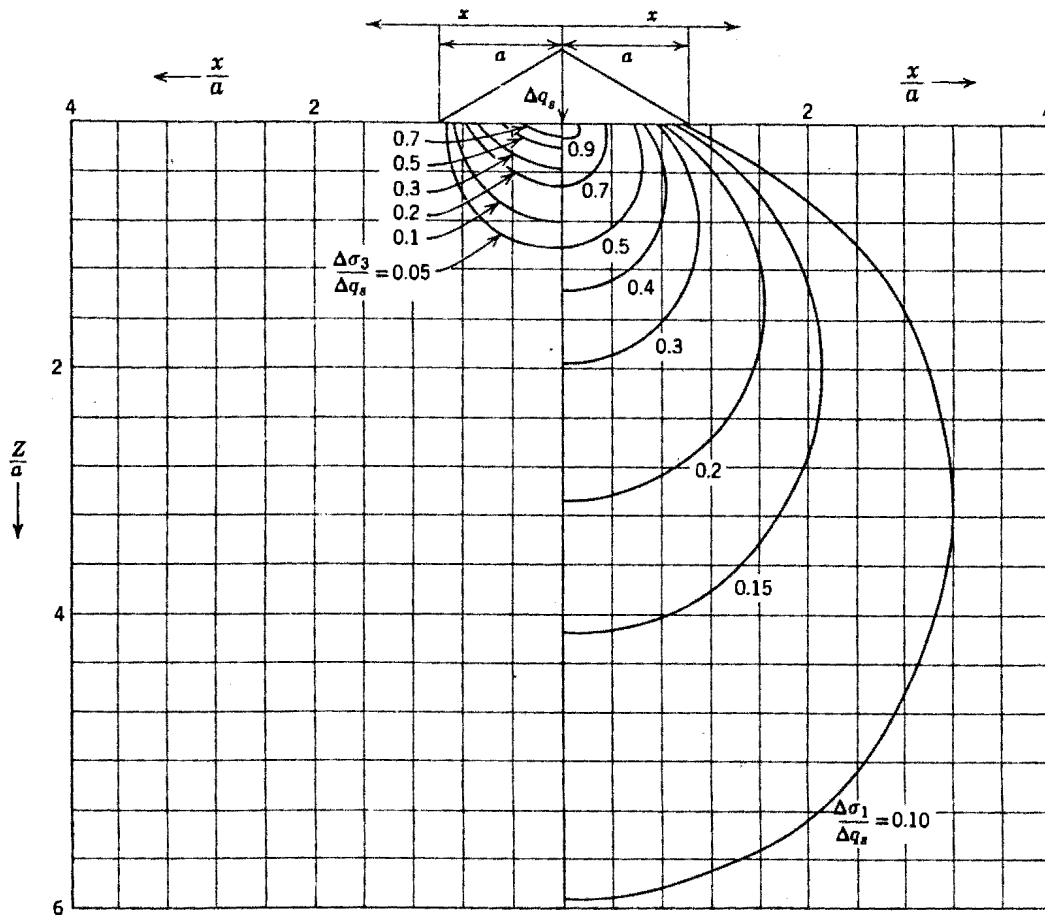


FIGURE 5.16 Stresses Under a Triangular Strip Load (Lamb & Whitman, Ref. 2)

TABLE 5.1 *Table of data for drawing actual stress paths under the centre of a 3 m x 3 m footing.*
($K_0 = 0,5$ Founding depth = 1 m)

Depth below footing		Initial (kN/m^2)				(kN/m^2)		(kN/m^2) Final	
Z/B	metres	$\bar{\sigma}_1$	$\bar{\sigma}_3$	q	\bar{p}	$\Delta\bar{\sigma}_1$	$\Delta\bar{\sigma}_3$	q	\bar{p}
0,1	0,3	26	13	6,5	19,5	78	38	26,5	77,5
0,2	0,6	32	16	8,0	24,0	77	27	33,0	76,0
0,3	1,0	40	20	10,0	30,0	70	18	36,0	74,0
0,4	1,2	44	22	11,0	33,0	63	12	36,5	70,5
0,5	1,5	50	25	12,5	37,5	57	8	37,0	70,0
0,6	1,8	56	28	14,0	42,0	49	6	35,5	69,5
1,0	3,0	80	40	20,0	60,0	27,5	0,5	33,8	73,8
2,0	6,0	140	70	35,0	105,0	9	0	39,5	109,5

TABLE 5.2 *Table of data for drawing actual stress paths under the centre of a 10 m x 10 m footing.*
($K_0 = 0,5$ Founding depth = 1 m)

Depth below footing		Initial (kN/m^2)				(kN/m^2)		(kN/m^2) Final	
Z/B	metres	$\bar{\sigma}_1$	$\bar{\sigma}_3$	q	\bar{p}	$\Delta\bar{\sigma}_1$	$\Delta\bar{\sigma}_3$	q	\bar{p}
0,1	1	40	20	10	30	98	47	35,5	102,5
0,2	2	60	30	15	45	96	34	46,0	110,0
0,3	3	80	40	20	60	87	22	52,5	116,5
0,4	4	100	50	25	75	79	15	57,0	122,0
0,5	5	120	60	30	90	71	10	60,5	130,5
0,6	6	140	70	35	105	61	6	62,5	138,5
1,0	10	220	110	55	165	34	1	71,5	182,5
2,0	20	420	210	105	315	11	0	110,5	320,5

TABLE 5.3 *Table of data for drawing actual stress paths under the centre of a 10 m x 10 m footing.*
($K_0 = 0,4$ Founding depth = 1 m)

Depth below footing		Initial (kN/m^2)				(kN/m^2)		(kN/m^2)	
Z/B	metres	$\bar{\sigma}_1$	$\bar{\sigma}_h$	q	\bar{p}	$\Delta\bar{\sigma}_1$	$\Delta\bar{\sigma}_h$	Final	
								q	\bar{p}
0,1	1	40	16	12	26	98	45	38,5	99,5
0,2	2	60	24	18	42	96	32	50,0	106,0
0,3	3	80	32	24	58	87	21	57,0	110,0
0,4	4	100	40	30	74	79	14	62,5	116,5
0,5	5	120	48	36	90	71	9	67,0	124,0
0,6	6	140	56	42	106	61	6	69,5	131,5
1,0	10	220	88	66	154	34	1	82,5	171,5
2,0	20	420	168	126	294	11	0	131,5	299,5

TABLE 5.4
TABLE 5.4 *Table of data for drawing actual stress paths under the centre of a 20 m x 20 m footing.*
($K_0 = 0,4$ Founding depth = 1 m)

Depth below footing		Initial (kN/m^2)				(kN/m^2)		(kN/m^2)	
Z/B	metres	$\bar{\sigma}_1$	$\bar{\sigma}_h$	q	\bar{p}	$\Delta\bar{\sigma}_1$	$\Delta\bar{\sigma}_h$	Final	
								q	\bar{p}
0,1	2	60	24	18	42	98	45	44,5	113,5
0,2	4	100	40	30	70	96	32	62,0	134,0
0,3	6	140	56	42	98	87	21	75,0	152,0
0,4	8	180	72	54	126	79	14	86,5	172,5
0,5	10	220	88	66	154	71	9	97,0	194,0
0,6	12	260	104	78	182	61	6	105,5	215,5
1,0	20	420	168	126	294	34	1	142,5	311,5
2,0	40	820	328	246	574	11	0	251,5	579,5

CHAPTER 6

SETTLEMENT PREDICTION

6.1 Introduction to the problems of settlement prediction

Assumptions used in settlement predictions must be accurately defined for each and every case. Numerous factors affect settlement prediction. These influences vary with soil type and loading systems.

6.2 Settlement

Settlement describes the vertical deformation that occurs when a loading system is imposed on a soil mass. The vertical deformation results in a denser packing of soil solids in a localized area. This localized area is mainly within a bulb of pressure extending down to at least $1,5 B$ or $2B$ (see Chapter 4).

For any settlement problem, points at which deformation and stress variations will occur, must be chosen. These points must be carefully selected so as to obtain an accurate settlement prediction. There are two approaches for the selection of these points.

The first method (see Figure 6.1) considers a number of points on different planes under the loaded area. For very accurate results a point under the centre of the footing and points under the centres of the edges of the footing should suffice. The number of horizontal planes considered, could be related to the breadth of the footing and the variability of the soil with depth.

The other method is to define an average point and to examine the behaviour of this single point. As the mass implies, the point should behave as an average of the points within the appropriate area of the soil mass. The position of the average point is defined as a function of B (see Figure 6.2(a) and 6.2(b)). The strain at this 'average point' is assumed to act over an effective compressible depth D (Sparks, Ref. 52). D is dependent upon the shape and size of the footing considered. This method is limited to soil masses which are homogeneous to a depth D .

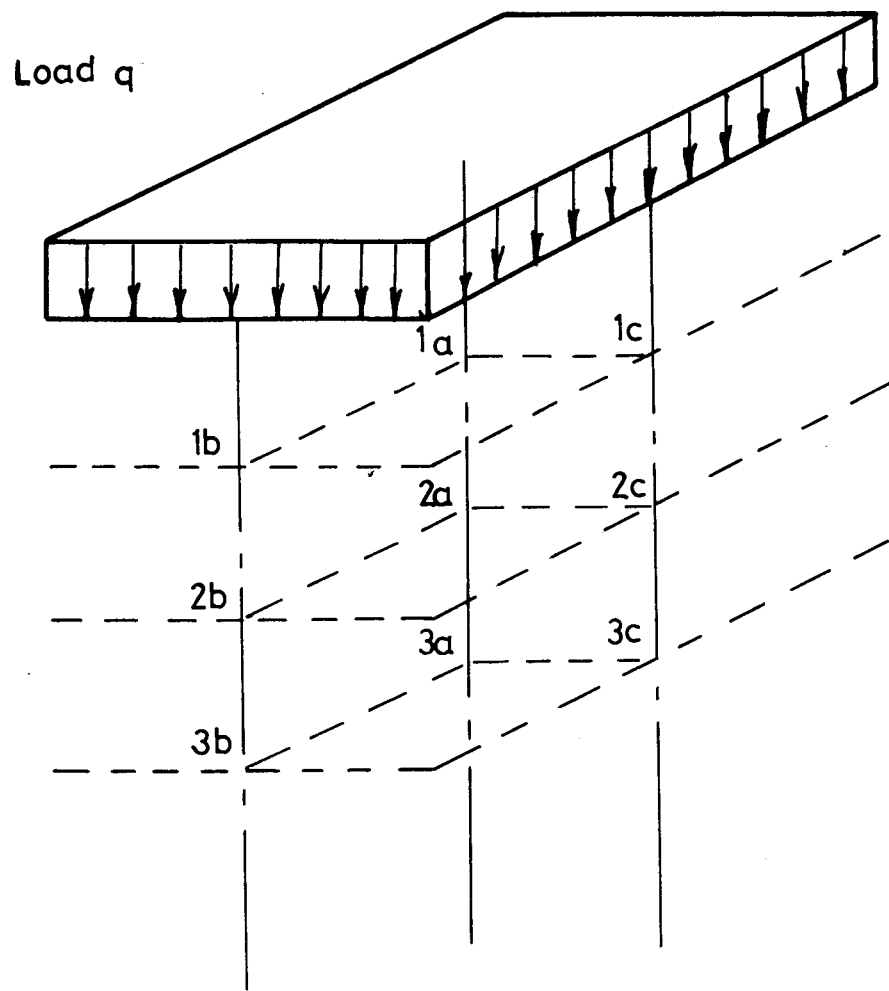


FIGURE 6.1 *Grid Type Layout for Choosing Points used in Settlement Prediction*

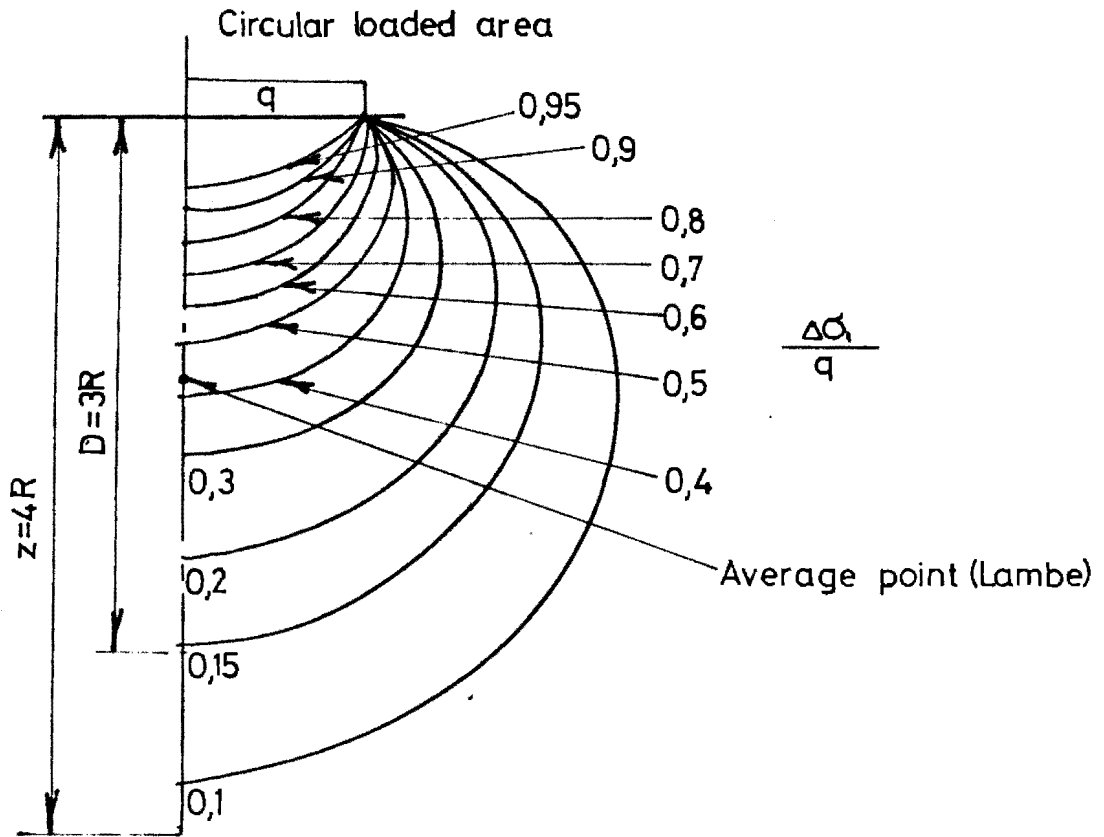


FIGURE 6.2(a) Definition of the Average Point for a Circular Footing

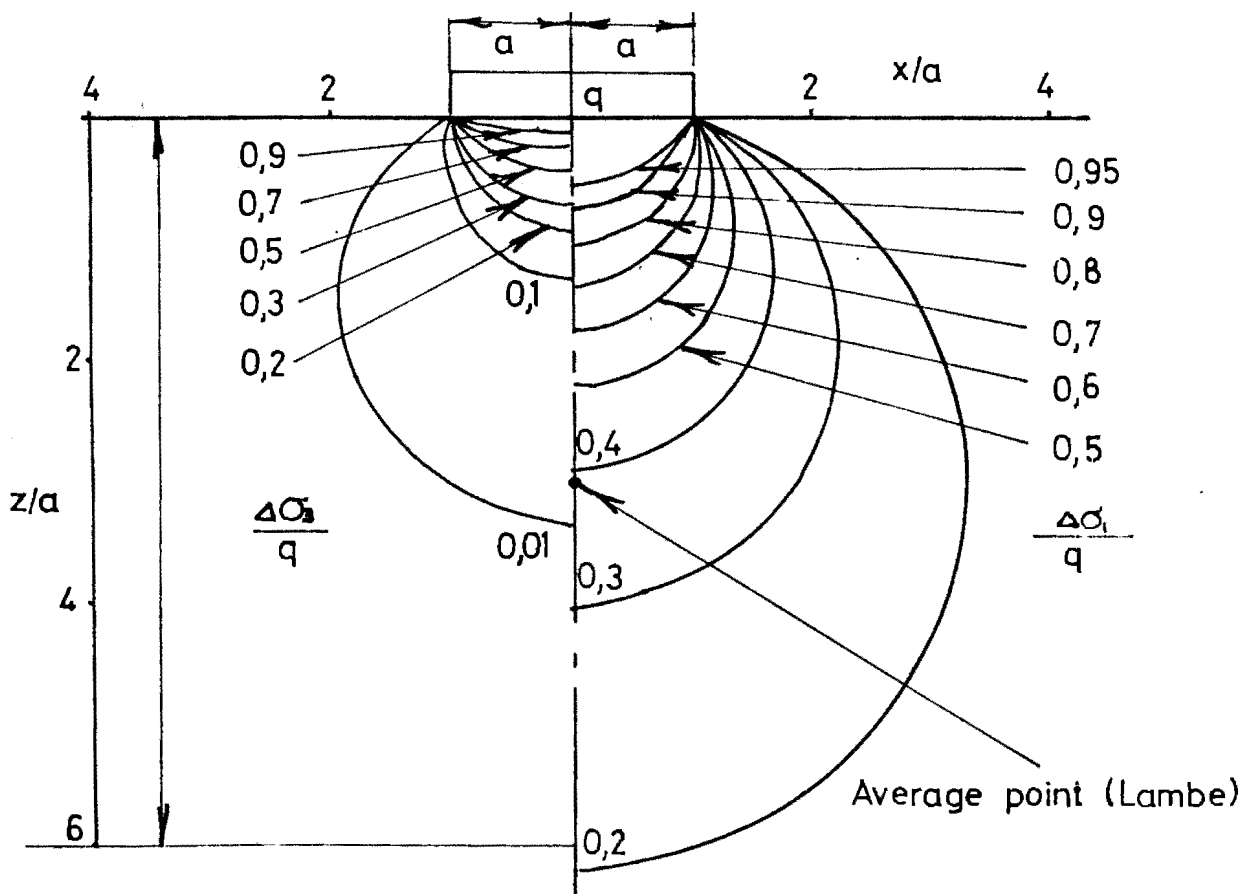


FIGURE 6.2(b) Definition of the Average Point for a Strip Footing

The cohesionless soils will deform immediately due to the loading of a localized area. Cohesive soils display a delayed consolidation characteristic. Consolidation is generally defined as the dissipation of excess water pressure with time.

The time of dissipation of excess water pressure should be a function of the volume of water which has to be forced out of the soil mass and the ease with which it can flow through the soil mass. This volume of water must in turn be a function of the stress change, the compressibility of the soil skeleton and the volume of the soil subjected to the stress change. The time should also be proportional to the velocity of flow.

Equation 6.1 can be used to determine the time for a certain percentage of the consolidation to take place.

$$t = \frac{H^2 T_v}{C_v} \quad (6.1)$$

where

- t = time for a percentage of the consolidation process to take place
- C_v = coefficient of consolidation
- H = thickness of the soil mass or ^{maximum} distance to a drainage surface
- T_v = time factor

From the formula it is evident that the time for a percentage of the consolidation to take place will:

1. Increase with increasing compressibility of the soil skeleton
2. Decrease with increasing permeability
3. Increase rapidly with increasing distance to drainage layer (H^2)
4. Not depend on the magnitude of the stress change. This magnitude of this stress change will only effect the magnitude of the settlement not the percentage of the final settlement

Equilibrium is finally established when the water pressure is equal to the static water pressure due to the water table. At this stage the effective vertical stress within the soil mass is equal to the initial overburden effective stress plus the increment due to the loading system.

Below are graphical representation of time settlement curves for a saturated clay and partly saturated clay.

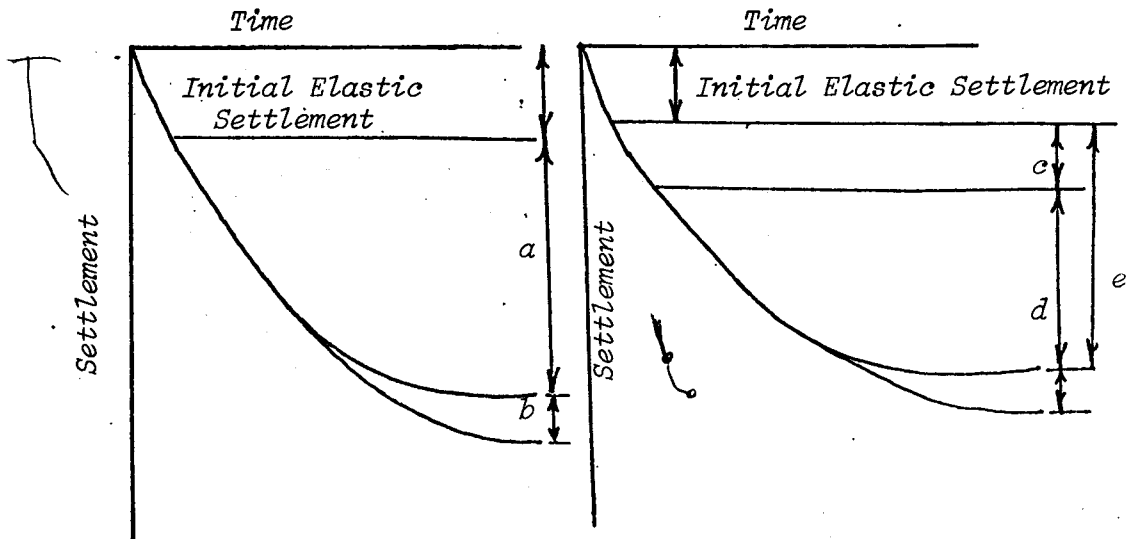


FIGURE 6.3 Saturated Clay

Partly Saturated Clay

- a* - Hydrodynamic consolidation settlement (obtained from consolidometer test)
- b* - Secondary consolidation due to time creep effects under constant load
- c* - Initial compression of air voids due to Boyle's law and Henry's law
- d* - Hydrodynamic consolidation due to outward movement of the water and air within the voids of the clay
- e* - Obtainable from a consolidometer test

6.3 Settlement prediction

The movements with which the engineer is concerned are the maximum vertical settlement (S) the maximum differential settlement (Δ) and the maximum angular distortion δ/L (see Figure 6.4). The determining settlement is the settlement which causes the maximum amount of distortion to a part of the building only. The maximum angular distortion (δ/L) should be limited to $\frac{1}{300}$ for buildings with interior panels and walls and $\frac{1}{150}$ for buildings without interior partitions or brick walls.

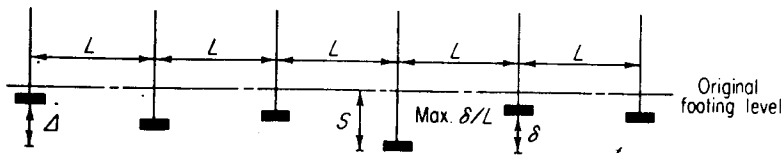
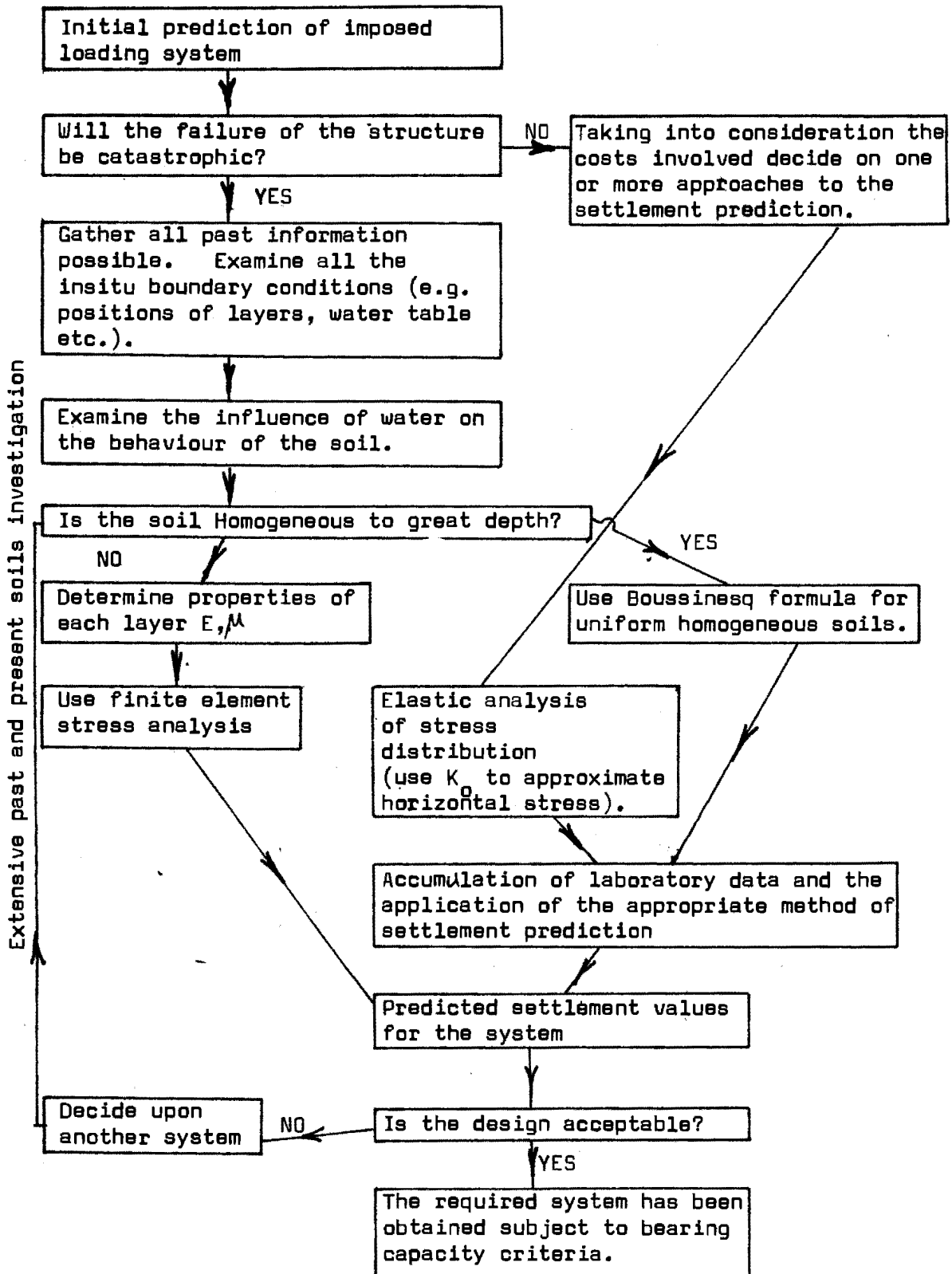


FIGURE 6.4 *Important Settlement Values*

Settlement prediction is not only concerned with stress variation. The techniques of theoretical soil mechanics involve the assumption that the site conditions approximate to the theoretical model (e.g. rock boundaries etc). If these assumptions are reasonable other additional influences on settlement prediction should be considered (e.g. stress history, rate of loading, variation of w_c etc).

The final cost of the structure will also influence settlement prediction as a detailed soil investigation is a costly process. A flow chart, describing the process involved from the initial design stage of the structure and foundation system to the final predicted settlements and design of the system, is shown.

The first column in the following table is based on Lambe and Whitman, Ref. 2.



Consequences of soil being a particulate system	Influences on settlement prediction
<p>The deformation of a mass of soil is controlled by the interactions between individual particles especially by sliding between particles</p> <p>Soil is inherently multi-phase, and the constituents of the pore phase will influence the nature of the mineral surfaces and hence the process of force transmission at the particle contacts</p> <p>Water can flow through the soil and thus interact with the mineral skeleton. This will alter the magnitude of forces at the contacts between particles, and influence the compression and shear resistance of the soil</p> <p>When the load applied to a soil is suddenly changed, this change is carried jointly by the pore fluid and by the mineral skeleton. The change in pore pressure will cause water to move through the soil, hence the properties of the soil will change with time</p>	<p>The plot of stress-strain is not a straight line and is not unique for load-unload cycles. Changes in water content can affect the case with which the particles may slide relative to each other.</p> <p>Settlement is dependent upon water content, and the water table at the moment of load transfer</p> <p>Variation in water content and water table will produce variations in deformation, even though a loading system remains constant</p> <p>Introduces a time-deformation relationship</p>

6.4 Conclusion

Settlement prediction is not merely concerned with conditions at the time of loading. Subsequent variations of local conditions (e.g. rain) will influence soil behaviour after loading. Settlement predictions should therefore make allowances for subsequent changes in water content in the soil which may take place after construction of the building.

CHAPTER 7

THE STRESS PATH

7.1 Stress states that influence settlement predictions

In most methods of settlement prediction (other than the stress path method) the engineer is concerned with the initial in situ field stress state (before application of design loads), the stress state immediately after application of design loads and the final stress state (after dissipation of pore water pressures). The engineer has not taken into account the 'path' followed in going from one stress state to another.

This chapter will illustrate the importance of considering the actual stress paths, and the influence of these stress paths on the behaviour of the soil.

7.2 Stress equilibrium (two dimensional stress state)

Consider an element of soil subjected to stresses σ_1 , σ_2 and σ_3 . In Figure 7.1 it is assumed in this case that $\sigma_2 = \sigma_3$ (see Chapter 4). Hence the normal stress on any vertical section in Figure 7.1 is $\sigma_h = \sigma_2 = \sigma_3$.

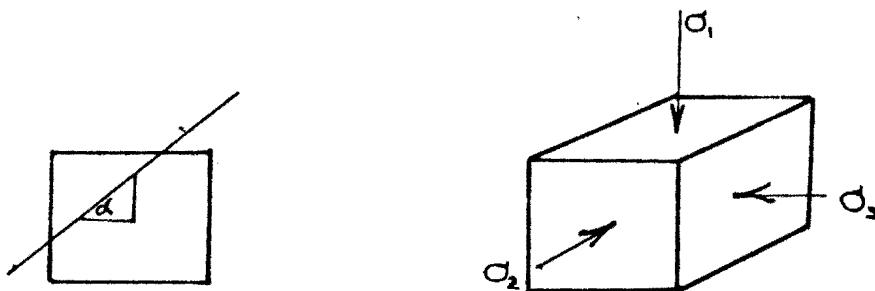


FIGURE 7.1 Principal Stresses σ_1 , σ_2 , σ_3
(i.e. zero shear stress on surfaces shown)

If the value of σ_1 is increased until shear failure occurs along an inclined face, the engineer would be interested in the stresses on the inclined face at failure (see Figure 7.1 and 7.2).

Resultant of σds and τds

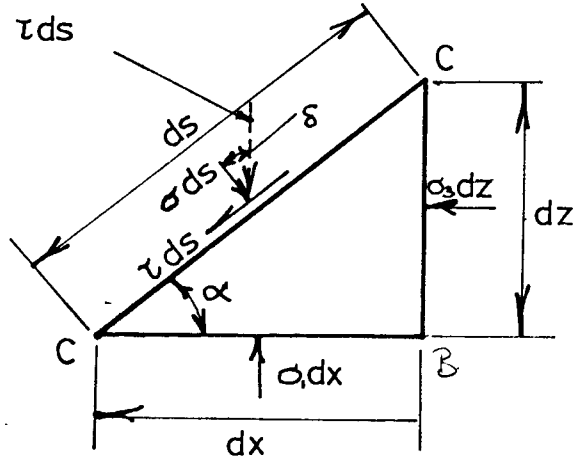


FIGURE 7.2 Definition of Stresses and Forces on a Face c-c Inclined to the vertical CB

For discussion of the stress paths, the assumption is made that under the footing, plane strain conditions are satisfied. Therefore it is only necessary to consider the stresses which act parallel to one vertical slice as in Figure 7.2.

Plane strain conditions (Lambe and Whitman, Ref. 2, Rauch, Ref. 17).

1. Every slice of earth orientated parallel to this plane is subjected to the same stress state. This implies a large loaded area.
2. Under normal conditions the soils engineer is dealing with a continuous mass of earth with a constant cross section and with outer boundaries perpendicular to a single vertical plane.
3. The thickness of the slice is not changed by a variation of stress conditions within the slice.

From the equilibrium of the element of soil in Figure 7.2 the following equations must be satisfied:

$$\Sigma \text{ Horizontal forces} = 0 \quad (7.1)$$

$$\Sigma \text{ Vertical forces} = 0 \quad (7.2)$$

Therefore from equation (7.1) and Figure 7.2

$$\sigma_3 \sin \alpha \, ds - \sigma \sin \alpha \, ds + \tau \cos \alpha \, ds = 0 \quad (7.3)$$

Similarly from equation (7.2) and Figure 7.2

$$\sigma_1 \cos \alpha \, ds - \sigma \cos \alpha \, ds - \tau \sin \alpha \, ds = 0 \quad (7.4)$$

Multiply equation (7.3) by $\cos \alpha$ to get:

$$\sigma_3 \sin \alpha \cos \alpha - \sigma \sin \alpha \cos \alpha + \tau \cos^2 \alpha = 0 \quad (7.5)$$

Similarly multiply equation (7.4) by $\sin \alpha$ to obtain:

$$\sigma_1 \sin \alpha \cos \alpha - \sigma \sin \alpha \cos \alpha - \tau \sin^2 \alpha = 0 \quad (7.6)$$

Subtract equation (7.5) from equation (7.6), hence:

$$(\sigma_1 - \sigma_3) \sin \alpha \cos \alpha - \tau (\sin^2 \alpha + \cos^2 \alpha) = 0$$

on simplification

$$\tau = \frac{1}{2}(\sigma_1 - \sigma_3) \sin 2\alpha \quad (7.7)$$

Similarly from equations (7.5) and (7.6) the following can be obtained:

$$\sigma = \frac{1}{2}(\sigma_1 + \sigma_3) + \frac{1}{2}(\sigma_1 - \sigma_3) \cos 2\alpha \quad (7.8)$$

These formulae become rather cumbersome if for a specific value of α the orientation of the plane and the stress on that plane is required. Rather than perform these mathematical manipulations for each state of stress on a plane, a graphical method is used. The graphical construction is called Mohr's circle.

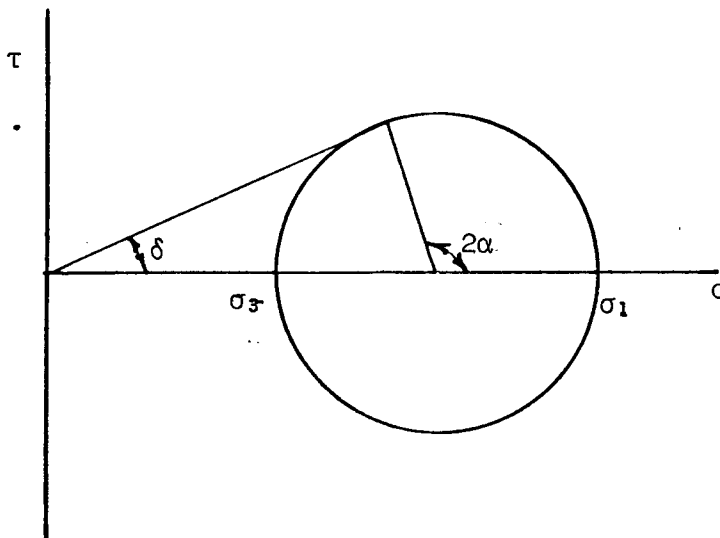


FIGURE 7.3 Definition of Angles α and δ (in equations 7.7 & 7.8)

In Figure 7.3 the compressive stress is plotted along the horizontal axis and the positive shear stress is plotted vertically from the horizontal axis. The resultant stress on the face c-c of the soil element (shown in Figure 7.2) acts at the angle of obliquity δ to the normal to the plane c-c. Mohr's diagram enables the engineer to determine the state of stress on any face of a soil element for a given stress condition.

7.3 The stress path

The Mohr's circle represents a method of graphic determination of stresses on various faces for one stress system. Therefore for every two dimensional stress system a Mohr's circle can be defined. Rather than draw a Mohr's circle for each stress system, use is made of a stress point. A stress point is a single point that fully defines the Mohr's circle in position and size (see Figure 7.4).

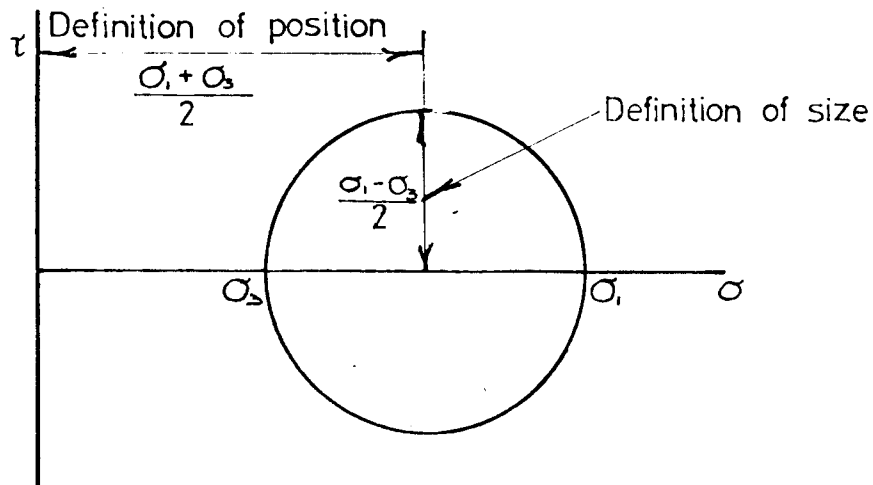


FIGURE 7.4 *Illustration of how a stress point effectively defines Mohr's Circle in Both Size and Position*

Figure 7.5 shows a number of Mohr's circles with their stress points. A stress path connects all these stress points.

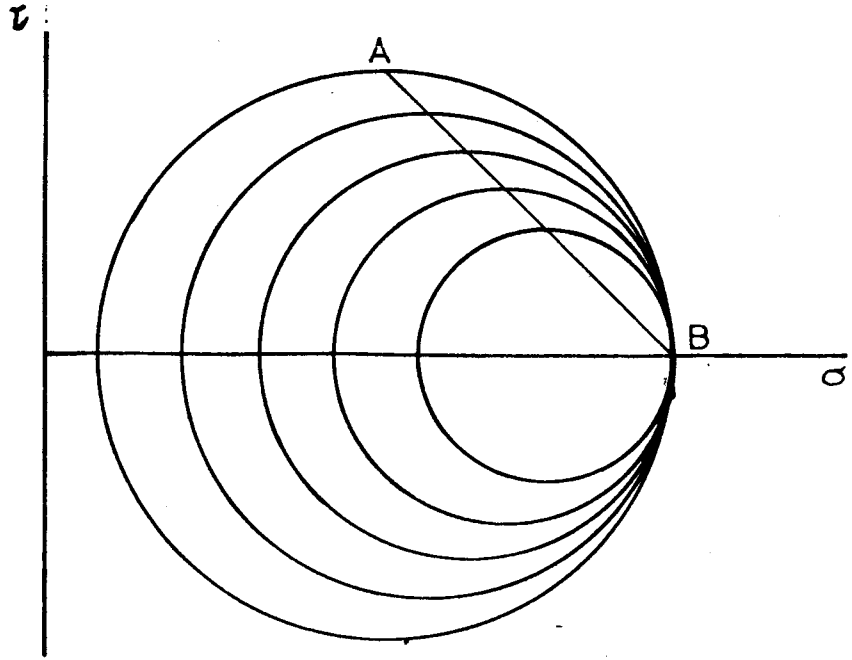


FIGURE 7.5 The stress Path AB Represents the Application of an Increasing σ_3 with a constant σ_1 . (In going from A to B)

To define the changes in stress due to the loading of a soil element an infinite number of stress points have to be plotted. The line joining these stress points defines the stress path. Stress paths are plotted on $p - q$ diagrams or $\bar{p} - q$ diagrams

$$p = \frac{\sigma_1 + \sigma_3}{2} \quad (7.9)$$

$$\bar{p} = \frac{\bar{\sigma}_1 + \bar{\sigma}_3}{2} \quad (7.10)$$

$$q = \frac{\sigma_1 - \sigma_3}{2} \quad (7.11)$$

$$\bar{q} = q \quad (7.12)$$

The total stress path defines the changes in total stress systems while the effective stress path is related to the effective stress changes.

7.3.1. Example of a stress path

Let ABC (see Figure 7.6) represent the effective stress path for a non-typical triaxial sample. The arrowheads indicate the loading sequence.

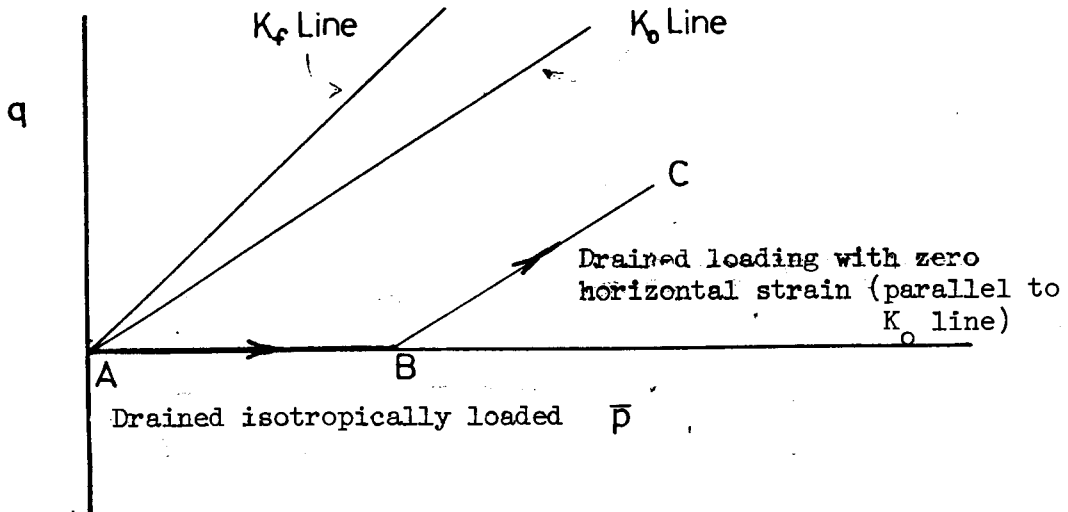


FIGURE 7.6 Stress Path Example

Section AB of the stress path will correspond to the drained isotropically loaded sample (final cell pressure is σ_B). Section BC corresponds to a drained loading condition with a zero horizontal strain (with cell pressure increasing from σ_B). This implies that the ratio of the increase of horizontal effective stress to the increase in vertical effective stress remains constant, and this ratio is equal to K_0 .

For this stress path we can define any one stress point. For that stress point any stress conditions on any plane for this soil sample can be described.

7.4 The stress path method of settlement prediction

The ultimate aim of the civil engineer is to apply field conditions to 'undisturbed' samples and to use the results from the tested samples for prediction of field conditions.

For accurate settlement prediction it is necessary to establish whether to make calculations for either one or more 'average' points under the foundation or to integrate a strain-versus-depth curve obtained for several points.

The stress path method of settlement prediction consists basically of two steps (Lambe, Ref. 7).

1. The estimation of the history and variation of stress and strain for one or more elements of soil in the actual field structure.
2. The use of soil tests (laboratory and field) and analytical techniques which approximate the field stress and strain conditions before, during and after construction.

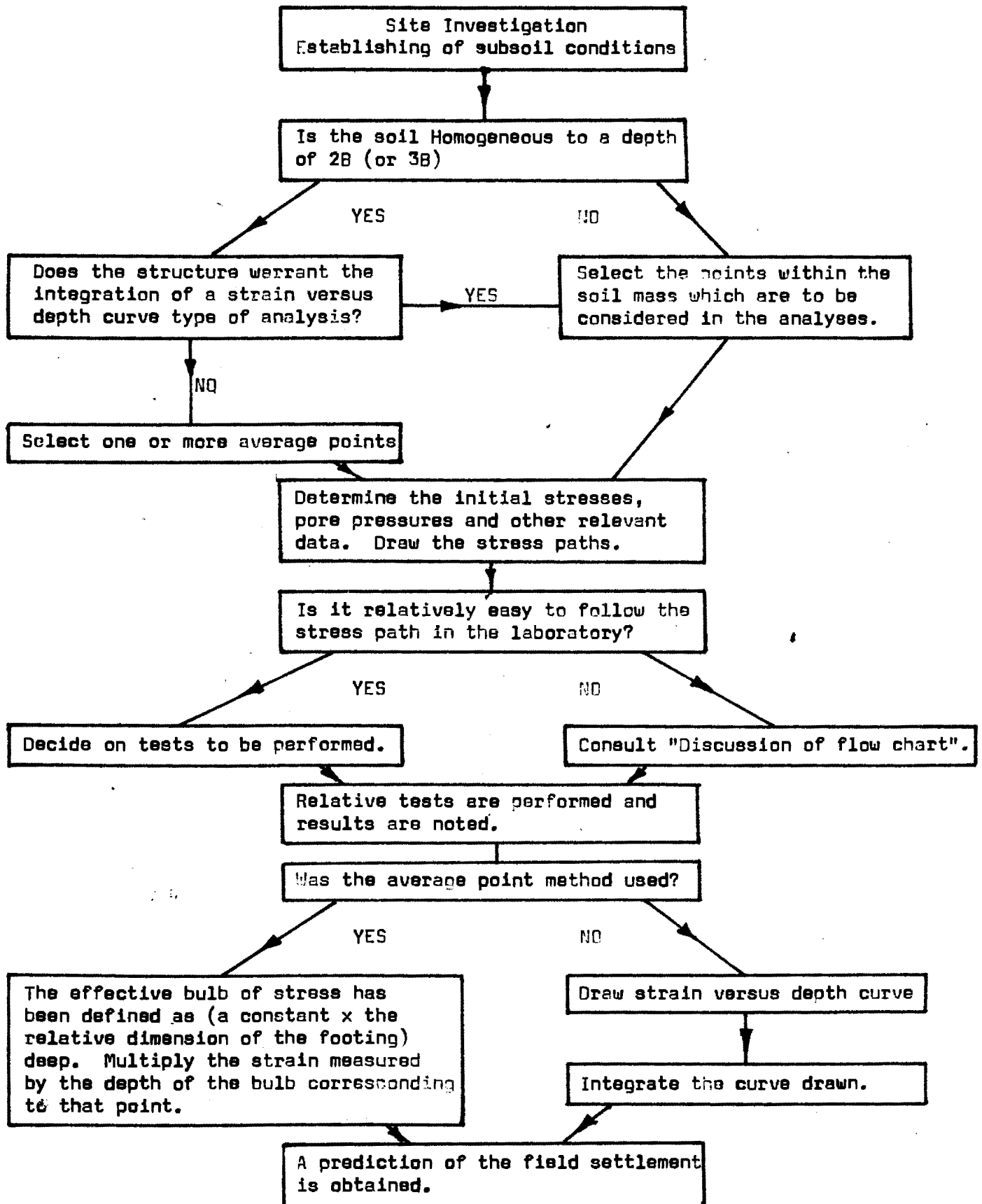
Lambe (Ref. 7) does not lay emphasis on the necessity of highly sophisticated apparatus, or three dimensional stress analysis and testing procedures. He does however emphasize ^{that} the most correct approximation of field conditions is essential for accurate settlement prediction.

The first step in the stress path method provides information on the consolidation stresses, or the initial stress system, before loading occurs. This information will denote the method of testing for the first stage of the test.

The second stage of the test involves the application of the imposed surface loads. From the stress path drawn from step two, the method of testing that will accurately duplicate the field conditions can be deduced. Figure 7.7 shows the flow chart for the stress path method of settlement prediction.

7.5 Discussion of the flow chart

Lambe does not provide a flow chart but the following is an example illustrating the method suggested by Lambe (Lambe, Ref. 7, Davis Poulos, Ref. 6). Consider a sample soil element in the field (in a triaxial cell) which is first allowed to consolidate



under K_0 conditions to the state A. Then it is subjected to an increase in vertical total stress (while the horizontal total stress remains constant). The sample is then allowed to consolidate under this loading.

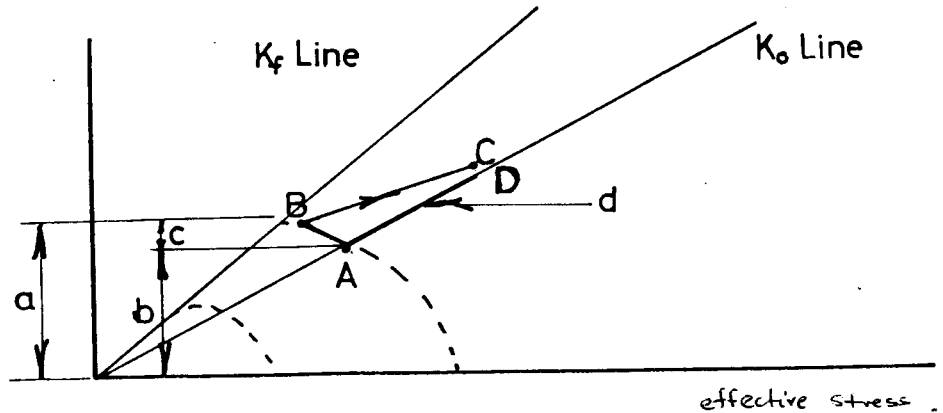


FIGURE 7.8 Example Illustrating the Stress Path Method used by Lambe (Ref. 7)

- a = total undrained shear strength
- b = shear stress developed due to application of K_0 conditions
- c = additional shear stress experienced during undrained shear
- d = equivalent K_0 stress path

Consider the field conditions to be described by the effective stress path ABC. Where AB shows the undrained loading stress variations, and BC represents the consolidation of the loaded soil.

The settlement will result from the stress variations in going from A to B and B to C.

Firstly the axial strain due to undrained compression is estimated. This can be found from an undrained triaxial test where the vertical deflections, in going from A to B, are recorded.

The next step followed by Lambe is to compute the volume change during consolidation (Σ volume consolidation) corresponding to the corresponding consolidation stress path along the K_0 line AD for this same total stress change. This is done as follows:

The position of C is estimated by using increments from Boussinesq's equations. These increments are from the state A. The point D is obtained by drawing a curve (similar to the undrained loading effective stress path BA) from C to cut the K_o line at D. The appropriate stress path which could be used in an ordinary oedometer is then represented by AD. Most of the samples are tested in the oedometer, but these results must be modified by a correction factor which varies with soil types and stress paths. A consolidation in a triaxial cell must be performed to estimate this correction factor.

Using a triaxial test, the actual vertical axial strain during consolidation BC, of the soil element, is determined. This is achieved by performing a triaxial test which follows the actual stress path BC. From this an estimate of the ratio between the axial strain and the volumetric strain during consolidation is obtained. An expression which approximates this relationship is:

$$(\Sigma_{\text{axial consolidation}}) = \frac{1 + K_o - 2K K_o}{(1 - K_o)(1 + 2K)} (\Sigma_{\text{axial strains oedometer}}) \quad (7.13)$$

where

$$(\Sigma_{\text{axial consolidation}}) = \text{actual axial strain during triaxial consolidation } (\Delta \ell / \ell_o)$$

$$(\Sigma_{\text{axial strains oedometer}}) = \text{volumetric strain obtained by the appropriate } K_o \text{ test } (\Delta e / 1 + e_o)$$

K_o = initial effective principal stress ratio (for state at A)

K = final effective principal stress ratio (for state at C)

Now the total axial strain for the in situ element subjected to triaxial stress can be estimated as follows. This value is the sum of the immediate axial strain during the undrained condition and the consolidation axial strain.

$$(\Sigma_{\text{total}}) = (\Sigma_{\text{undrained}}) + (\Sigma_{\text{axial consolidation}})$$

Lambe therefore suggests that only one (or maybe two) triaxial tests be performed following the stress path ABC and to find the K_0 value and to estimate ϵ undrained and to verify equation (7.13). The remaining tests can be carried out on the consolidometer following an appropriate K_0 stress path. Equation (7.13) is applied to the oedometer results to obtain ($\epsilon_{\text{axial consol.}}$)

7.5.1. Modification suggested by the writer

From test results compute as before the axial strain due to undrained loading. Now examine the stress path. Does the end point of the stress path lie close to the assumed K_0 line for this soil (i.e. is K approximately equal to K_0). If it is not, then carry on with Lambe's method (i.e. equation (7.13)).

If K approximates K_0 , then only consolidometer tests or K_0 triaxial tests need be considered for the appropriate K_0 stress paths. The field consolidation axial strain will be approx equal to the volumetric strain determined by the K_0 test.

In the K_0 triaxial test, the factor on the left-hand side of equation (7.13) is equal to the axial strain term in the brackets on the right-hand side of this equation. Note that this becomes possible when one uses $K = K_0$ in equation (7.13).

Does the portion of the stress path corresponding to drained consolidation (as calculated by using Boussinesq) have the same slope as the assumed K_0 line? If it does, then a K_0 type triaxial test can be performed to obtain ($\epsilon_{\text{axial consolidation}}$) directly, instead of using equation (7.13). This K_0 test must be done in a triaxial cell, and not in an oedometer.

This simplification will be appreciated by the triaxial machine technician ^{because to simulate} (as to follow) a relatively complicated stress path is a drawn out process which demands the highest degree of concentration.

7.6 Stress paths for standard laboratory testing procedures

The stress path that is in most cases the critical one for settlement is the effective stress path, as this is the stress path that the soil skeleton will experience on a macroscopic scale. It is this stress path that causes displacements in soils.

7.6.1 The consolidometer (i.e. the oedometer)

A typical stress path for a loading increment in consolidometer is shown in Figure 7.9. This is described in this section. The load is applied instantaneously to the sample. The soil is prevented from deforming laterally; that is, zero horizontal strain occurs (see Figure 7.10(a)). If we assume zero horizontal strain, then if the vertical stress increment is applied quickly to a saturated sample there is no volumetric strain and therefore no shear strain. This implies zero changes in effective stress and shear stresses during the instant of load application.

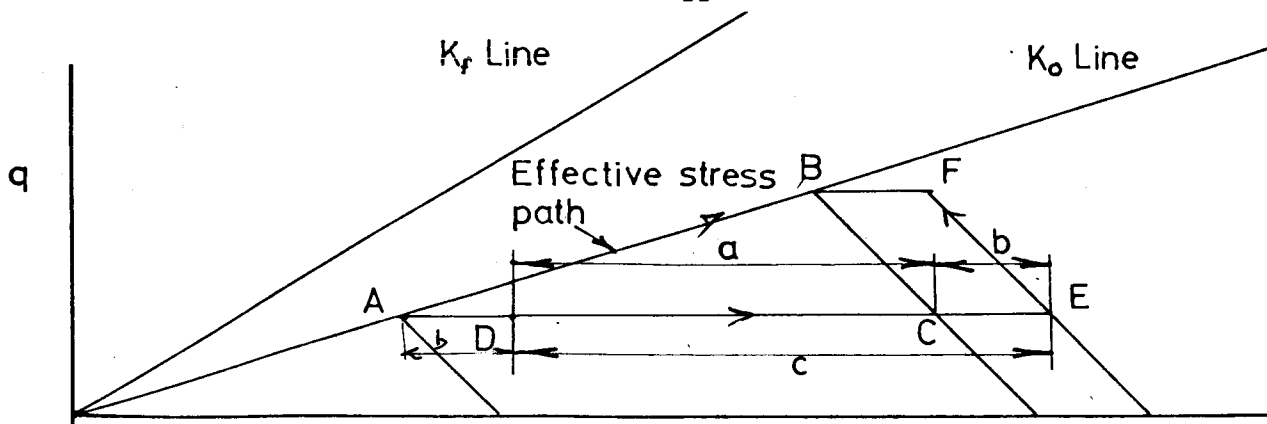


FIGURE 7.9 Stress paths for Consolidometer Test (loading)

- a = excess pore pressure Δu due to load increment
 b = static pore water pressure u before loading
 c = total pore pressure u immediately after loading

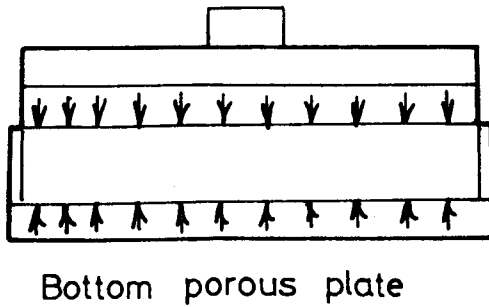
- AB = effective stress path
 DEF = total stress path
 ACB = (total - u_{static}) stress path

$$u_{static} = \text{static pore water pressure}$$

u = pore water pressure (total)

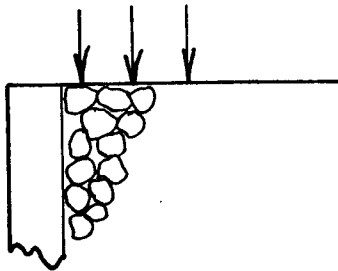
For undrained loading: Effective stress path stays at A

Total stress path = DE

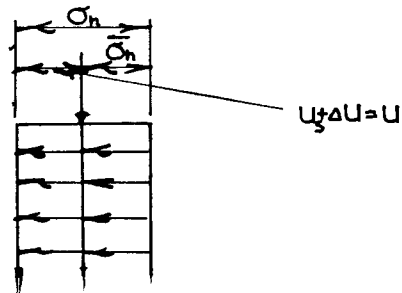


Consolidometer ring provides
confining horizontal pressures

FIGURE 10(a) *Consolidometer Sample*



Consolidometer ring



Horizontal pressures exerted on the ring

FIGURE 10(b) *Pressures Experienced by Consolidometer Ring*

If at the instant of load application there is no change in effective stresses or shear stresses then the excess water pressure must be equal to the load increment. The stress on the consolidometer ring (which equals the total horizontal stress) is equal to the effective stress plus the total pore water pressure. Thus at the instant of loading there is an increase in the total stresses while the effective stresses and shear stresses remain constant.

The effective stress path from A to B (see Figure 7.9) describes the sequence of effective stress systems imposed on the soil particles as dissipation of water pressure takes place.

The total stress path from E to F (see Figure 7.9) describes the total stress system imposed on the consolidometer ring during dissipation of excess water pressures.

During drainage, the horizontal and vertical effective stresses change, therefore a volume change and a shear strain will occur. The relationship of the vertical and horizontal effective stresses remain constant because K_0 conditions are approximately satisfied in the oedometer.

7.6.2 Unloading

Figure 7.11 depicts a typical stress path for the unloading of a consolidometer sample. For undrained unloading the effective stress path stays at A and the total stress path is DE and the $(\text{total} - u_{\text{static}})$ stress path is AC.

When the specimen is unloaded, a decrease in pore pressure causes the water surrounding the sample to be sucked into the sample and the soil swells during the dissipation of the negative pore pressures.

During this swelling after unloading, the ratio of the vertical to horizontal effective stress does not remain constant, as the sample is not perfectly elastic in that each soil particle will not return to its original position before loading occurred.

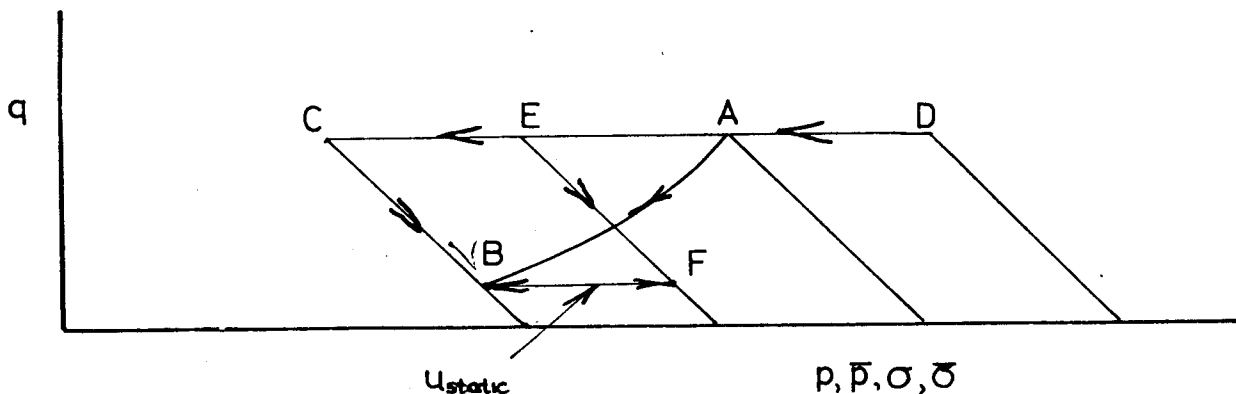


FIGURE 7.11 *Stress Path for Unloading of a Consolidometer Sample (Lambe, Ref. 7) (Horizontal stresses determined from other research workers results)*

AB	=	effective stress path
DEF	=	total stress path
ACB	=	(total - u_{static}) stress path
u_{static}	=	static pore water pressure
u	=	total pore water pressure
$u - u_{static}$	=	excess pore water pressure

The curve in Figure 7.11 was drawn by Lambe and based on experimental results observed by Hendron, Brooker and Ireland in 1965. They performed consolidometer tests in which the horizontal and vertical stresses could be measured. They produced curves which related K_0 , overconsolidation ratio and plasticity index P.I. The overconsolidation ratio can be defined as

$$\text{Overconsolidation ratio} = \frac{\bar{\sigma}_{vm}}{\sigma_{vo}}$$

where

$\bar{\sigma}_{vm}$ = maximum previous vertical stress (e.g. if A lies on K_0 line in Figure 7.11, then $\bar{\sigma}_{vm}$ corresponds to state A)

σ_{vo} = field stress (e.g. stress at state being considered; state B or state A)

7.6.3 The triaxial tests - (consolidated undrained)

The consolidated undrained loading in nature is regarded as consisting of two distinct stages. The first stage is the application of the stresses due to self weight of the soil mass. The second is the application of the stress increments due to a load being applied at some point on top of, or at some point within that soil mass.

The triaxial test results as shown, differ slightly from the in situ condition in that during the first stage of the triaxial test the soil is allowed to consolidate isotropically under the action of a stress system which does not represent the stresses induced due to the self weight of the soil mass. In nature

this would correspond to a K_0 condition. The second stage of the triaxial test is concerned with the undrained vertical loading of the sample. In the triaxial test this vertical loading is applied while the horizontal cell pressure σ_z remains constant (i.e. horizontal strain is permitted). In nature, horizontal strain is limited by the adjacent soil during this undrained shear. From the results of this type of triaxial test, the effective undrained loading stress paths can be drawn. Lambe superimposes undrained vertical strain contours on the stress paths to produce the 'pure form' of the stress path method of settlement prediction.

The method to determine the total settlement from the curves shown in Figure 7.12 is as follows. Firstly the field effective stress path must be superimposed on the diagram. The strain value corresponding to the initial state of stress is subtracted from the strain value of the final state of stress. This difference in strain value will be the total strain for that stress path. Where the total strain is the sum of the immediate strain due to undrained loading plus the hydrodynamic consolidation strain. The total settlement will be the total strain multiplied by the depth of the soil layer corresponding to the stress path.

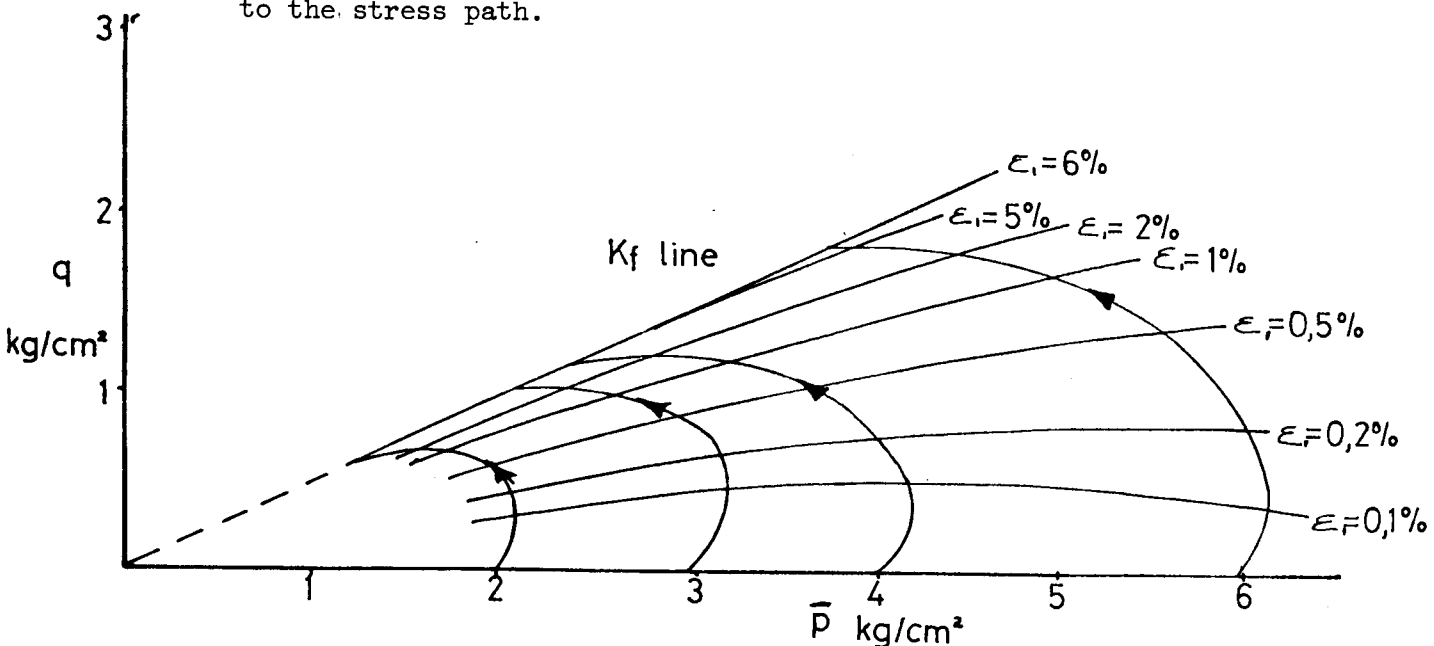


FIGURE 7.12 The Pure Form of the Stress Path Method
(Lambe and Whitman, Ref. 2)
Effective stress paths from consolidated undrained tests on a normally consolidated clay

7.6.4 Consolidated drained test

To be able to demonstrate the variation in drained stress paths from the undrained test, the first stage of the test will be considered similar to the above. The second stage is different in that the soil is allowed to drain during loading. This implies that the excess pore pressure will remain constant and equal to zero (see Figure 7.13) - Depending upon the rate of loading.

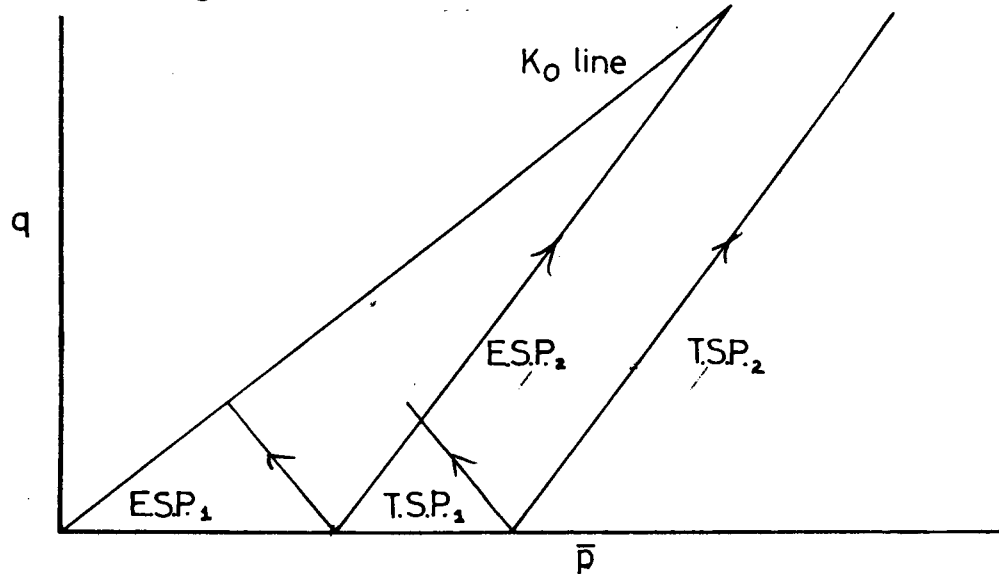


FIGURE 7.13 *Stress Paths for Consolidated Drained Triaxial Tests*

Each soil particle will immediately 'feel' the total stress variation and therefore the effective stress path and the total stress path will be parallel.

7.7 Deformations associated with various stress paths

In an elastic material subjected to a three dimensional stress system, the following formulae apply (see Chapter 4):

$$\epsilon_x = \frac{1}{E} [\sigma_x - \mu(\sigma_y + \sigma_z)] \quad (7.14)$$

$$\epsilon_y = \frac{1}{E} [\sigma_y - \mu(\sigma_x + \sigma_z)] \quad (7.15)$$

$$\epsilon_z = \frac{1}{E} [\sigma_z - \mu(\sigma_x + \sigma_y)] \quad (7.16)$$

From these formulae it is obvious that each component of strain is a function of the three dimensional stress system; and therefore the deformations of the elastic material are relative to the stress system applied to it. For a perfectly elastic body the particular stress system would provide sufficient information to calculate the deformations (if E and μ are known).

In the theory of soil mechanics an elastic stress distribution within a soil mass is assumed (i.e. elastic formulae are used to predict the extra total stress distribution within the soil mass - see Chapter 4). The soil mass, however does not generally behave elastically and it is therefore necessary to know the immediate and long term 'stress history' of a soil mass.

Under long term stress history all the past overburden pressures are considered. The immediate stress history would be represented by the stress path. The stress path being the variations in stress systems from immediately before construction until an equilibrium stress system is achieved. Equilibrium occurs when the stress system is such that the appropriate total stress minus the static pore pressure equals the effective stress. From the above it can be concluded that the deformation within a soil mass and the effective stress path are related.

The following examples are of stress paths and the deformation associated with them. The deformations are obtained from triaxial tests (Lambe, Ref. 7, Lambe and Whitman, Ref. 2, Moore and Spencer, Ref. 38, and E.D. Appolonia, Ref. 24).

The triaxial samples in Figure 7.14 have been allowed to consolidate fully under K_0 conditions. Drained compression along stress paths 1, 2 and 3 are applied to the consolidated samples in order to illustrate the relationship between types of deformation and the position of the effective stress path (see Table 7.1).

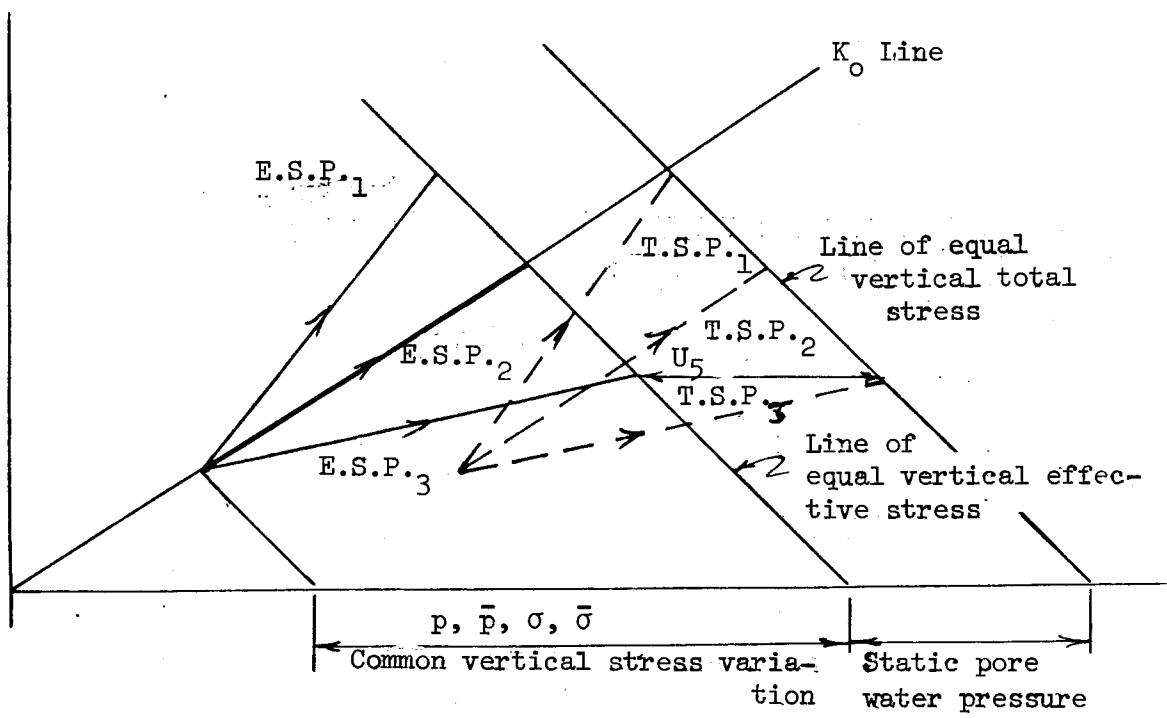


FIGURE 7.14 The Deformations Associated with these Stress Paths are shown in Table 6.1

----- Total stress path
———— Effective stress path

TABLE 7.1 Stress paths and their associated deformations

Effective Stress Path No	Deformation
1	
2	
3	

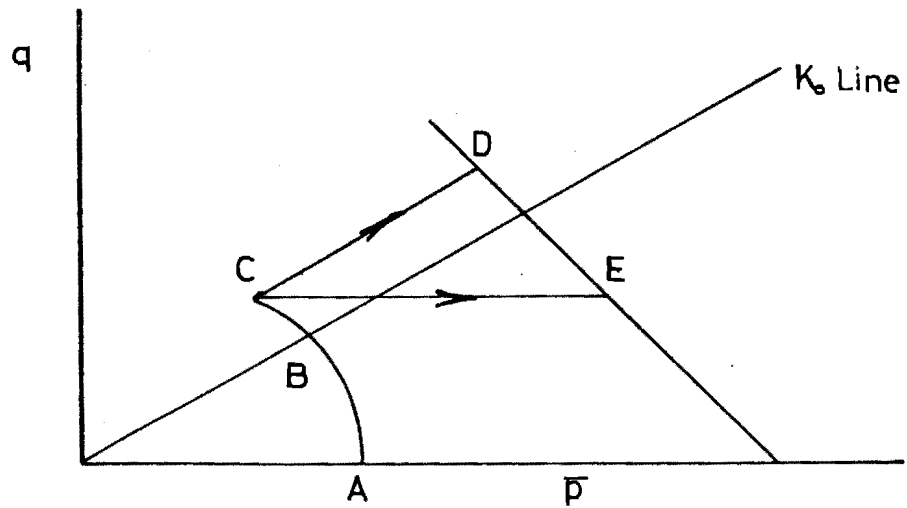





FIGURE 7.15 Examples of Stress Paths and their Associated Deformations (see Table 7.2)

TABLE 7.2

Stress Path	Description	Deformation
ACD	In the triaxial, the soil is initially isotropically consolidated (at state A). Increases in stress are then applied to the soil i.e. the vertical total stress is increased and the horizontal total stress (all pressure) is increased slightly while the stress path moves in an undrained condition from state A to C.	A \rightarrow C 
CD	From C to D the loading remains constant, but the internal effective stress distribution changes. Dissipation of excess pore pressures take place.	In going from C to D there is no additional horizontal deformation as CD is parallel to the K_0 line

Stress Path	Description	Deformation
ACE	Stress path AC is as before. Stress path CE is due to the dissipation of excess pore pressures. The slope of CE is different. This implies the mode of stress change during drainage is different and hence the deformations will be different (i.e. see Figure 7.12 which shows the vertical deformations)	<p>A → C </p> <p>C → E </p> <p>For a effective stress path which is horizontal (CE), the ratio of the vertical strain to the volumetric strain $\approx \frac{1}{3}$ (Lambe, Ref, 7)</p>
BCD	Corresponds to ACD except that the initial condition satisfies the equation $\bar{\sigma}_3 = K_o \bar{\sigma}_1$	
BCE	Corresponds to ACE except that the initial condition satisfies the equation $\bar{\sigma}_3 = K_o \bar{\sigma}_1$	

7.8 Examples of field stress paths

(Lambe, Ref. 7, Lambe and Whitman, Ref. 2, Moore and Spancer, Ref. 38 and E.D.'Appolonia, Ref. 24)

Figure 7.16 describes various stress paths with their associated K_o approximated stress paths. It is necessary to establish whether the K_o approximation is valid (see Section 7.5).

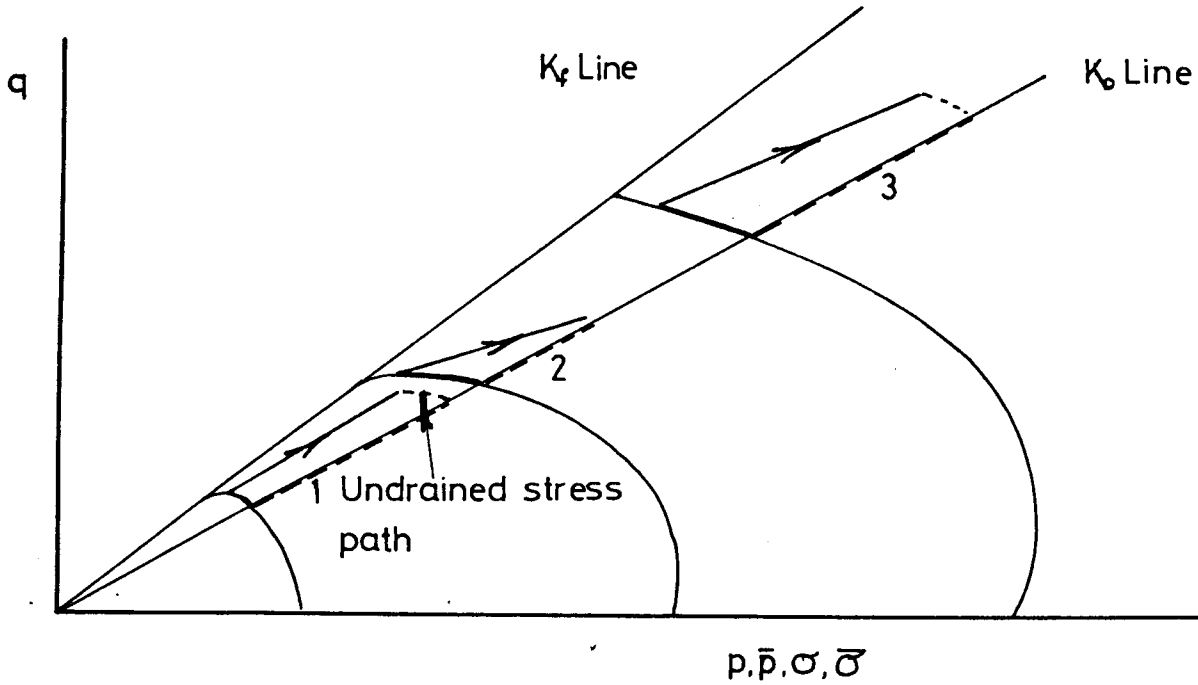


FIGURE 7.16 Stress Paths with Equivalent K_0 Conditions

----- Equivalent K_0 stress path
 ————— Stress path

The K_f line is obtained from q_f versus \bar{p}_f plots from consolidated drained tests

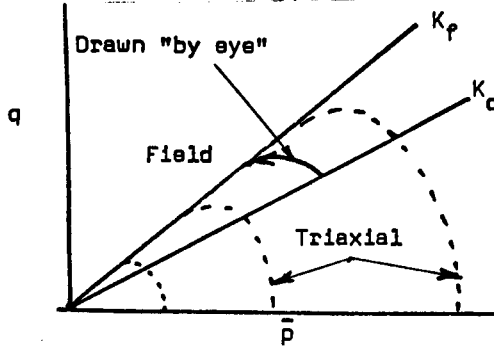
$$q_f = \frac{\sigma_1 - \sigma_3}{2} \quad \text{at failure} \quad (7.17)$$

$$\bar{p}_f = \frac{\bar{\sigma}_1 + \bar{\sigma}_3}{2} \quad \text{at failure} \quad (7.18)$$

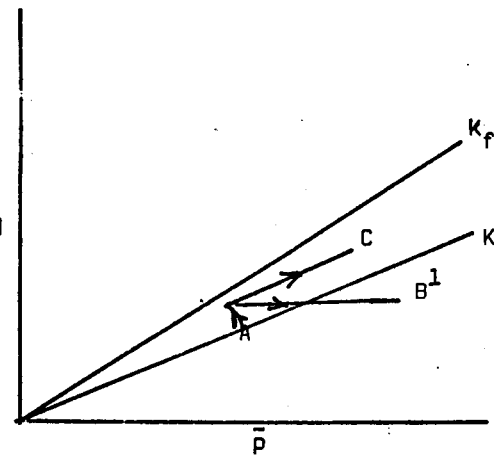
The K_0 line is obtained from a triaxial test allowing zero horizontal strain. From the data of this test the slope of the K_0 line is obtained. The writer suggests the following general method for settlement analysis:

STRESS PATH

DETAILS



First perform consolidated undrained triaxial tests in which the pore pressures are measured (Bishop, Ref. 9) The undrained stress paths (dotted) would be drawn before the field stress paths are drawn. The field undrained loading effective stress paths could be approximated knowing the shape of 3 or 4 of these undrained triaxial stress paths. This is used to draw the dotted line DC in the last diagram of this table



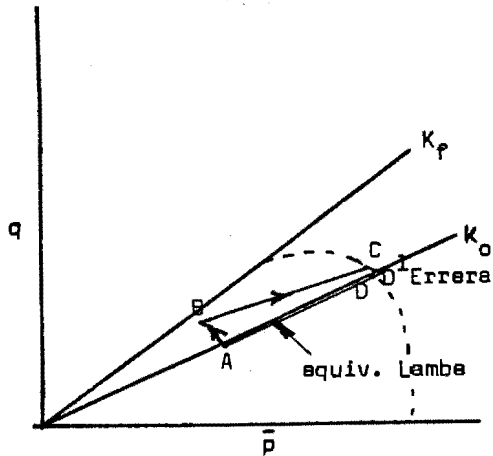
ABC might be the stress path under a column footing for a bridge. The field stress distribution obeys the K_0 criteria before application of the foundation load. AB is the immediate change in stress due to undrained loading at the time when the load is applied. Point B can be found from field measurement (i.e. piezometer tubes will indicate the excess pore pressure at state B. Total stresses are estimated by using Boussinesq's equations Hence the total stress point B' is known. B is found from B' by using the measured pore pressure). Alternatively laboratory measurements can be used (triaxial undrained test from state A to state B). The immediate settlement due to AB would be observed in the undrained triaxial test. The final stress system (at C) can be calculated from elastic formulae, (see Chapter 4).

Looking at the flow chart drawn for settlement prediction using the stress path method it can be seen that the decision to be made is, 'is it relatively easy to follow the natural stress path in the triaxial machine'.

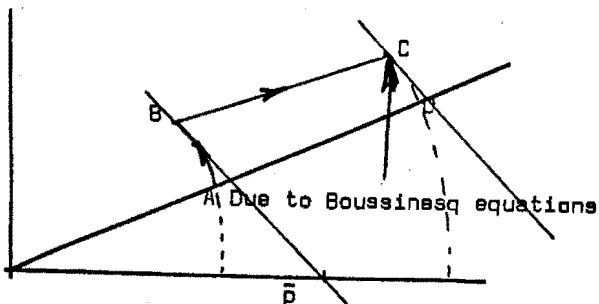
The answer to this would be yes, as the slope BC on the 'q versus \bar{p} ' plot is parallel to the K_0 line. The triaxial test corresponding to BC would then be a drained test with zero horizontal deflection (Chapter 10). The horizontal deflection is zero because BC is parallel to the line K_0 . From these triaxial test results the hydrodynamic consolidation settlement during drainage can be computed by summing the vertical strains from state B to state C. To find the total settlement due to the load, this hydrodynamic settlement (due to drainage from state B to state C) should be added to the initial undrained settlement found above (due to loading from state A to state B).

STRESS PATH

DETAILS



In most practical cases the line BC is not parallel to the K_o line. The field stress system obeys the K_o criteria (point A). Because the increment A to C is determined by Boussinesq's type equations, it does not follow that the point C will lie on the K_o line even when the soil has fully drained. Point C can be calculated relative to point A by using these Boussinesq's equations (see Chapter 4). To find the point D (which determines the simplified laboratory stress path A to D) one can assume that CD lies on the unstrained stress path from C to D. (The stress path CD can be sketched in by eye, knowing the shape of 3 or 4 typical curves. see Figure 7.12). Hence the stress path AD to be used in the laboratory K_o test is known. One can use a K_o triaxial test, or an oedometer test for the settlement prediction. AB is the immediate change in stress systems due to the undrained loading. BC is the consolidation stress path, due to drainage. AD could be the stress path used in a laboratory K_o test. The in situ stress path BC is not a relatively easy stress path to simulate in the laboratory [horizontal strain $\approx \frac{1}{3}$ volumetric strain during in situ drainage]. Hence the advantage of using the simpler stress path AD in the laboratory tests. Lambe uses the simplified stress path AD. Considering that point C is a stress system which approximates K_o conditions then Lambe's approximate K_o stress path would be appropriate. Lambe does not sketch in the line CD but assumes the same 45° line passes through C and D to the stress $\bar{\sigma}$, on the \bar{p} axis. According to Lambe the immediate settlement would be computed as before by performing undrained triaxial tests or by using available curves such as Figure 7.12. It seems that Lambe determines the consolidation drained settlement from either consolidometer or triaxial tests.



If the final state C deviates considerably from the K_o line the diagram is as shown. AB is the immediate stress path. BC is the consolidation (i.e. drained) stress path. The immediate settlement is calculated as before. The point C is relatively distant from the K_o line and consequently Lambe's method (see Section 7.5) would have to be used. CD is on the undrained stress path from C to D.

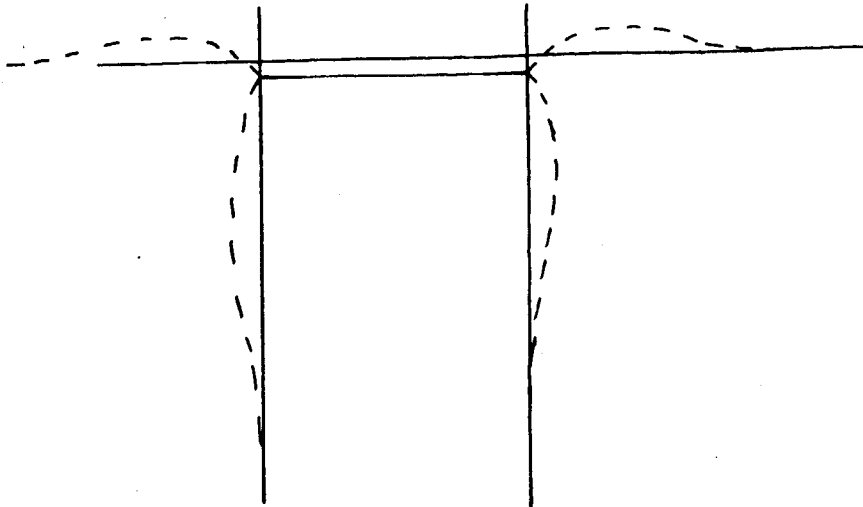
Cohesionless Soils

FIGURE 7.17 *Settlement Deformations Associated with Cohesionless Soils*
(D. Bond, Ref. 39)

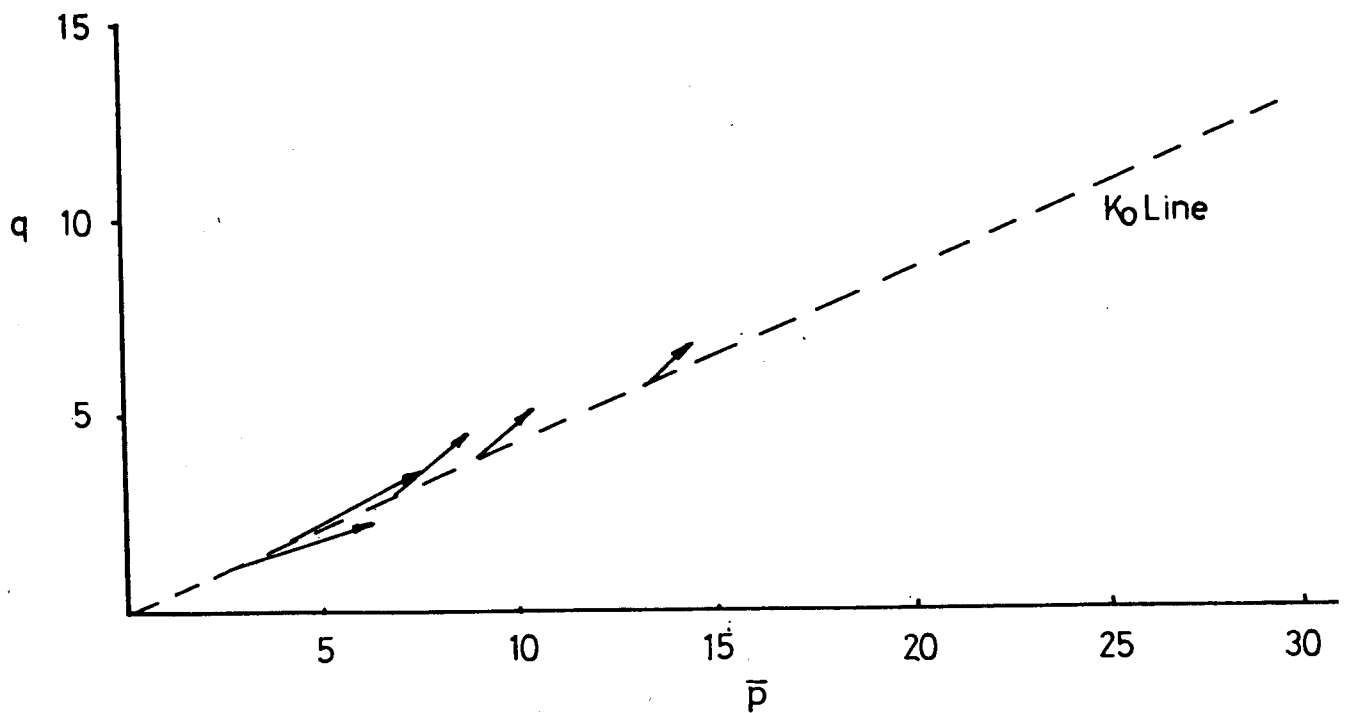


FIGURE 7.18 *Stress Paths for Cohesionless Granular Soil (fine to medium soil)* (Lambe and Whitman, Ref. 2)

The stress path for a granular cohesionless soil might start on the K_0 line and end at some point relatively close to the K_0 line after being subjected to some load system. Because the final state does not lie on the K_0 line the inference is that a horizontal deformation has taken place. The magnitude of this horizontal deformation is however very small in comparison to the vertical deformation. It is generally considered to be negligible (see Chapter 4). The equivalent K_0 stress path is considered to be appropriate for laboratory tests.

The settlement would then be computed by summing the vertical strains from a consolidometer or K_0 triaxial test. If for some reason the initial stress system does not satisfy the K_0 condition then a suitable triaxial test is imperative.

7.9 Conclusion

The theory of the stress path method has been presented. The deformations and laboratory tests which are associated with field conditions have been described. A civil engineer must visit a proposed construction site to obtain a profile and soil samples. Field stress paths are predicted. Appropriate laboratory stress paths are followed in testing the soil. From this information described, an experienced civil engineer can without further visits to the site describe in some detail, the type of soil, the deformations occurring, the variation in the pore pressures and the immediate and drained consolidation settlement.

Collapsing and expansive strains due to subsequent changes in water content may occur and hence the laboratory tests should include these changes which would be applied after the laboratory sample has reached state C (see diagram on previous page).

Inspection of the predicted field stress path indicates the suitable laboratory testing procedure which can be used (i.e. special triaxial settlement tests; or K_0 tests in triaxials or oedometers).

CHAPTER 8

METHODS OF SETTLEMENT PREDICTION - A REVIEW OF AVAILABLE METHODS

8.1 Introduction

It was necessary to describe the stress path method in Chapter 7 before attempting a historical review of methods of settlement prediction.

8.2 Historical notes (Lambe, Ref. 5, Lambe and Whitman, Ref. 2, D'Appolonia, Ref. 24)

Initially settlement prediction methods were limited to the use of elastic formulae applied to initial and final stress values. The initial stress value is the in situ state of stress before application of foundation loads. The final in situ stress state occurs after dissipation of excess water pressures caused by foundation loads. Terzaghi who is considered to be the 'Father of soil mechanics' first presented theories in 1924 for the computation of ultimate settlement and the rate of settlement. The original solution was developed for a layer of clay subjected to a pressure increment over a large area. Large areas were considered in order to limit the shear deformations and to obtain a uniform hydrostatic pressure within the clay layer itself. His theory related the ultimate settlement to the area of the 'vertical strain versus depth' curve.

In 1936 Casagrande recognised the effects of preconsolidation pressures on an $e - \bar{p}$ curve determined from standard consolidometer tests. The correlation of field tests and laboratory tests was improved by taking account of this effect. The accuracy of settlement predictions were also improved.

In 1955 research workers Skempton, Peck and Mac Donald predicted values of settlement for six buildings in London and Chicago. The observed settlements agreed with their predictions. Immediate settlement ρ_i or instantaneous shear strains in the clay layers were calculated separately from consolidation settlements.

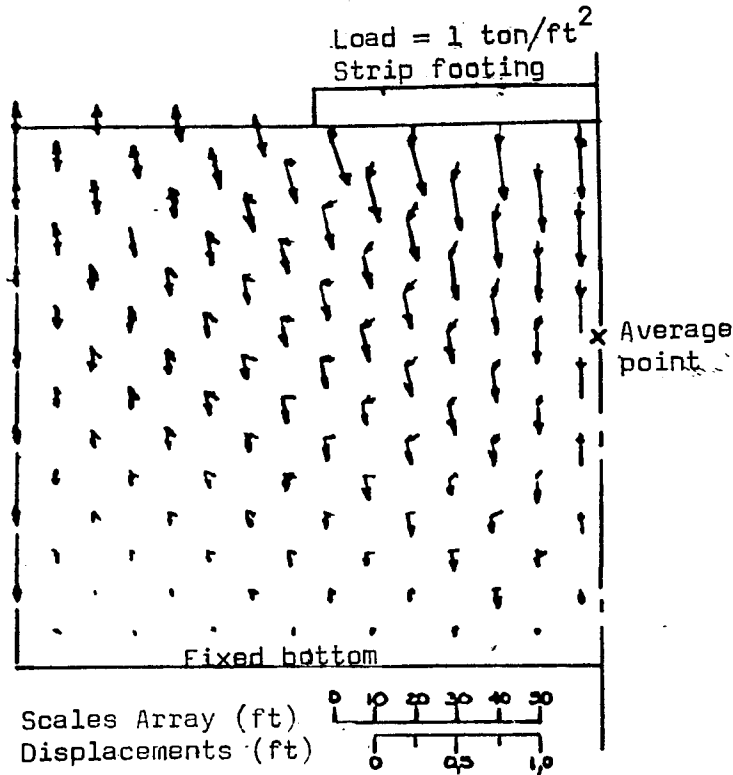


FIGURE 8.1 *Computed Displacements in Elastic Body Subjected to Strip Load. The first arrow is the displacement during undrained loading (shear strains for zero volume change). The second arrow is the displacement during subsequent consolidation (the volume decreases and additional shear strains arise) (Lambe and Whitman, Ref. 2)*

To predict this immediate settlement they used elastic Boussinesq's formula. They then stated (Seed, Ref. 4)

$$\rho_t = \rho_i + (\text{consolidation settlement}) \quad (8.1)$$

where (consolidation settlement) = $(\rho_{\text{conventional}} - \rho_i)_{\text{consolidometer}}$

$$\text{therefore } \rho_t = \rho_i + U (\rho_{\text{conventional}} - \rho_i)_{\text{consolidometer}} \quad (8.2)$$

$$\text{where } \rho_i = qB \left(\frac{1 - \mu^2}{E} \right) I_\rho \quad (8.3)$$

U = degree of consolidation at time t

Boussinesq's formulae when applied to immediate settlement always over estimates the field value. This is attributed (Seed, Ref. 4) to the dependence of the in situ modulus of deformation upon (1) the stress level at which the modulus is measured, (2) the type of test, (3) the stress system used in the test, (4) the direction of the applied major principal stress during laboratory loading relative to the direction of the major principal stress during field consolidation.

In 1956 another two important factors were uncovered by Schmertmann. He proved that consolidation curves for samples with all degrees of disturbance merge together at a void ratio of approximately 40% of the initial void ratio. He also noted that swelling curves due to unloading have essentially the same slope regardless of the pressure at which load reduction is begun.

At about the same time it was shown by Crawford that $e - \bar{p}$ curves are greatly influenced by time intervals during load increments. More important was the discovery that preconsolidation values estimated from laboratory tests are dependent upon load durations during testing.

In 1958 Skempton and Bjerrum modified the formula for immediate settlement after realising that generally the immediate increase in pore pressure (Δu) is not equal to the increase in vertical load ($\Delta \sigma_1$). They expressed Δu as a function of $\Delta \sigma_3$, $\Delta \sigma_1$, and a pore water coefficient A . As A is rarely equal to one, Δu is rarely equal to $\Delta \sigma_1$

$$\Delta u = \Delta \sigma_3 + A(\Delta \sigma_1 - \Delta \sigma_3) \quad (8.4)$$

They therefore effectively reduced the increment in effective stress for consolidation settlement.

From the above it should already be obvious that not only are the initial and final in situ stress conditions important, but also the in situ effective stress path followed. In 1964 Lambe emphasized this point when putting forward the theory of the stress path method of settlement analysis.

8.3 Elastic methods of settlement prediction

Elastic theories state that stress is proportional to strain and that the law of superposition of stress and strain is valid. In Chapter 4 the extra vertical and extra average horizontal stresses due to a load on a finite area were computed.

Consider some point N' a certain distance away from the foundation. The strain curves in Figure 8.4 are for a point under the corner of a rectangle (Terzaghi, Ref. 1). The foundation therefore has to be broken up into a number of elemental rectangles. Each of the rectangles must have a common corner such that point N' is at this 'corner'.

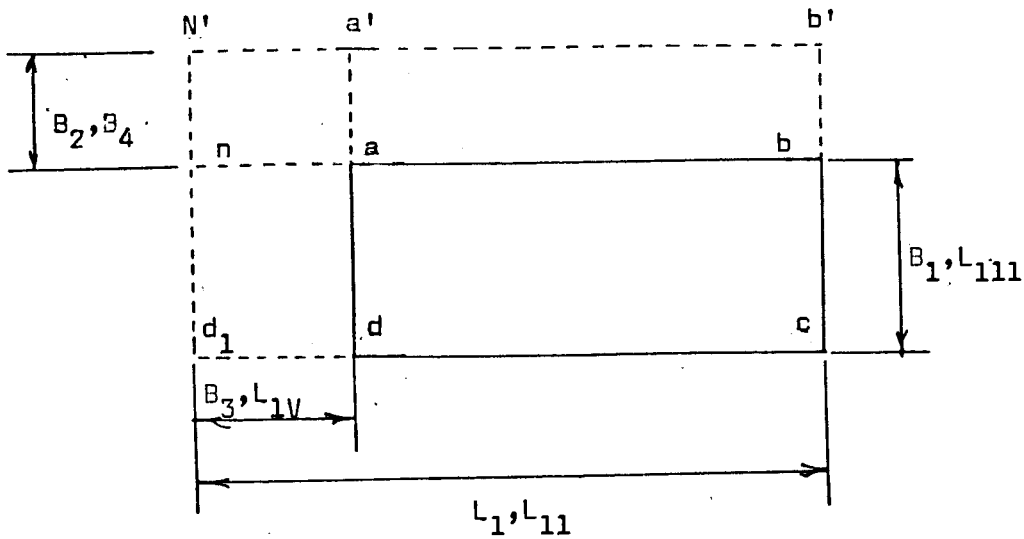


FIGURE 8.2 Point N for which the settlement prediction is to be made

8.3.1 Elastic formulae

In 1885 Boussinesq produced equations 8.5 and 8.6 for the vertical displacement and the horizontal displacement caused by a vertical point load at the soil surface and at internal points in elastic half-space (Terzaghi, Ref. 1).

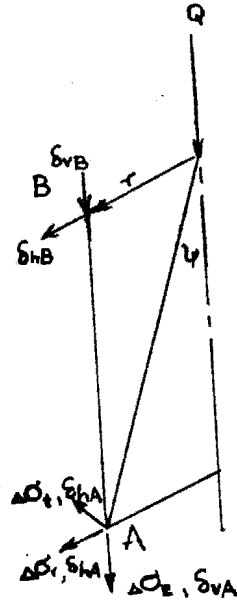


FIGURE 8.3 *Definition of stresses and strains associated with point load Q*

$\Delta\sigma$ = change in stress

δ = displacement associated with change in stress

Q = vertical point load

Sign convention:

δ_v ; positive downward

δ_H ; positive in outward direction

The displacements at point A are:

$$\delta_{vA} = \frac{Q}{2\pi r} \frac{1+\mu}{E} [2(1-\mu) + \cos^2\psi] \sin\psi \quad (8.5)$$

$$\delta_{hA} = \frac{Q}{2\pi r} \frac{1+\mu}{E} [-1(1-2\mu) + \cos\psi + \cos^2\psi] \sin\psi \tan\frac{\psi}{2} \quad (8.6)$$

Consider a point B at the surface (i.e. $\psi = 90^\circ$)

At B therefore, $\cos\psi = 0$

$$\tan\frac{\psi}{2} = 1$$

$$\sin\psi = 1$$

Therefore at B the displacements of the soil surface are:

$$\begin{aligned} \delta_{vB} &= \frac{Q}{2\pi r} \frac{1+\mu}{E} [2(1-\mu)] \\ &= \frac{Q}{\pi r} \frac{1-\mu^2}{E} \end{aligned} \quad (8.7)$$

$$\begin{aligned} \delta_{hB} &= \frac{Q}{2\pi r} \frac{1+\mu}{E} (-1 + 2\mu) \\ &= -\frac{Q}{2\pi r} \frac{1-\mu-2\mu^2}{E} \end{aligned} \quad (8.8)$$

Equations 8.7 and 8.8 are for the settlement prediction at the surface for a surface load (or at founding level) due to a point load applied to a soil mass.

Consider now a uniformly distributed load acting on abcd (Figure 8.2). Divide abcd into elemental areas ($dA = dx.dy$). On each of these areas a 'concentrated' load dQ acts ($dQ = qd.dy$). By integration the vertical strain at a single point can be obtained (see Figure 8.4). For $\psi = 90^\circ$; that is for conditions at the surface or at founding level, the settlement under the corner of the footing is:

$$\begin{aligned} \Delta\rho = \delta v &= qB \frac{1-\mu^2}{E} \frac{1}{\pi} \left[\ell \log \frac{1 + \sqrt{\ell^2 + 1}}{\ell} \right. \\ &\quad \left. + \log (\ell + \sqrt{\ell^2 + 1}) \right] \end{aligned} \quad (8.9)$$

where $\ell = \frac{L}{B}$

substituting

$$I_{\rho} = \frac{1}{\pi} \left[\ell \log \frac{1 + \sqrt{\ell^2 + 1}}{\ell} + \log (\ell + \sqrt{\ell^2 + 1}) \right] \text{ into 8.9}$$

gives

$$\Delta \rho = qB \frac{1 - \mu^2}{E} I_{\rho} \quad (8.10)$$

I_{ρ} is a pure number and is analogous to I_{σ} (see Chapter 4). Numerous charts have been drawn up for various ℓ and depth values (see Figure 8.4).

For circular areas

$$\Delta \rho = \Delta q \frac{R}{E} I_{\rho} \quad (\text{Lambe and Whitman, Ref. 2}) \quad (8.11)$$

For a circular area I_{ρ} is equal to $2(1 - \mu^2)$

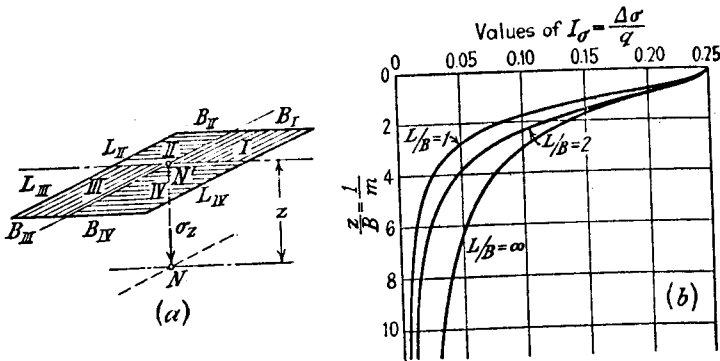


FIGURE 8.4 Influence coefficient for settlement prediction of rectangular loaded area

To determine the settlement (using equation 8.10) of point N' (Figure 8.2) the value of l for each of the rectangles $N'b_1cd_1$, $N'b_1bn$, $N'a_1an$, $N'a_1dd_1$ has to be calculated.

For the l values calculated I_ρ values are obtained from the chart (Figure 8.4). The settlement is then calculated as follows:

$$\rho = q \frac{1 - \mu^2}{E} (B_1 I_{\rho 1} - B_2 I_{\rho 2} - B_3 I_{\rho 3} + B_4 I_{\rho 4}) \quad (8.12)$$

The effects of the other rectangles are subtracted or added to the effects of the large rectangle.

In 1934 Steinbrenner modified the values (Lambe and Whitman, Ref. 2)

$$\Delta \rho = (1 - \mu^2) F_1 + (1 - \mu - 2\mu^2) F_2 \quad (8.13)$$

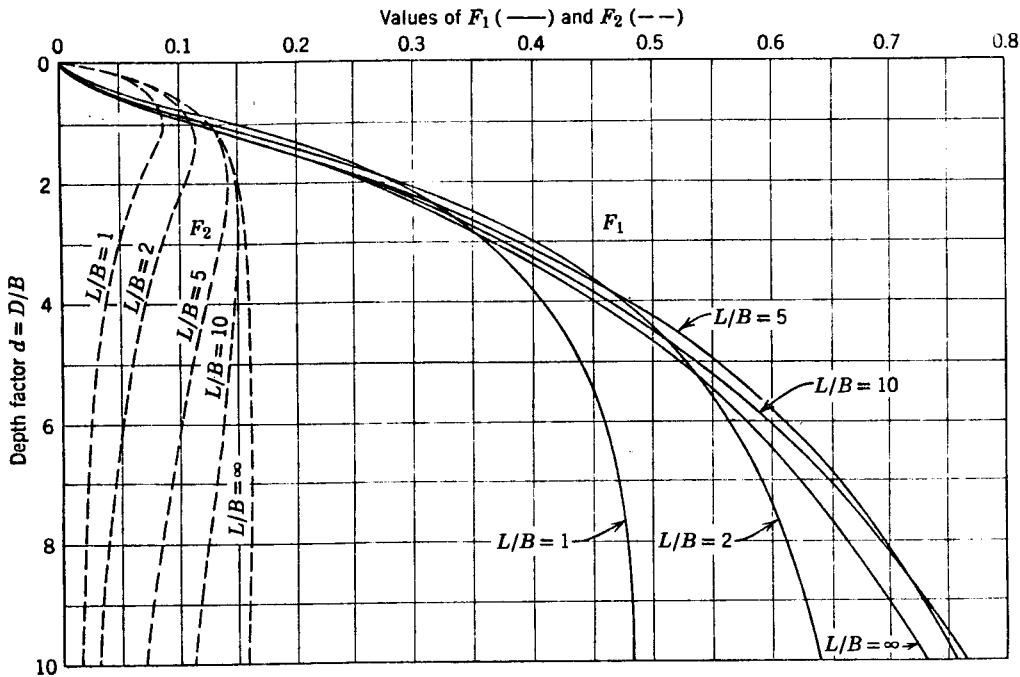


FIGURE 8.5 Steinbrenner's modification alters Figure 8.4 to the chart shown in Figure 8.5

8.3.2 Where an elastic method would be considered appropriate

1. Low cost structures where failure would not be catastrophic, or they do not involve large repair costs. Here accurate settlement prediction would not be justified (see flow chart Figure 7.7 Chapter 7). Plate loading tests (using square plates) can be conducted on typical soils to yield the factor $\left[\frac{1 - \mu^2}{E}\right]$ from equation 8.10. This could be done on a grid basis in a township by the local authority.
2. Where the behaviour of the soils produce an approximate linear relationship for $e - \bar{p}$ curves (for low $\Delta \bar{p}$ values). For single storey houses and similar types of structures where foundation loads are relatively small and the above condition is satisfied.
3. For the collapse settlement due to setting a soil under constant vertical loading (i.e. BC in Figure 8.6). Consider the stress path shown below.

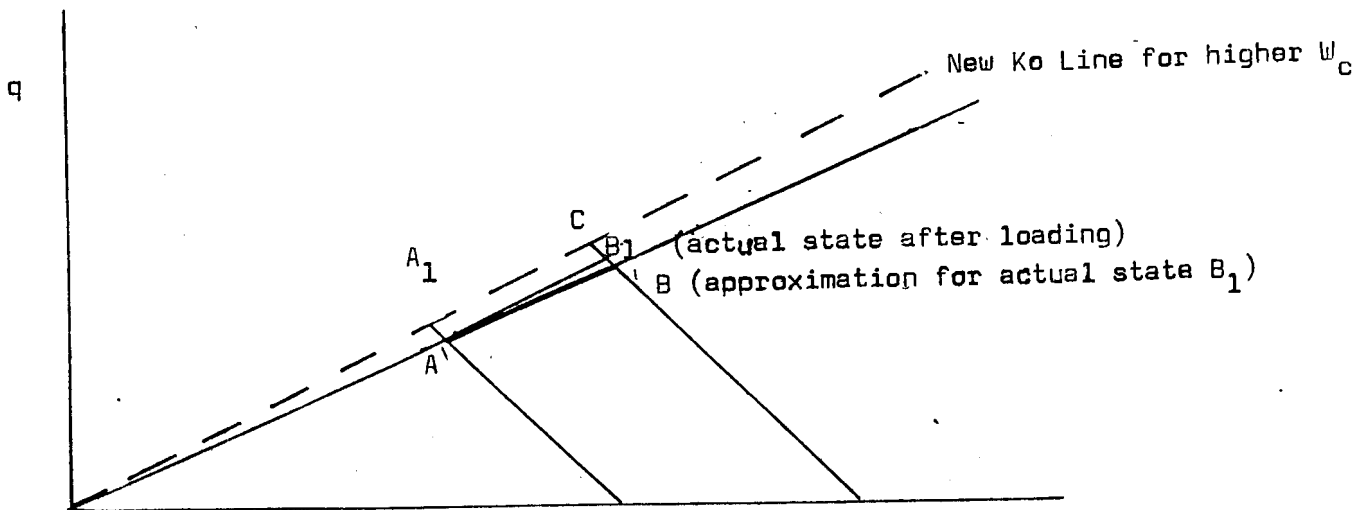


FIGURE 8.6 Typical stress paths (effective) for collapsing sands

Point A represents the initial in situ field stress state. Points B and B_1 represent in situ field stress states after loading, but at original field moisture content. The state B is the laboratory approximation for the actual field state B_1 . B_1 differs from the position of B because collapsing sands, being granular material, are associated with a slight horizontal deformation which differs from the K_0 conditions. This difference between B and B_1 is usually ignored, and for drained conditions, the stress path is approximated to the K_0 line (see Chapter 4).

At collapse due to wetting (defined in Chapter 2) there is no alteration in vertical loading, therefore $\Delta\bar{\sigma}_1$ remains constant. If $\Delta\bar{\sigma}_1$ remains constant, there is no variation in vertical stress in going from B to C in Figure 8.6. This implies that any changes in effective stress must be in the horizontal direction, and it can be concluded that the stress path BC must be at 45° to the horizontal.

If the final moisture content (as at state C) had been originally used in K_0 laboratory tests, the K_0 line OC would have had a different slope from the line OB. That is, the collapsing sand would have displayed the properties of a different material. Therefore the effective stress path being at 45° discloses that the only cause for variation in horizontal effective stresses, is a variation in the properties of the material.

8.4 Terzaghi's method of settlement analysis for the consolidation of a clay layer

Assumptions involved in this theory of consolidation are:

(Terzaghi, Ref. 1, Lambe and Whitman, Ref. 2, Lambe, Ref. 7).

- a. All the voids of the soil are completely filled with water
- b. The water and the solid constituents of the soil are perfectly incompressible
- c. Darcy's law is valid
- d. The coefficient of permeability (k) is constant

- e. Consolidation is entirely due to the low permeability of the soil
- f. There is lateral confinement and therefore no horizontal deformation
- g. The effective and total stresses are the same for every point in any horizontal plane through the clay for every stage of the consolidation process
- h. An increase in pressure from $\bar{\sigma}_{10}$ to $\bar{\sigma}_1$ will cause a change in void ratio from e_o to e . (e_o is the initial void ratio before application of surface loads, e is the final void ratio after consolidation).

Table 8.1 The coefficient of compressibility and coefficient of elastic recovery

Coefficient of Compressibility	Coefficient of Elastic Recovery
$a_{vc} = \frac{e_o - e}{\bar{\sigma}_1 - \bar{\sigma}_{10}}$ <p>where</p> $e < e_o$ $\bar{\sigma}_1 > \bar{\sigma}_{10}$ <p>e_o and $\bar{\sigma}_{10}$ are the initial values</p>	$a_{vs} = \frac{e' - e}{\bar{\sigma}_1 - \bar{\sigma}'_1}$ <p>where</p> $e' > e$ $\bar{\sigma} > \bar{\sigma}'$ <p>$\bar{\sigma}$ and e are the initial values</p>

From Table 8.1 a formula which relates the volume change to the stress change is produced.

$$e_o - e = a_{vc}(\bar{\sigma}_1 - \bar{\sigma}_{10}) \quad (8.14)$$

The initial volume of the soil block is $1 + e_o$.

Therefore:

$$\begin{aligned} \frac{\Delta e}{1 + e_o} &= \frac{\text{volume change}}{1 + e_o} = \frac{e_o - e}{1 + e_o} = \frac{a_{vc}(\bar{\sigma}_1 - \bar{\sigma}_{10})}{1 + e_o} \\ &= m_{vc}(\bar{\sigma}_1 - \bar{\sigma}_{10}) \end{aligned} \quad (8.15)$$

a_{vc} = coefficient of compressibility

a_{vs} = coefficient of elastic recovery

where m_{vc} = coefficient of volume decrease

From assumption f., $\Delta e/(1+e_o)$ is equal to the vertical strain. The settlement in Figure 8.7 would be the sum of each vertical strain multiplied by the corresponding vertical thickness of each horizontal layer.

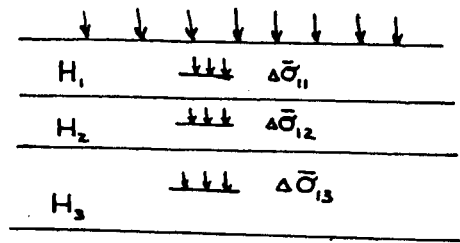


FIGURE 8.7 Determination of settlement of various soil layers

$$\text{Settlement} = \sum_{n=1}^n H_n \Delta\bar{\sigma}_{1n} m_{vc} \quad (8.16)$$

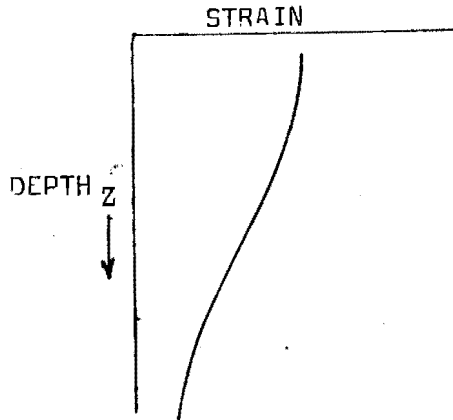
Substituting $\Delta\bar{\sigma}_{1n} m_{vc}$ = vertical strain = ϵ_{vn}

$$\rho = \sum_{n=1}^n \epsilon_{vn} H_n \quad (8.17)$$

From this Terzaghi produced his formula (1924) equating the settlement to the integral of the (strain x height), integrated from depth 0 to z (equation 8.18)

$$\text{Settlement} = \int_0^z \epsilon_v dz \quad (8.18)$$

where z is the depth below founding level.



Typical depth strain curve

FIGURE 8.8 Typical depth strain curve. Area of this diagram = settlement to some scale

8.4.1 Where Terzaghi's method would be considered appropriate

Consider the stress paths shown in Figure 8.9. Terzaghi states that the increment in vertical stress is equal to the initial change in pore water pressure.

$$\begin{aligned} \Delta u_o &= \bar{\sigma}_1 \text{ final} - \bar{\sigma}_1 \text{ initial} \\ &= (\text{distance } \Delta u_o \text{ in Figure 8.9}) \end{aligned}$$

Terzaghi also states that the shear deformation is zero and that the initial settlement is zero (Terzaghi, Ref. 1, Lambe, Ref. 7).

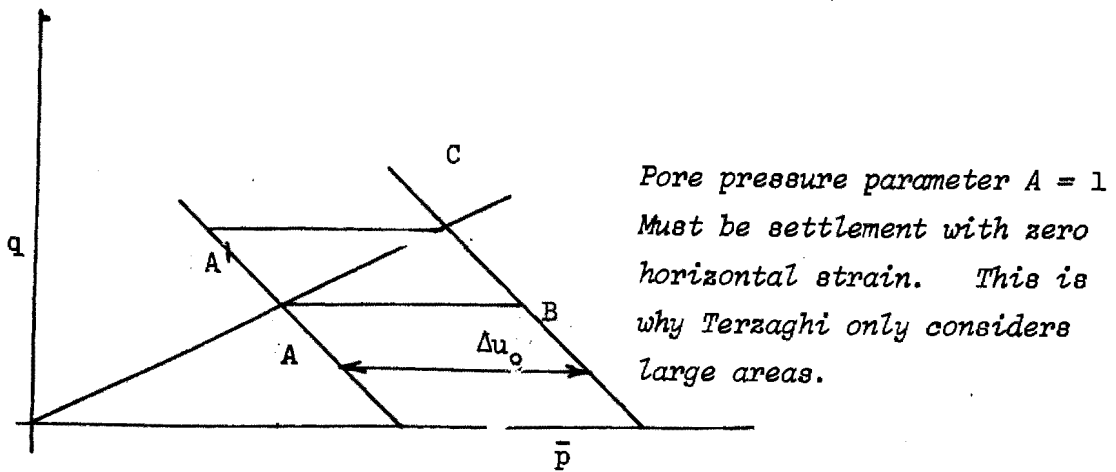


FIGURE 8.9 Stress paths for Terzaghi's method of settlement prediction

From the stress path it is obvious that there is an initial settlement. This settlement is not due to a change in vertical stress, but can be thought of as a shear settlement. Terzaghi looks at large loaded areas and therefore the shear settlement is kept to a minimum (compare shear movements at and the side of the footing in Figure 8.1). The stress path that should be followed for the consolidation settlement is A'C.

The stress path that is followed in the Terzaghi theory is AC. It should be noted that AC is the equivalent K_0 stress path if the pore pressure parameter A was equal to one.

From above it is deduced that Terzaghi's method is appropriate and relatively accurate for settlement prediction on cohesive soils subject to the following conditions.

1. The pore water pressure parameter $A \approx 1$ and $\Delta u \approx \Delta \sigma_1$
2. The shear strain is limited, that is a large loaded area is considered.

This method is not justified where a catastrophic failure might occur.

8.4.2 The fallacies of Terzaghi's method as revealed by using stress paths

The soil will show an initial settlement due to the fact that the change in pore pressure Δu can be defined via a pore parameter A (see equation 8.19). If the pore pressure parameter A is unity, then the stress path moves from point B to A in Figure 8.10.

From Chapter 7 it is known that the mode of deformation is relative to the stress path. From this it can be seen that each of the stress paths AC' , AC'' and AC''' (see Figure 8.10) must have different modes of deformation. Also assuming $A = 1$, the consolidation settlement determined by BD will only be accurate if:

- the field stress path is parallel to the K_0 line, and if
- the field stress path is relatively close to the K_0 line

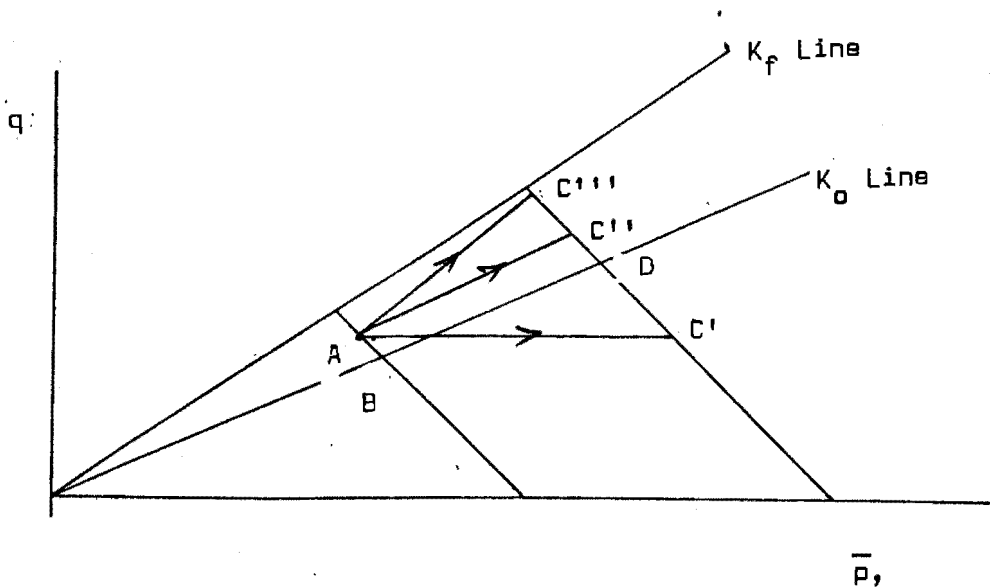


FIGURE 8.10 *Illustration of the fallacies of Terzaghi's method
BD is the equivalent K_0 stress path AC' , AC'' and AC'''
assuming that $A = 1$*

It is therefore evident that even in cases of field conditions approaching Terzaghi's boundary conditions for clay, his method should be approached with caution.

For relatively permeable material in which the release of excess pore pressure matches the rate at which loading is applied, the increase in pore water pressure is very nearly zero, the stress paths below might be obtained.

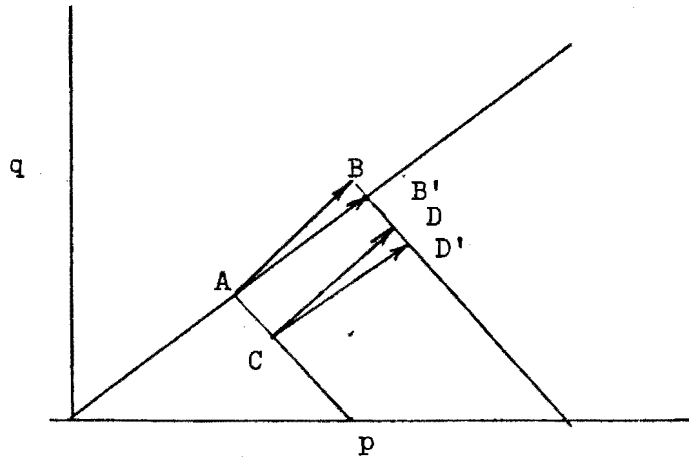


FIGURE 8.11 Stress paths for permeable soil (very little cohesion)

AB would be a typical stress path for an undisturbed (at zero) field condition. CD might be a typical stress path for a developed area where horizontal compressive strains have previously occurred due to the adjacent structures. The stress paths in both cases could be approximated by AB' and CD' respectively if the points B and B' and D and D' are relatively close to one another.

Therefore it can be concluded that the accuracy of this method is solely dependent upon the in situ effective stress path followed.

8.5 Skempton and Bjerrum method of settlement prediction

Skempton and Bjerrum considered the effects of pore pressure parameters on settlement prediction. The immediate settlement due to shear deformations was taken into account by recognising that in general $\Delta u \neq \Delta \sigma_1$

The formula introduced was:

$$\Delta u = \Delta \sigma_3 + A(\Delta \sigma_1 - \Delta \sigma_3) \quad (8.19)$$

The formula relates the change in pore water pressure to the change in horizontal stress plus a pore pressure coefficient A multiplied by the change in deviator stress.

In general it is found that $A \neq 1$ and therefore Δu cannot be equal to $\Delta \sigma_1$. If $A = 1$ then equation (8.19) becomes:

$$\begin{aligned} \Delta u &= \Delta \sigma_3 + 1(\Delta \sigma_1 - \Delta \sigma_3) \\ &= \Delta \sigma_1 \end{aligned}$$

(This is what Terzaghi considered to be accurate for saturated undrained soils - see section 8.4)

Skempton and Bjerrum then altered Terzaghi's formula for consolidation settlement to incorporate this modification.

$$\int_c = \int_0^z m_v \Delta u_z dz \quad (8.20)$$

(Consolidation settlement determined from excess pore pressures)

The Skempton and Bjerrum method of settlement prediction can be divided into three distinct stages (Lambe, Ref. 7, Davis Poulos, Ref. 6)

- a. Determining of excess pore pressures due to the total stress changes (i.e. the factor A)
- b. Determining the volume strains (i.e. vertical strain) due to excess pore pressures as determined from (a.). The volumetric strains are obtained in consolidometer tests in which $\Delta \sigma_1$ is applied such that $\Delta \sigma_1 = \Delta u$ where Δu is in formulae (8.20)

- c. Determining the settlement from the volumetric strains K_0 conditions are assumed, therefore the volumetric strain is equal to the vertical strain.

8.5.1 Critical examination of Skempton-Bjerrum method using stress paths

Consider the large cylindrical steel tank (see Figure 8.12). The maximum load imposed at the soil surface is equal to $-q$ kN/m^2 . To predict the consolidation settlement consider an average point H below the surface. (H being related to a depth D - see Chapter 4). For simplification assume that initially $\bar{\sigma}_1 = \bar{\sigma}_3$; and that the water table is deep. The initial change in vertical effective stress plus the original effective vertical stress $\bar{\sigma}_1$ due to the soil mass is $\bar{\sigma}_1$ initial.

$$\bar{\sigma}_1 \text{ initial} = \bar{\sigma}_1 + \Delta\bar{\sigma}_1 - \Delta U_{\text{initial}} \quad (8.21)$$

The final change in vertical effective stress $\Delta\bar{\sigma}_1$ plus the original effective stress $\bar{\sigma}_1$ due to the soil mass is $\bar{\sigma}_1$ final.

$$\bar{\sigma}_1 \text{ final} = \bar{\sigma}_1 + \Delta\bar{\sigma}_1 \quad (8.22)$$

$$(\Delta\bar{\sigma}_1 = \Delta\sigma_1 - U_{\text{static}} \quad \text{if } U_{\text{static}} \text{ is constant})$$

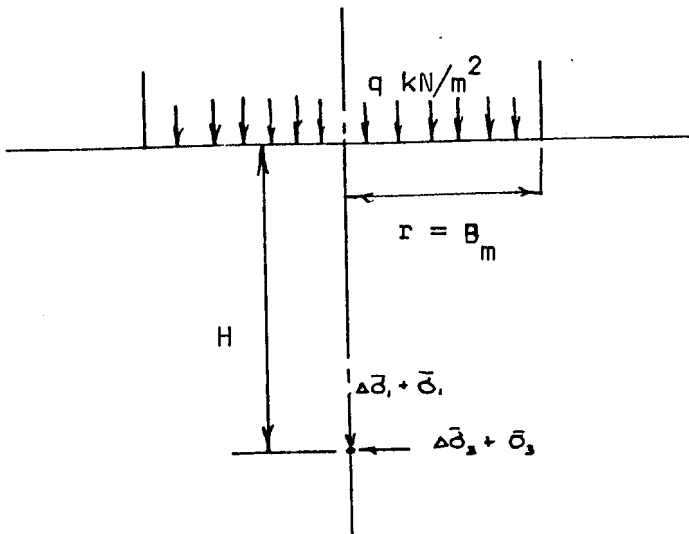


FIGURE 8.12 Illustration of Skempton-Bjerrum method using stress paths

The establishment of values for equations (8.21) and (8.22) are the first stage of the Skempton-Bjerrum method.

A soil specimen is now inserted in the consolidometer and subjected to a number of load increments. From the information obtained from the consolidometer tests an $e - \bar{p}$ curve can be plotted.

From the $e - \bar{p}$ curve $\Delta e / (1 + e_0)$ can be obtained for the required \bar{p} values ($\bar{\sigma}_1$). Since K_0 conditions are assumed, the vertical strain $\epsilon_v = \Delta e / (1 + e_0)$. Consider the stress path shown below.

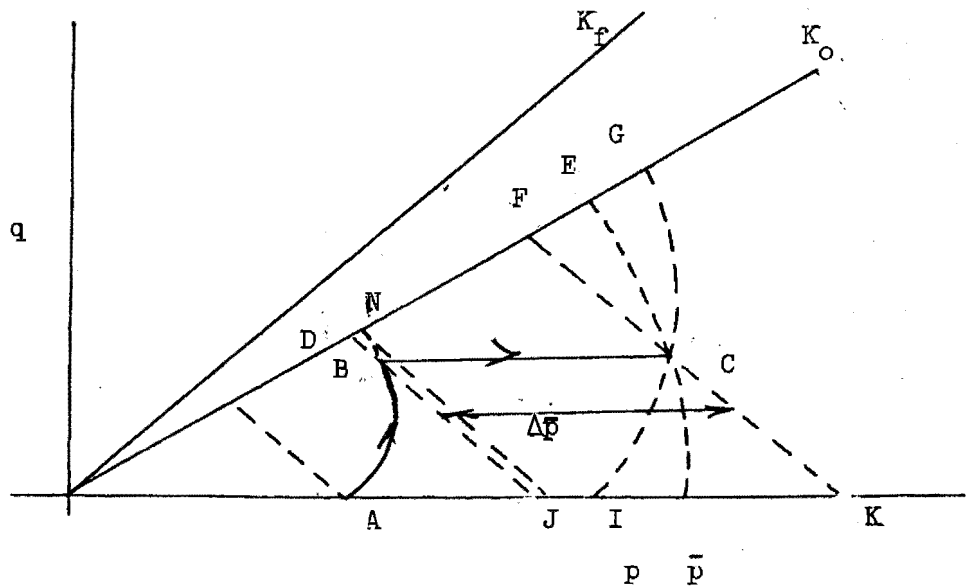


FIGURE 8.13 Stress paths for the discussion of the Skempton-Bjerrum method

The only stress states described by the Skempton-Bjerrum method for the problem in Figure 8.12 are A, B and C. Therefore the results of the settlement prediction are only dependent upon the pore pressures and pore pressure parameters. That is to say the shapes of stress paths between these points (A, B and C) are not important.

The actual field stress path (effective) which would be followed is ABC in Figure 8.12. BC would represent all the stress variations contributing to the hydrodynamic consolidation settlement.

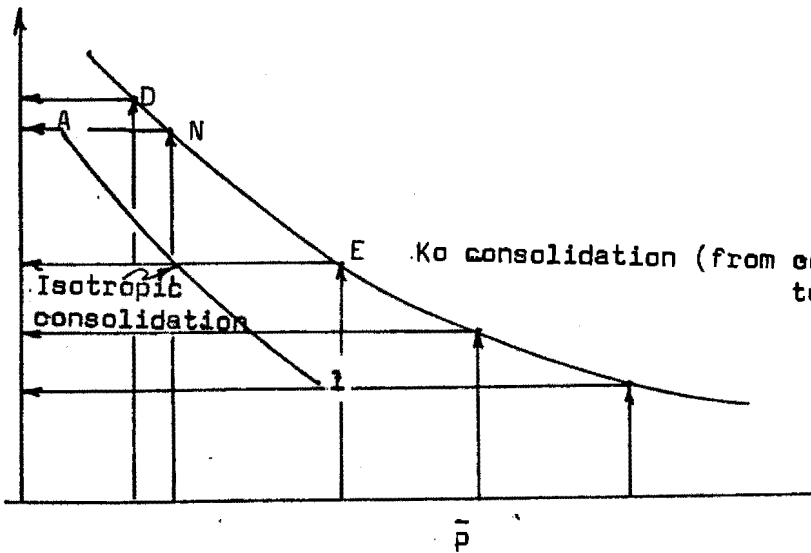


FIGURE 8.14 Typical $e - \bar{p}$ curves

With reference to Figure 8.14, from the Skempton-Bjerrum method the volumetric strain is $e_v - e_f / 1 + e_o$. In Figure 8.13, depending upon which is the undrained loading stress path through C, the equivalent portion of the K_o stress path for settlement prediction might be NE or NG. The Skempton-Bjerrum method and the stress path have the following similarities:

1. Both methods use pore pressure parameters (or field pore pressure measurement)
2. Both methods define identical points A, B and C
3. Skempton-Bjerrum use K_0 tests (i.e. their method does not require the use of stress paths) These K_0 test results can be used for certain stress path settlement predictions providing they are modified by using Lambe's formula (see Chapter 7).

The differences in settlement predictions arise because of the different methods of approximating K_0 conditions. To approximate the K_0 conditions Skempton-Bjerrum calculate $\bar{p}(\bar{\sigma}_1)$ for points B and C (Figure 8.13). Looking at the stress paths it can be seen that the equivalent construction will be lines at 45° from B and C to the horizontal axis and the K_0 line. The distance between the intercepts describes $\Delta\bar{p} = \bar{\sigma}_1 \text{ final} - \bar{\sigma}_1 \text{ initial}$ for consolidation and DF is the equivalent portion of the K_0 stress path. Once again a pore pressure parameter $A = 1$ is implied for this operation. Since immediately before this section attention was specifically drawn to the fact that $A \neq 1$ in general, the Skempton-Bjerrum method is open to criticism where accurate settlement prediction is required.

The difference between the Skempton-Bjerrum method and Lambe's stress path method (which follows the K_0 line) is that the K_0 consolidation test for the first method would follow stress path DF (Figure 8.13), while the Lambe stress path method would follow the stress path NE or NG depending upon the assumed undrained stress path through point C. The difference in results can be seen in the $e - \bar{p}$ plot in Figure 8.14. The points D, N, E, F, G in Figure 8.14 correspond to points which have the same labels in Figure 8.13.

8.5.2 Where the Skempton-Bjerrum method is applicable

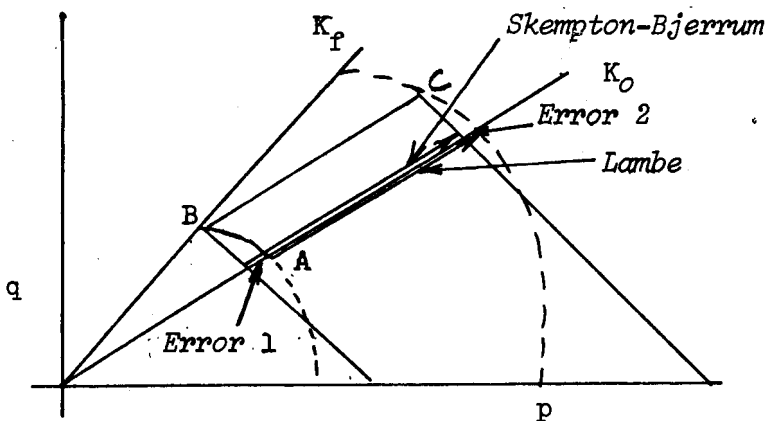


FIGURE 8.15 Stress paths to indicate when the Skempton-Bjerrum method is applicable

Figure 8.15 illustrates the differences between the Skempton-Bjerrum method and the Lambe stress path method. The Skempton-Bjerrum method would be applicable in the following instances:

- a) If after studying the stress path it is decided that Error 1 and Error 2 do not contribute any major effects to the settlement prediction
- b) Where failure is not catastrophic

To avoid criticism Skempton and Bjerrum would either have to adjust the testing procedures or draw undrained stress paths from B and C to the K_0 line to produce an effective K_0 stress path. Both of these solutions tend to approximate the stress path method of settlement prediction.

8.6 Davis Poulos method of settlement prediction

This is a three dimensional method of settlement analysis which relies on displacement theory for a homogeneous isotropic elastic body (Davis Poulos, Ref. 6). This method is similar to the other methods in that the settlement ρ , is composed of an immediate settlement, ρ_i , and a consolidation settlement ρ_c .

For rigid footings Davis Poulos assumes that the mean displacement is the average displacement under a flexible loaded area which settles in a parabolic shape. This implies that the centre and edge or corner displacements for a flexible footing define the mean displacement of a rigid footing.

For a circular rigid footing:

$$\text{Mean settlement} \approx \frac{1}{2}[\text{settlement centre} + \text{settlement edge}] \quad (8.23)$$

For a rectangular rigid footing:

$$\text{Mean settlement} \approx \frac{1}{3}[2(\text{settlement centre}) + \text{settlement corner}] \quad (8.24)$$

For a strip rigid footing:

$$\text{Mean settlement} \approx \frac{1}{2}[\text{settlement centre} + \text{settlement edge}] \quad (8.25)$$

(Davis Poulos, Ref. 6)

Davis Poulos suggested the following elastic type formula

$$\rho_i = \frac{qB(1 - \mu^2)I_\rho}{E} \quad (8.26)$$

$$\rho = \frac{qB(1 - \mu'^2)I_\rho}{E'} \quad (8.27)$$

(Davis Poulos, Ref. 6.)

These formulae are for rectangular footings in elastic isotropic materials which are homogeneous to great depths. Davis Poulos also refers to an average point (usually $\frac{1}{3}$ depth of D) which is based on the following reasoning.

- a) Extra vertical stress decreases with increasing depth
- b) Compressibility decreases with increasing depth

The following formulae (equations 8.28 and 8.29) are for odd shaped footings. They also apply to layered materials with properties which vary with depth.

$$\rho_i = \sum_{n=1}^n \frac{1}{E_n} \left[\Delta\sigma_{1n} - 0,5(\Delta\sigma_{2n} + \Delta\sigma_{3n}) \right] \delta h_n \quad (8.28)$$

$$\rho = \sum_{n=1}^n \frac{1}{E'_n} \left[\Delta\sigma_{1n} - \mu' \Delta\sigma_{2n} - \mu' \Delta\sigma_{3n} \right] \delta h_n \quad (8.29)$$

where

E' = Young's modulus of soil skeleton

μ' = Poisson's ratio for the soil skeleton

It should be noted that these values are for the appropriate stress changes within the soil mass.

I_ρ = Influence value in elastic displacement theory

B = Width of rectangular footing

μ_i = 0,5

E = Value obtained from the undrained triaxial test or the unconfined compression test

δh_n = Thickness of layer n

q = Stress at founding level due to design loads

$\Delta\bar{\sigma}_2$ & $\Delta\bar{\sigma}_3$ = Extra horizontal stresses due to foundation loading

$\Delta\bar{\sigma}_1$ = Extra vertical stress due to foundation loading

μ' and E' are found from the following formulae:

$$\mu' = \frac{\epsilon_1 \Delta \bar{\sigma}_3 - \epsilon_3 \Delta \bar{\sigma}_1}{\epsilon_1 (\Delta \bar{\sigma}_1 + \Delta \bar{\sigma}_3) - 2\epsilon_3 \Delta \bar{\sigma}_3} \quad (8.30)$$

$$E' = \frac{\Delta \bar{\sigma}_1 - 2\mu' \Delta \bar{\sigma}_3}{\epsilon_1} \quad (8.31)$$

8.6.1 Description of stresses and tests involved in the Davis Poulos method

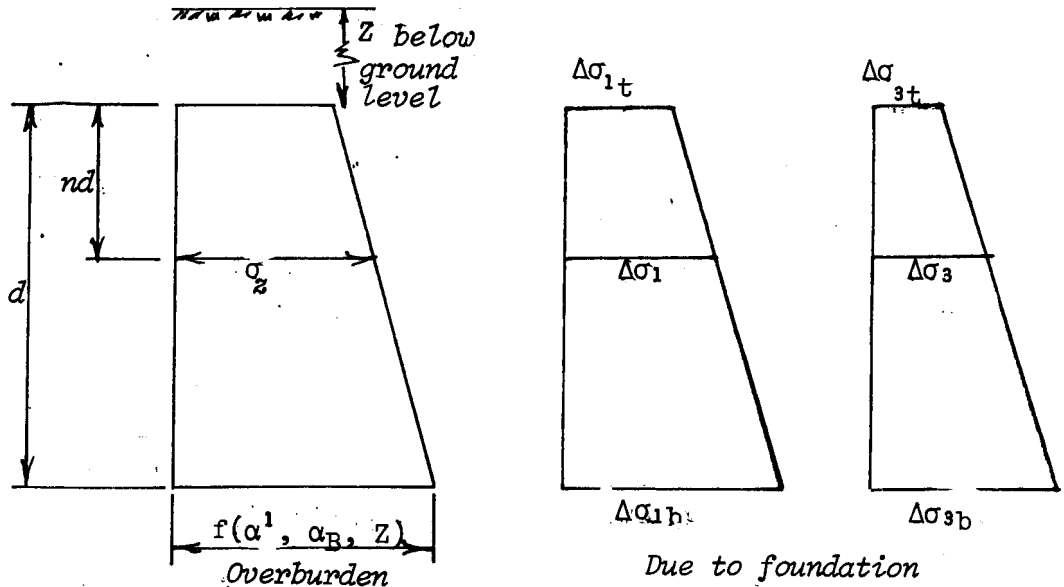


FIGURE 8.16 Stress distribution within a soil layer

$\Delta \sigma_{1t}$ is the vertical stress change at the top of the layer. $\Delta \sigma_{1b}$ represents the vertical stress change at the bottom of the layer. nd is a representative depth; it defines the average point. The factor n varies with the fraction $\Delta \sigma_{1b}/\Delta \sigma_{1t}$. For values of $\Delta \sigma_{1b}/\Delta \sigma_{1t}$ tending to zero, n tends to $\frac{1}{4}$. For values of $\Delta \sigma_{1b}/\Delta \sigma_{1t}$ tending to unity, n tends to $\frac{1}{3}$.

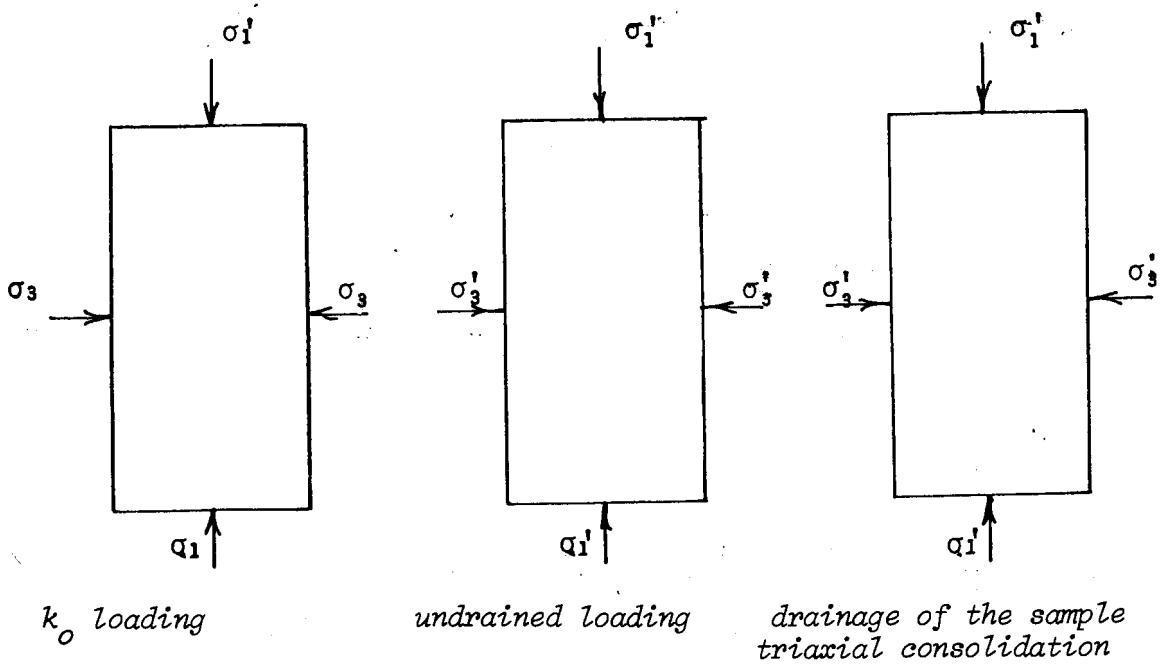


FIGURE 8.17 Defining the triaxial test sequence

σ_1 = vertical stress at depth z due to overburden

$\sigma_3 = K_o \sigma_1$

$\sigma_1' = \sigma_1 + \text{extra vertical stress at depth } z \text{ due to the foundation system}$

$\sigma_3' = K_o \sigma_1 + \text{extra horizontal stress at depth } z$

The axial strain (ϵ_1) and the volumetric strain (ϵ_v) are measured. From these values the horizontal strain [$\epsilon_3 = \frac{1}{2}(\epsilon_v - \epsilon_1)$] is calculated.

Applying all these values to the appropriate equations will produce a predicted settlement value for the foundation system.

It is obvious that the Davis Poulos method follows the field stress paths in the test procedures. The major difference between this method and the Lambe stress path method is that here the measured strains are not used directly. The information from the tests is rather used to define parameters such as E , μ , μ' , and E' . The exact field stress path is followed in the test procedure. This is difficult to achieve i.e. the

exact field conditions are simulated and then the direct strain results are ignored. It therefore seems to be a method which ignores the obvious route of integrating measured vertical strains.

CHAPTER 9

SOIL SAMPLING

9.1 Introduction to soil sampling

Once a testing procedure has been defined, it is necessary to obtain an undisturbed soil sample. There are three aspects to soil sampling:

- a) the design and use of the sample box
- b) the process of obtaining the soil sample and transporting it to the laboratory.
- c) the care of the sample once it has reached the laboratory

These three factors must be approached separately. Unnecessary emphasis laid on any one of them will in no way provide a better end result.

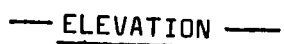
9.2 The design and use of the sample box

A sample box must be easy to assemble, able to protect the sample during transportation and provide the maximum possible support and protection to the sample once the sample has been opened. Figure 9.1 shows a working drawing of the sample box as designed.

From Figure 9.2 it can be seen that should the top of the box and side D be removed, the sample will still be protected and supported on three sides and the bottom. The box has been designed so that the remaining sides are always firm.

9.3 The process of obtaining a soil sample (Krynine, Ref. 8)

The necessary equipment for taking a soil sample is the sample box, spades, wax, a pot for heating the wax and a gas or parafin stove. The wax is heated to just over 60° C. This temperature will convert the wax to a liquid but will not cause blistering of the skin if the hot wax should come into contact with it.



— PLAN WITH COVER REMOVED —

FIGURE 9.1 Working drawing of the sample box

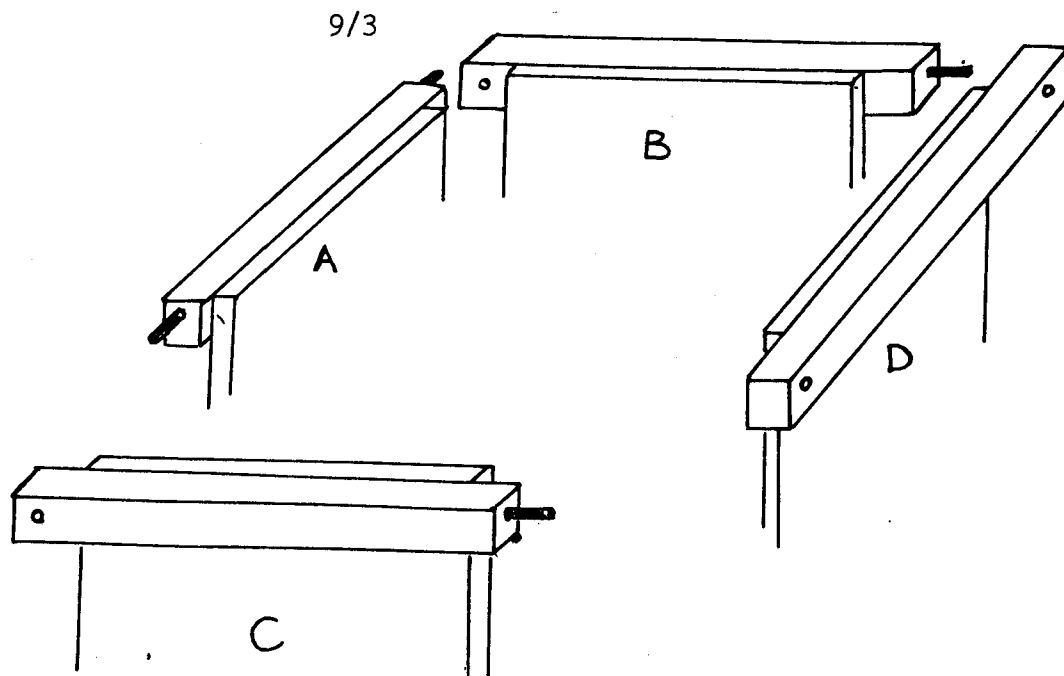


FIGURE 9.2 Assembly of the sample box

- a) stand side A upright
- b) push sides B and C onto the studs of side A
- c) push side D onto the studs of side B and C
- d) the covers fit on the open sides. Each cover has its own marking so that all the holes will be aligned

At the site where the sample is to be taken a 'tower' of soil is excavated. (see Figure 9.3). The sample box without the top or bottom is then fitted over this tower. The molten wax is poured into the 4 mm gap surrounding the sides of the soil sample. Once this operation is completed the top must be trimmed.

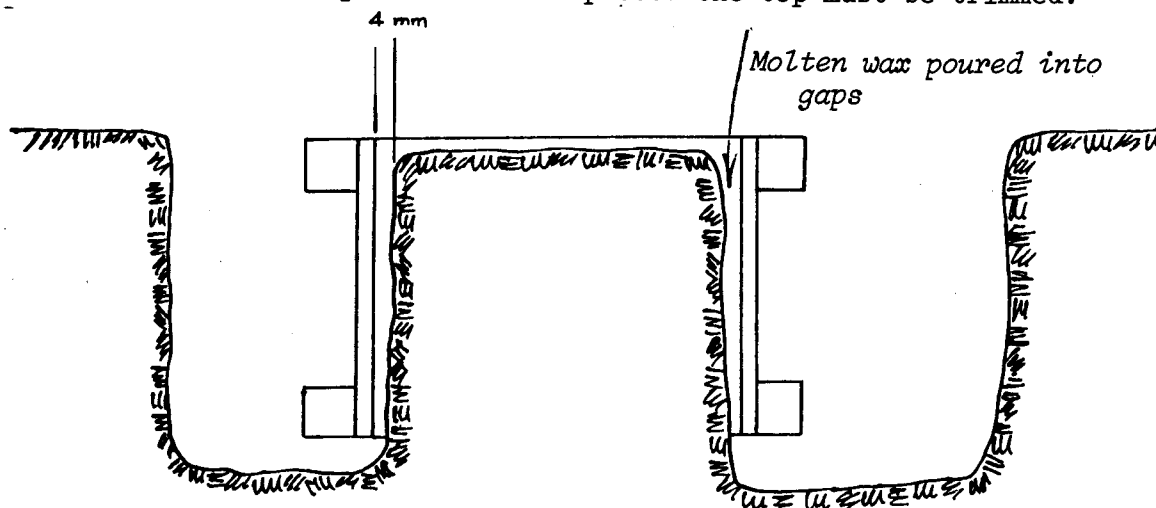


FIGURE 9.3 Excavation for the soil sample

Trimming the top of the soil must always be done from the sides inwards towards the centre (see Figure 9.4). This could be done with a small spade, but depending upon the material, a saw or piece of wire might prove much more useful. For the Constantia sample a saw and a small axe was used for the trimming of the sides and the edges of the sample.

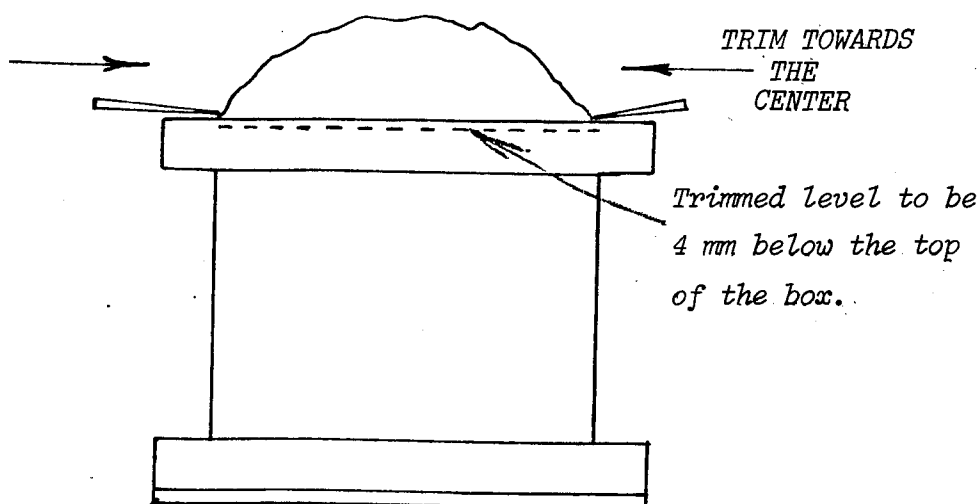


FIGURE 9.4 *Trimming the top or bottom of the sample*

After the top has been trimmed the wax must be poured over and levelled with the top of the sides of the box. Once the wax has cooled and hardened the top must be screwed tightly into place.

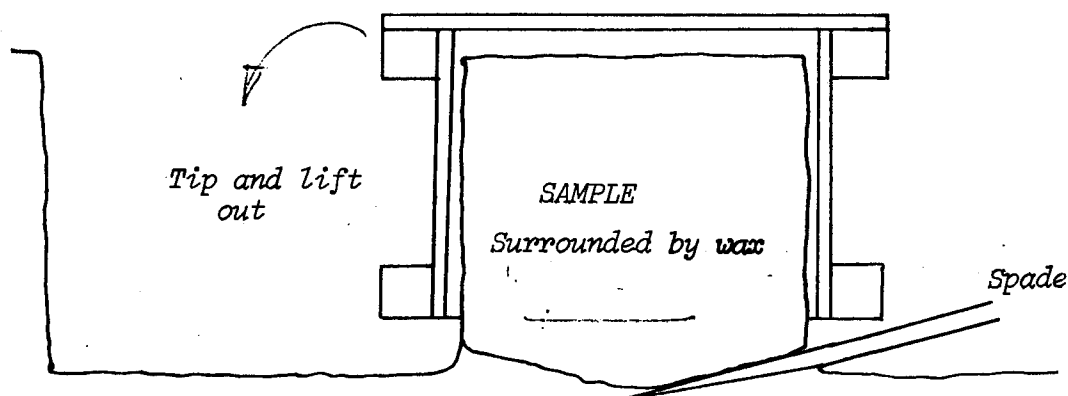


FIGURE 9.5 *Cutting off and inversion of the 'tower'*

The 'tower' must now be cut off. To do this a spade is struck at an angle under the one side of the box. The spade should be inserted until it is at least under the centre of the box. The sample and box are now tipped over and lifted out of the hole. It is now trimmed, waxed and sealed. It may now be carefully transported to the laboratories.

9.4 Caring of the sample after it has reached the laboratory

There are two main aspects of sample care, namely

- a) storing of the sample, and
- b) planning of sample usage

The sample should be stored in a place which allows free access to the user, but avoids general contact with the normal laboratory traffic. The protection that the sample box provides to the sample has already been discussed. Another precaution which might retard a continuous wetting or drying process due to long storage, is to wrap a large plastic bag around the open section of the sample.

The planning of sample usage is important for two reasons, the one is economics and the other is the availability of the sample. Depending upon the type of soil, one sample box should contain enough soil to allow most soil tests to be performed.

The soil sample for this thesis had to provide two consolidometer specimens, six to eight triaxial specimens and two or three model footing specimens. Figure 9.6 shows how the original sample was planned to accommodate these requirements.

9.5 Cutting out of individual samples for tests

Initially for tests, a rectangular piece of soil was cut off, (see Figure 9.7). The next step was to trim the sides down to the required dimensions after which the top and bottom ends were trimmed.

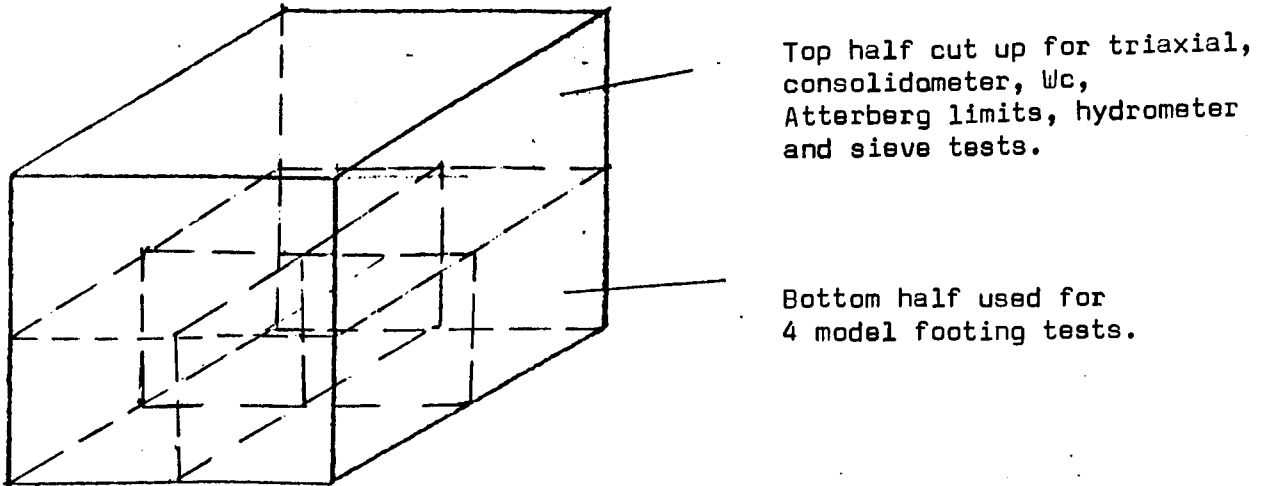


FIGURE 9.6 *Planning of sample usage*

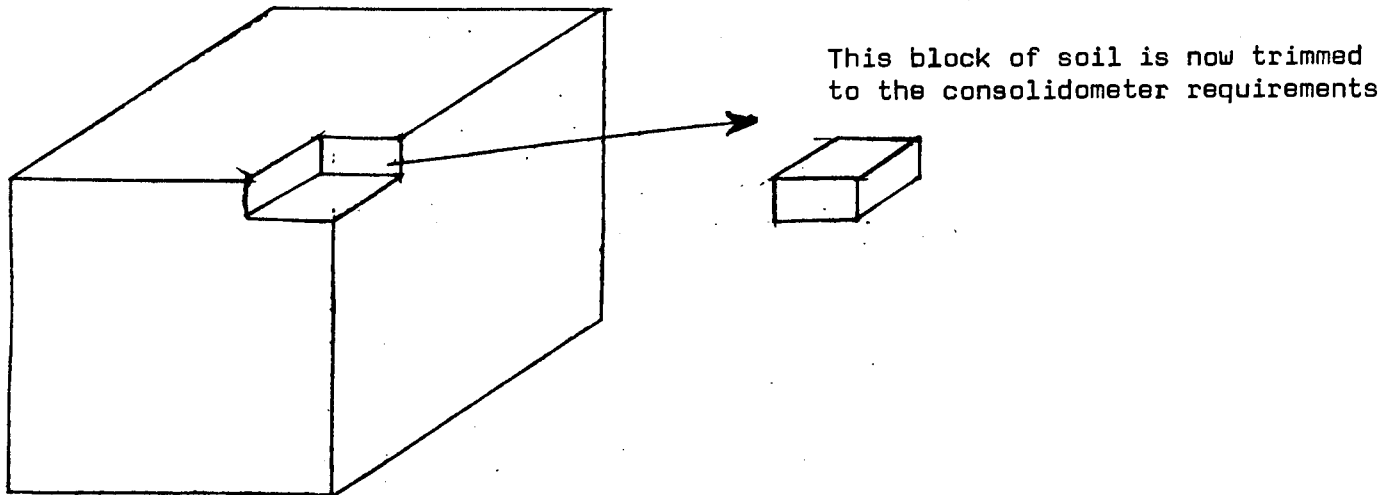


FIGURE 9.7 *First step in cutting out an undisturbed sample*

For the consolidometer tests the ring was put on a levelled surface of the soil block. The soil was then trimmed away from the sides of the ring. Ideally the trimming was carried on until the ring under the action of self weight slipped down over the cylinder of trimmed soil. The final operation was the trimming of the top and bottom of the sample.

Consolidometer ring slides down under the action of its own weight.

Sample trimmed down to the internal diameter of the consolidometer ring.

Sample top and bottom is trimmed towards the centre of the sample.

FIGURE 9.8(a)

Initial stages of trimming a consolidometer sample

FIGURE 9.8(b)

Final stage of trimming a consolidometer sample

For the triaxial sample a piece of apparatus which defines a vertical straight side and a horizontal cutting guide was used, (see Figure 9.9). Once the sides were approximately correct the sample ends were trimmed to their final sizes. Perspex discs were then placed on these ends and placed on a vertical line. Now the final trimming of the sides between these ends was done.

9.5.1 Berea road sample

This sample had been previously obtained by Professor Sparks. It had been air dried. There was only a very small piece of it left. From this a piece 90 mm x 90 mm x 40 mm was cut. For the initial cutting an ordinary hacksaw blade was used.

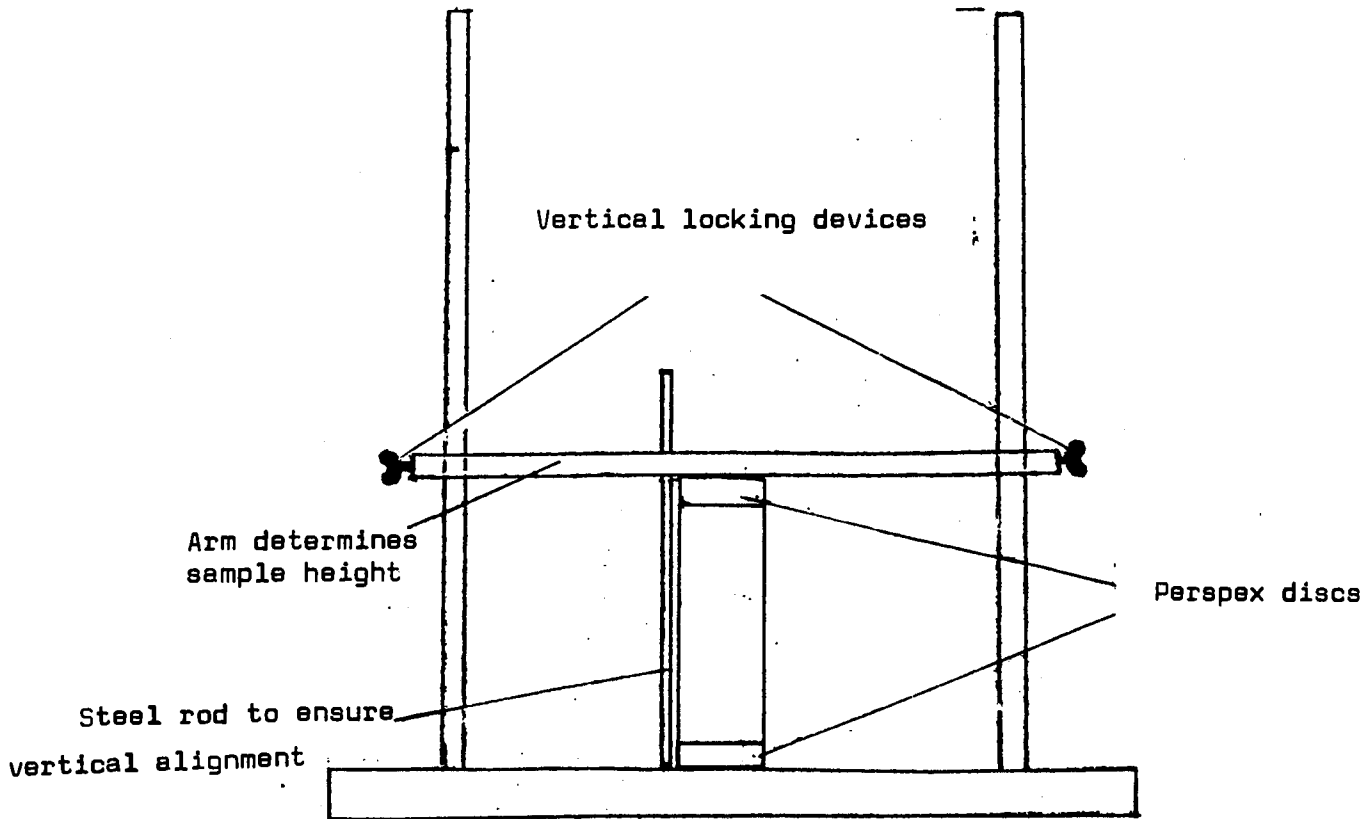


FIGURE 9.9 Apparatus used to cut out triaxial sample

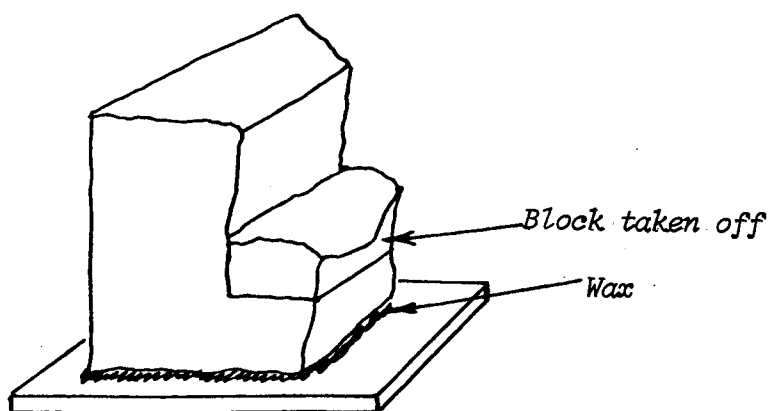


FIGURE 9.10 Berea road sample

For the trimming of the sides of the sample, old hacksaw blades were used. These old blades had been broken into lengths varying from 75 to 150 mm. The one side had the teeth on and the other was ground down to a knife edge which had a point.

The Berea road sample was the easiest sample to work with. It displayed relatively high cohesive properties and had no roots or large sized particles in it. The sample took approximately $3\frac{1}{2}$ hours to cut out.

9.5.2 Constantia sample (collapsing in situ decomposed granite)

This sample was obtained from the property 'Feathers' belonging to Mr P.A. Butters. The sample was taken at a depth of one metre and contained small amounts of roots. It has a large variation in particle size (see Chapter 2). The percentage of clay sized particles is very low and the material was therefore very brittle and tended to crack extremely easily. The sample was not sealed in wax as an immediate determination of field moisture content was initiated.

The original rectangles which had to be cut out had to be much bigger, approximately 120 x 120 x 50 mm, for the consolidometer and 110 x 50 x 50 mm for the triaxial specimens. The time taken for the cutting out of each sample varied from three hours to one and a half days for the consolidometer and six hours to three and a half days for each triaxial specimen.

The tools used for the trimming of the sample were hacksaw blades, parts of hacksaw blades, scribes and straightened paperclips. The excessive time taken to cut out samples was due to the fact that each large particle near the final surface had to be taken out separately. Three samples were lost because large stones were found in the centre of the specimens. It was also extremely difficult to obtain true end faces because of the voids left by the larger particles. These voids were filled with finer material. To get the triaxial specimens into the cell and ready for testing was another extremely delicate and tedious process.

9.5.3 The Sishen sample (collapsing windblown sand)

This sample was obtained by indirect means. The empty sample box was included in Mr W.M. Stern's air luggage to Sishen. There it was left together with the wax in the CSIR offices. Shortly after that Mr Donaldson from the CSIR took the sample. After taking the sample Mr Donaldson made arrangements with the main contractor, Murray and Stewart, to fly the sample down to Cape Town.

The sample was taken adjacent to an open trench excavation. The depth was approximately one metre. The wax that was sent up was not sufficient and the gap between soil and sample box was reduced to 3 mm.

The Sishen sample is a very loosely packed, weakly bonded collapsing sand. The samples tend to crumble very easily. The time taken to cut out the samples varied from three and a half hours to one day for a consolidometer sample and three and a half hours to one and a half days for each triaxial sample.

9.6 Conclusion

The three aspects of obtaining the undisturbed sample have been examined. It can be seen that each aspect should be given the same attention, as the end result is dependent directly on all three aspects.

The cutting out of the samples is a tedious but necessary process. The approach to the final trimming of the sample and the tools required is dependent upon the soil type.

The degree of sample disturbance is extremely important especially in cases where the increase in load is not high. It is therefore necessary to lay emphasis on this section of soil testing.

C H A P T E R 10

THE CONSOLIDOMETER

10.1 Introduction

The consolidometer can be used effectively for settlement prediction (see Chapter 8). Knight suggests the use of the consolidometer for collapse settlement prediction. The test he prescribes is the double consolidometer test. This test however is uneconomical in sample usage. The method described (Sparks, Ref. 12) enables settlement prediction for any combination of moisture contents to be determined using a single sample.

10.2 The consolidometer test for collapse settlement prediction

The double consolidometer test has two distinct disadvantages. The one is the uneconomical sample usage and the other is the lack of information of intermediate moisture contents other than the initial field moisture content and the final moisture content of the inundated sample.

To eliminate these disadvantages a method of testing, which could enable prediction of collapse settlement for any variation in moisture content, using only one sample had to be devised. The single sample therefore had to be wetted during testing. After each increment in moisture content there had to be a period in which the water could enter and distribute itself within the sample.

In order to vary the moisture content and simulate a field condition, a means had to be devised to limit the strain of the sample while the added water was still concentrated at the point of application and before it had distributed itself within the sample. The sample cannot be unloaded as repetitive loading and unloading cycles introduce the hysteresis effect. The system shown below was designed by Professor Sparks.

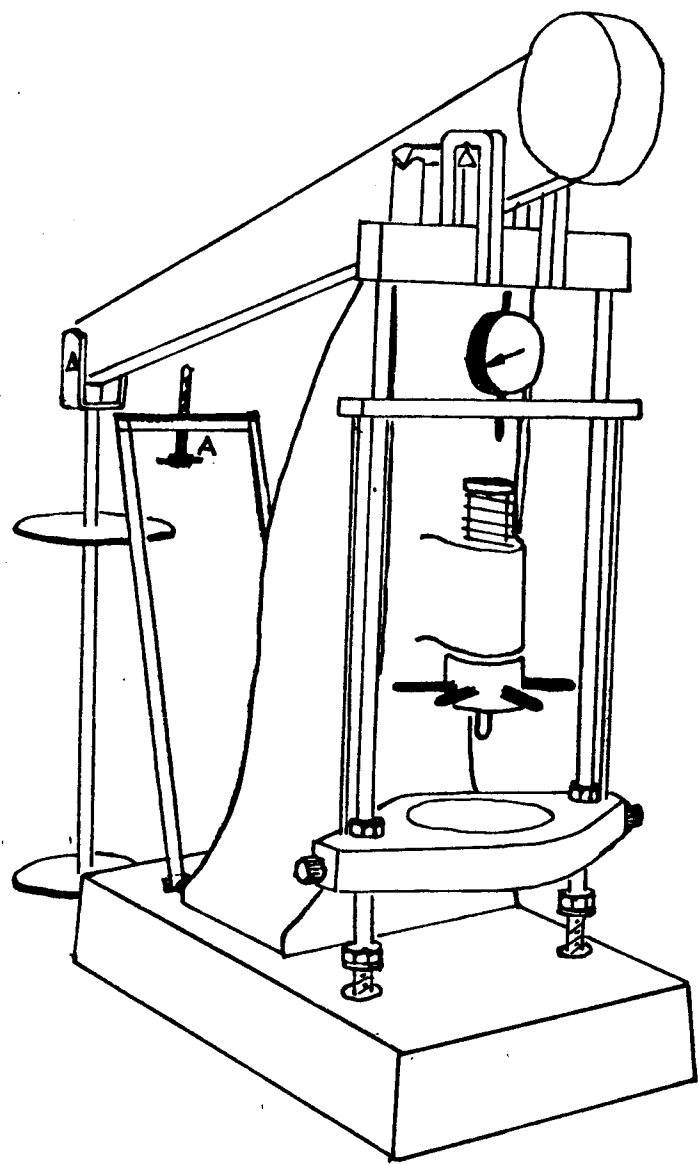


FIGURE 10.1 The 'collapse settlement consolidometer'

The arm with a screw device (A) is situated at the rear end of the consolidometer. This screw device can extend to the consolidometer arm. When it is raised or engaged it can either remove the load or simply limit the strain. For the limiting strain condition the screw is extended until there is a single division movement on the deflection dial gauge of the consolidometer.

The method for taking field samples, and the trimming of a consolidometer sample has been discussed in Chapter 8. Once the sample ring surrounding the sample has been placed in the consolidometer it is sealed with a plastic bag (see Figure 10.2). Access holes are made in four places around the sample. These hatches must be sealed when they are not in use (see Figure 10.2). This keeps the loss of moisture to a minimum during a test.

To add the water increments to the sample a syringe is used. The tube fitted to the syringe is passed through a hatch in the plastic covering to the filter paper at the bottom of the sample. The water is added in equal quantities at four points around the bottom of the sample. The water seeps into the sample via the filter paper. Weight corrections are made at the end of the test for the water retained within the filter paper, and lost by any evaporation.

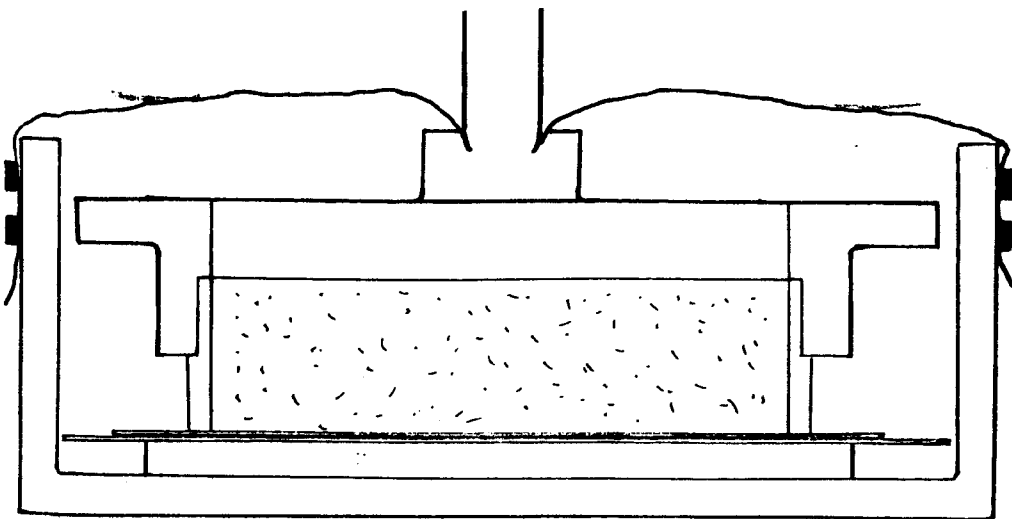


FIGURE 10.2(a)
Sealing of consolidometer sample

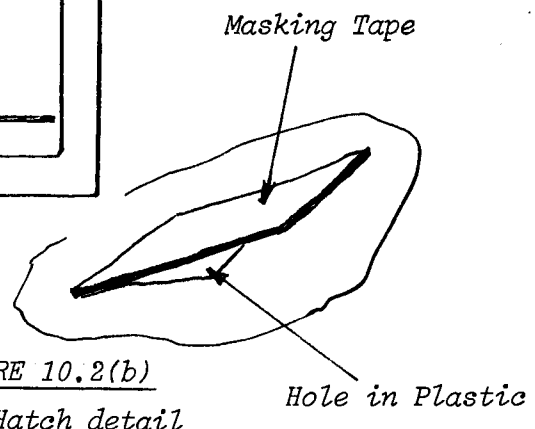


FIGURE 10.2(b)
Hatch detail

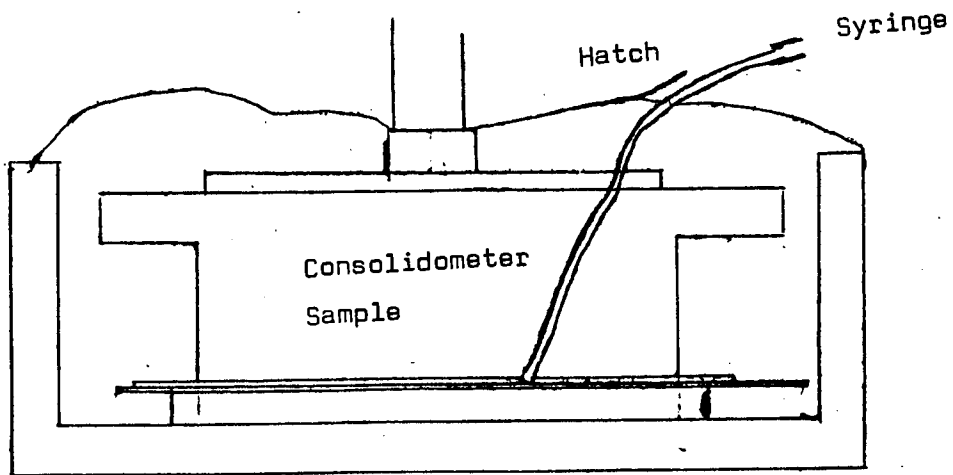


FIGURE 10.3 *Addition of water to consolidometer sample*

10.3 Test procedure

After it has been placed in the consolidometer and sealed, the sample is loaded at the original water content. The first load variations are zero to five pounds and five pounds to ten pounds (on the hanger). A load of ten pounds is equivalent to one long ton per square foot. The moisture content is kept constant during these loading operations.

After the ten pound load readings have been completed the strain is limited during the application of a water increment as previously described. The moisture content is then varied by adding water with the syringe at the four points around the sample. The amount of water added each time is predetermined and varies from one to two ml of water. The wetted sample is ^hthen allowed to soak for twenty four hours, after which the limitation imposed on the strain is released. A time-settlement curve is now observed until no further vertical strain occurs. Times up to three hours were required. The time intervals for loading of the sample should be kept as constant as possible as loading intervals do effect settlement prediction results.

Once the settlement readings for this new moisture content have been taken, the strain is once more limited. The moisture content is again changed and the sample is allowed to soak. The process is repeated until the total settlement due to increases in moisture content are negligible. The sample is then loaded to two tons/ft² and permitted to consolidate under this new load. Once this stage is reached the sample undergoes, at constant moisture content, the unloading cycle. The unloading cycle consists of two stages, i.e. two tons/ft² to a half-a-ton/ft²; and then to a zero pressure.

10.4 Determination of T_{90} and effective T_{90}

T_{90} is determined in the usual way for loading and unloading cycles. In Figure 10.4 the T_{90} for Berea Road soil is shown.

For a cycle which incorporates a change in moisture content there is an effective T_{90} value. This is not a true T_{90} value as there is no load variation associated with it. For consistency of results the writer attempted the start of new wetting cycles before secondary creep was evident (see Chapter 3) as secondary creep causes erratic results. However, in practice, secondary creep will occur in a soil, and should be allowed to occur in the laboratory tests. This would considerably lengthen the time of

testing, which was more than 2 weeks per sample using the above abbreviated method. Figure 10.5 shows how T_{90} and effective T_{90} values were obtained for Berea Road sample.

In Figure 10.5 the values of the deflection dial gauge readings are plotted along the vertical axis. These readings are referred to a common origin. Referring each set of readings to a common origin facilitates the plotting of the results and also allows easier comparison of results.

The T_{90} and effective T_{90} curves for the Constantia samples (from 'Feathers') show some peculiarities at the short loading times. It would appear as if the curves have a kink at the beginning. This could be a result of any of the following reasons:

- a) loading a thixotropic soil
- b) the rupture of the cementing of particles
- c) release of lateral side friction
- d) unequal wetting within the sample

10.5 Deciding when to stop the addition of water to the sample (Determining the limit of moisture content above which no further collapse occurs)

Ideally the moisture content should be varied from the field state to a state after which there is no collapse settlement under the design loading. To determine the latter stage accurately during experiments is difficult.

To overcome this problem a plot of $\Delta_W/(\Delta_W + \Delta_P)$ versus total water mass added is drawn during the experiment. Δ_W represents the deflection dial gauge difference between the start of the moisture content variation and the latest reading after settlement at the new moisture content. The amount of water added is the accumulative amount to the natural initial moisture added to the sample in mls. The additions of water should be stopped when the slope of the curve shown in Figure 10.7 approaches the horizontal.

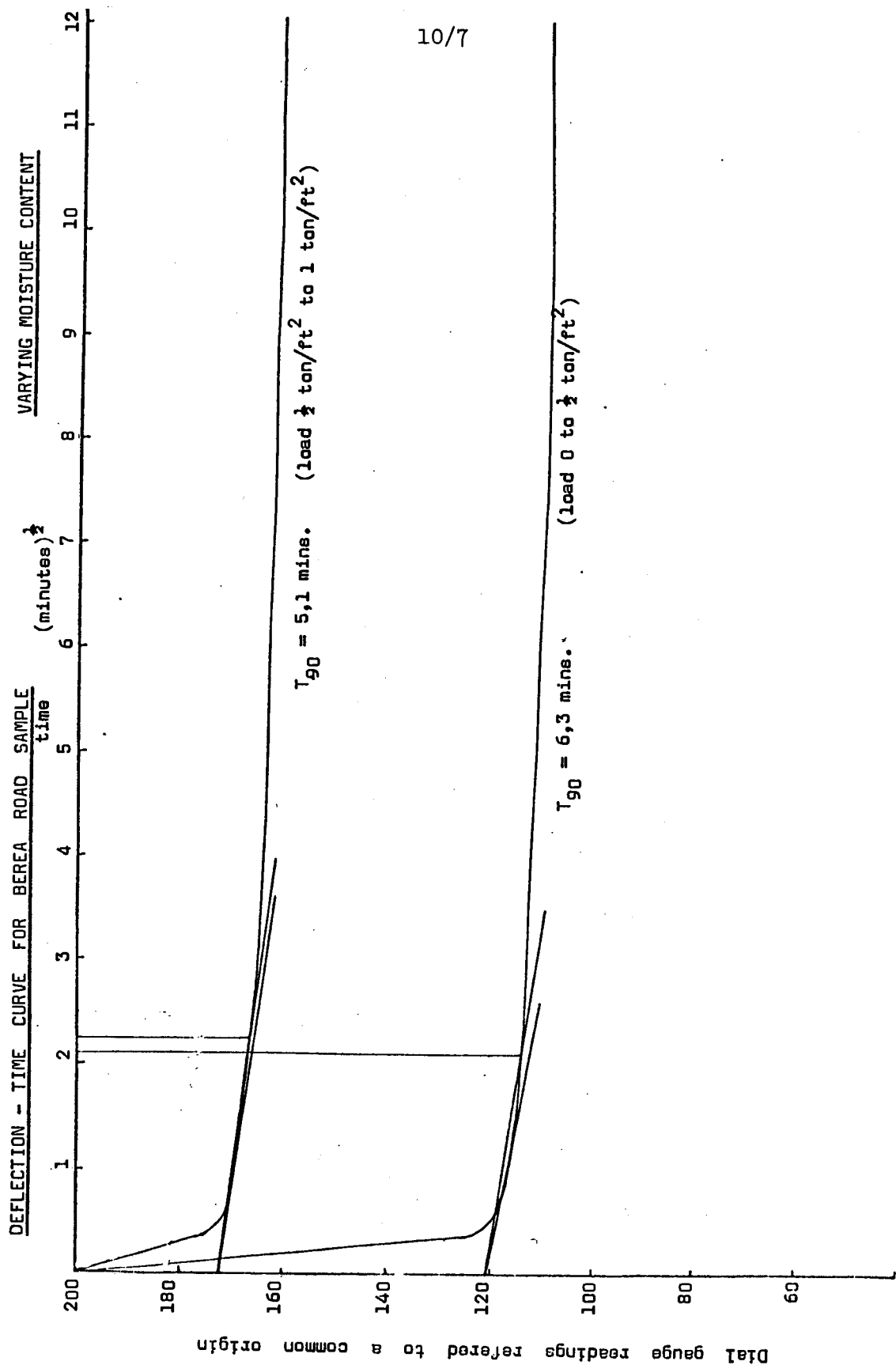


FIGURE 10.4 Time - Deflection curves for Berea Road sample
 (For each loading increment. Constant W_c
 i.e. before wetting)

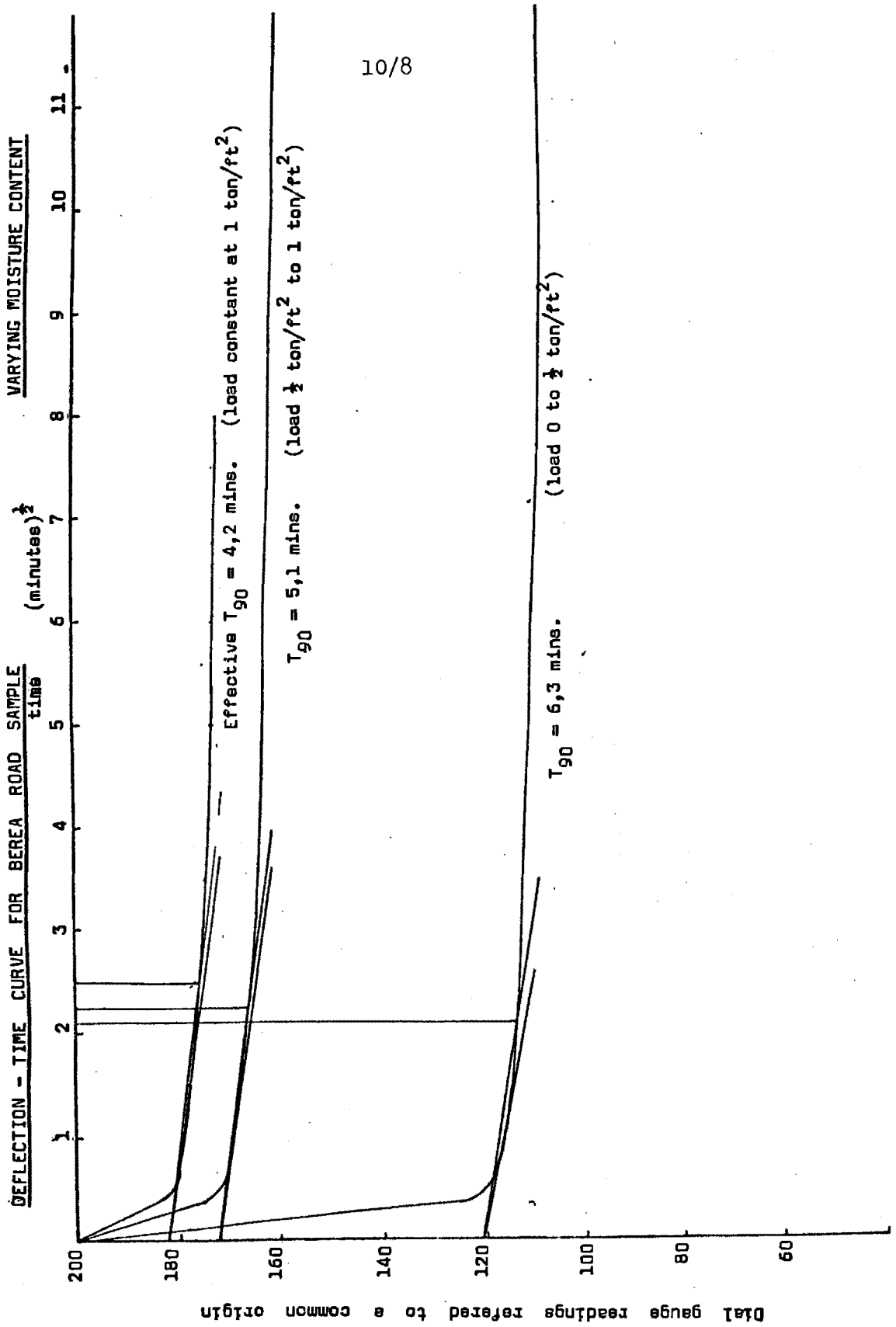


FIGURE 10.5 Time - Deflection curves for Berea Road showing T_{90} and effective T_{90} values
(For each load increment, or for each wetting increment at constant load)

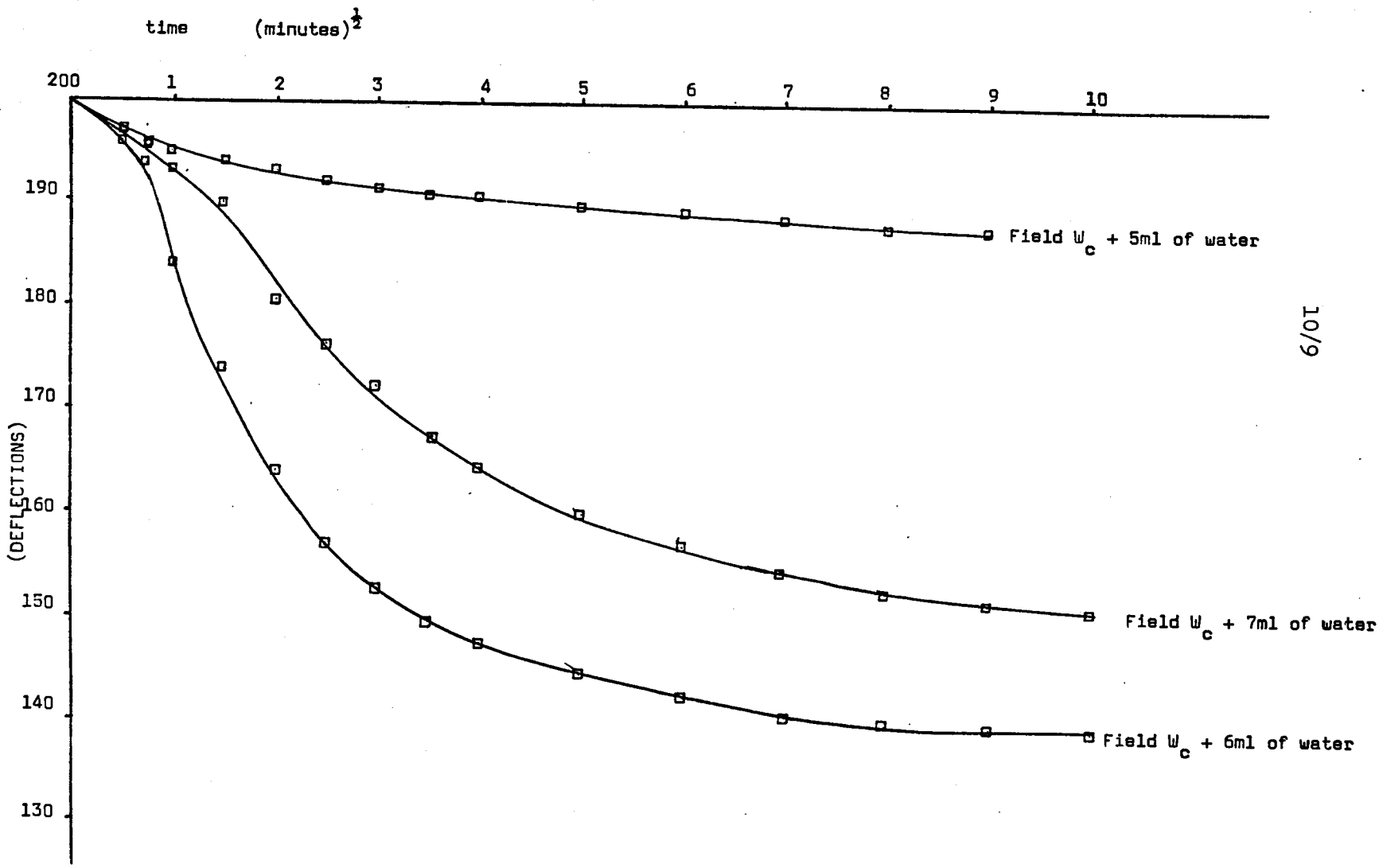


FIGURE 10.6 Time - Deflection curves for Constantia sample
(ex 'Feathers' farm)
(Wetting under constant load)

The effects of secondary creep must be controlled. By watching the time settlement curves under constant load for the moisture content variations it can be seen that the secondary creep produces a straight line of almost horizontal slope.

It is possible to observe the moisture content range over which collapse settlement occurs. The determination of the final moisture content beyond which collapse does not occur is shown in Figure 10.8. This is the water content at point X. If one waits for a period long enough to permit secondary creep of the wetted soil (under constant load), then the soil will show a larger collapse settlement Δ_w due to wetting. Hence the factor $\Delta_w/(\Delta_w + \Delta_p)$ is increased. Therefore the upper curve in Figure 10.8 is more correct than the lower curve which is observed in an abbreviated test in which loading or wetting increments are imposed before full settlement occurs due to secondary creep. Note that the upper limit of collapse water content has moved to the right from X to X'. The importance of the upper limit of collapse moisture content becomes obvious.

10.6 The void ratio-effective stress relationship

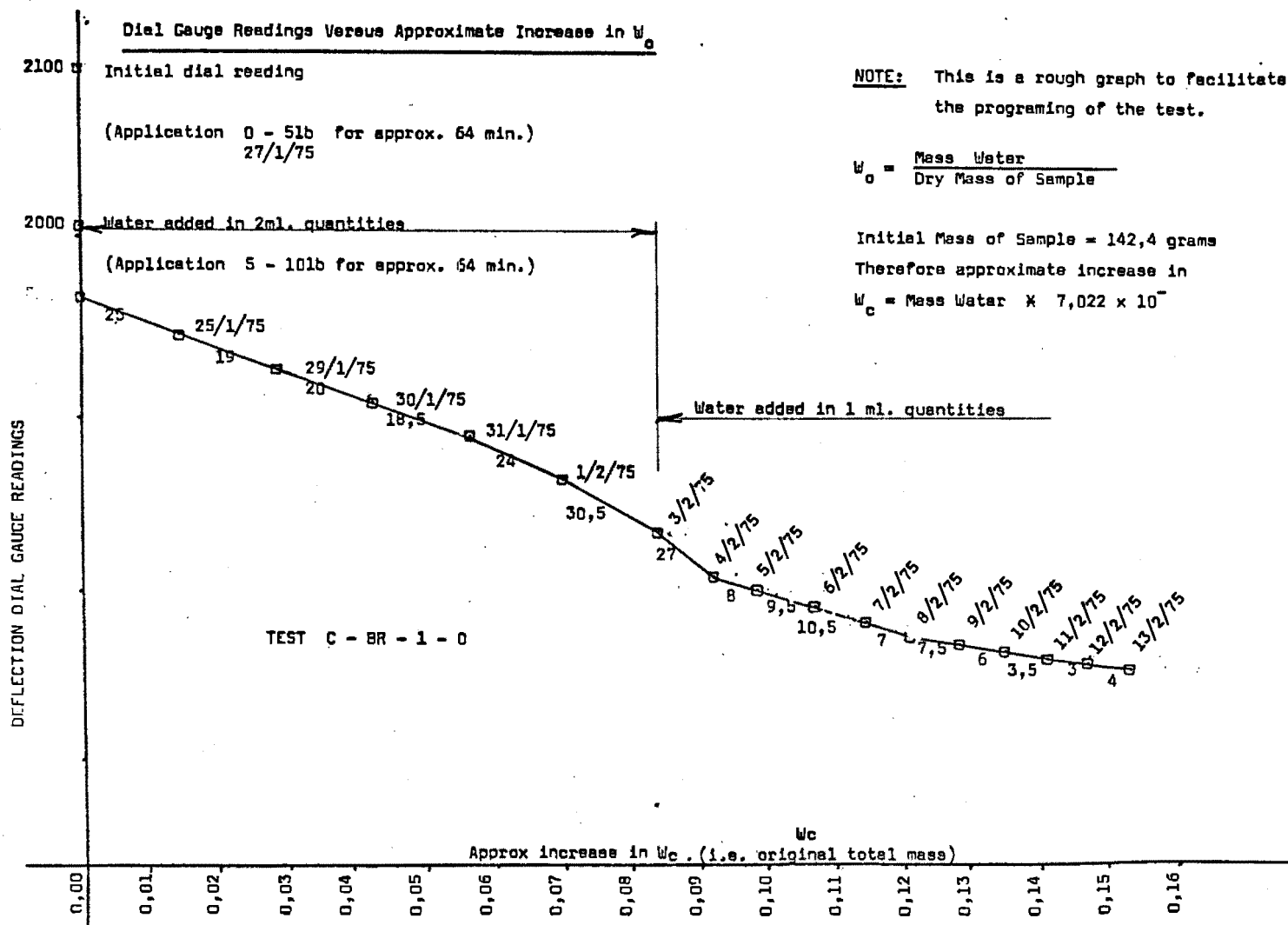
The one curve in Figure 10.9 is the $e - \bar{p}$ curve for the constant field moisture content, while the other is the one for the varying moisture content. The latter curve is important for estimating the possible collapse settlement.

The change in void ratio Δe_p is associated only with the variations in loading of the soil mass. The change in void ratio Δe_w is associated with the variation in moisture content. Therefore Δe_p represents the settlement due to the loading of the sample at constant water content while Δe_w represents the collapse settlement (see Chapter 2) for a specific moisture content variation. It must be noted that Δe_p is redefined for each initial moisture content.

For a certain collapsing soil, the higher the initial water content at loading, the larger the value of Δe_p and the smaller the subsequent value of Δe_w when wetting occurs up to the same water content. Taken to its natural conclusion, this implies that if the soil is saturated and loaded then total collapse will be immediately achieved. This method of precollapse was used by Robert Leslie and Partners at their Sishen contract.

FIGURE 10.7

Curve for determining the limit of moisture content above which collapse will not occur (under this constant vertical load)



$\Delta w / \Delta w + \Delta p$ - moisture content graph

Date	D	H ₀	e _s	e _u	% < 0,075 mm	Sample description	Clay content (%)	Test no.
18/2/75	75 mm	20 mm	0,712	0,636	19	collapsing sand	19	C-BR-1-0

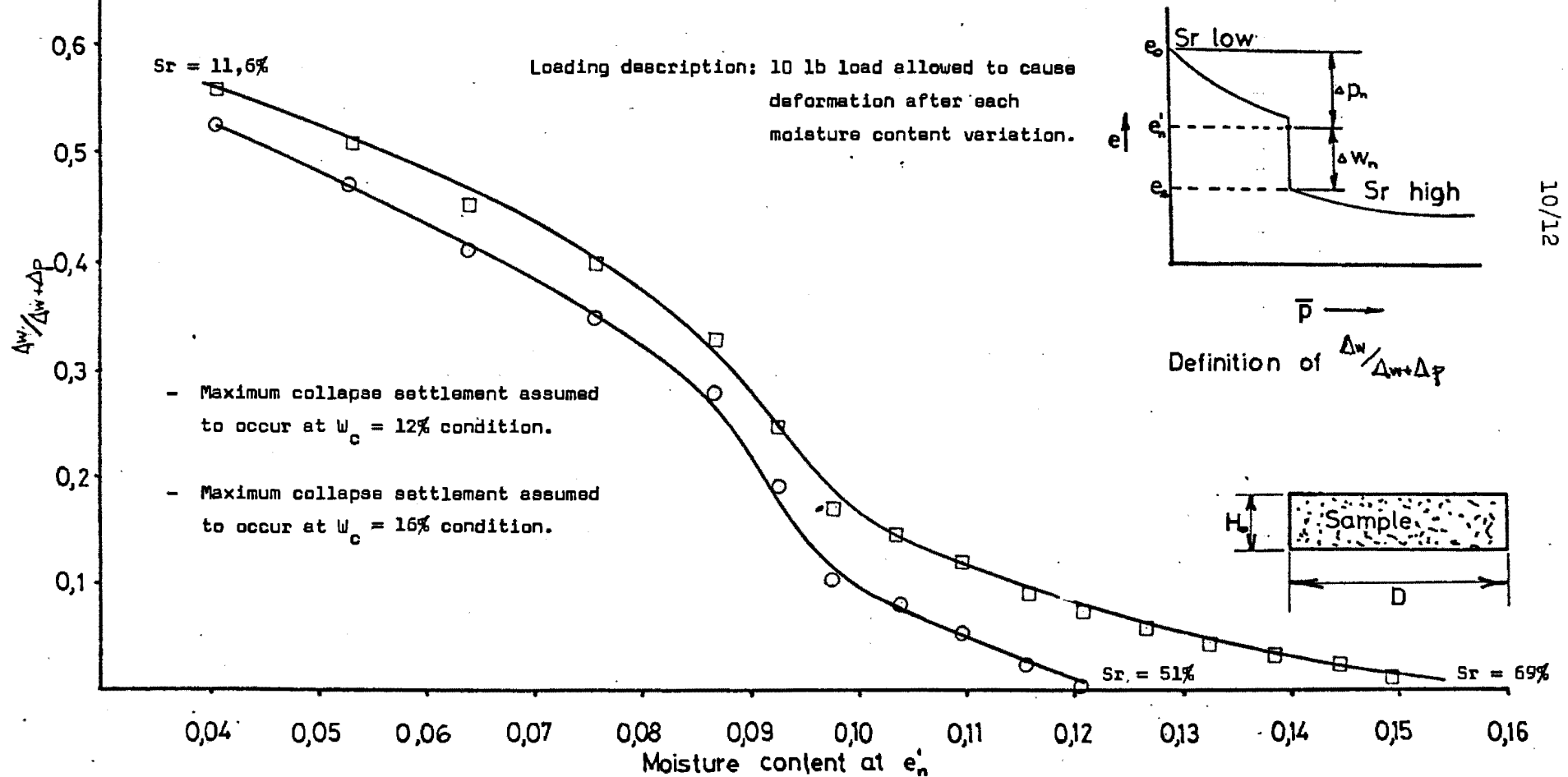
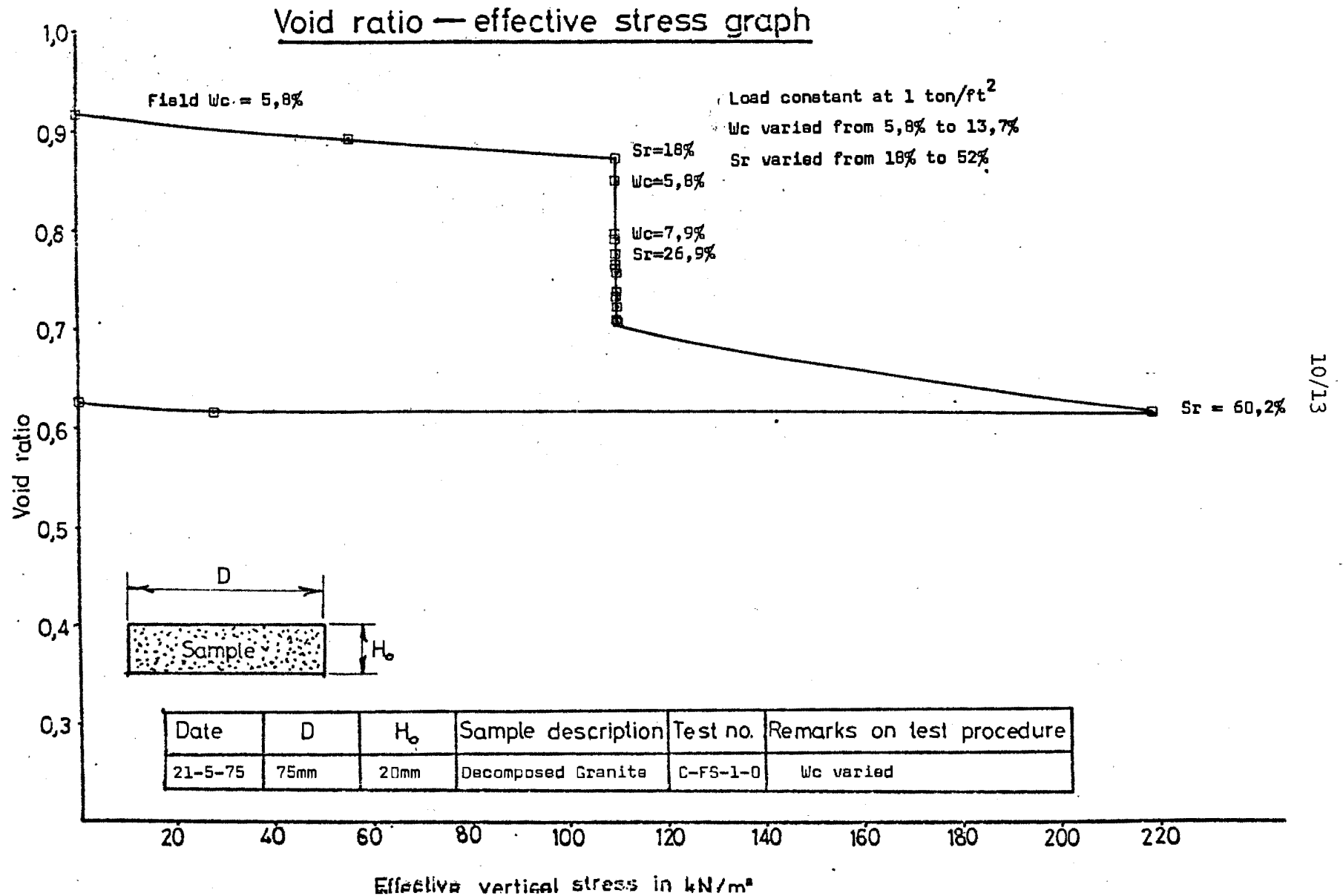


FIGURE 10.9 The $e - \bar{p}$ curves for the Constantia sample



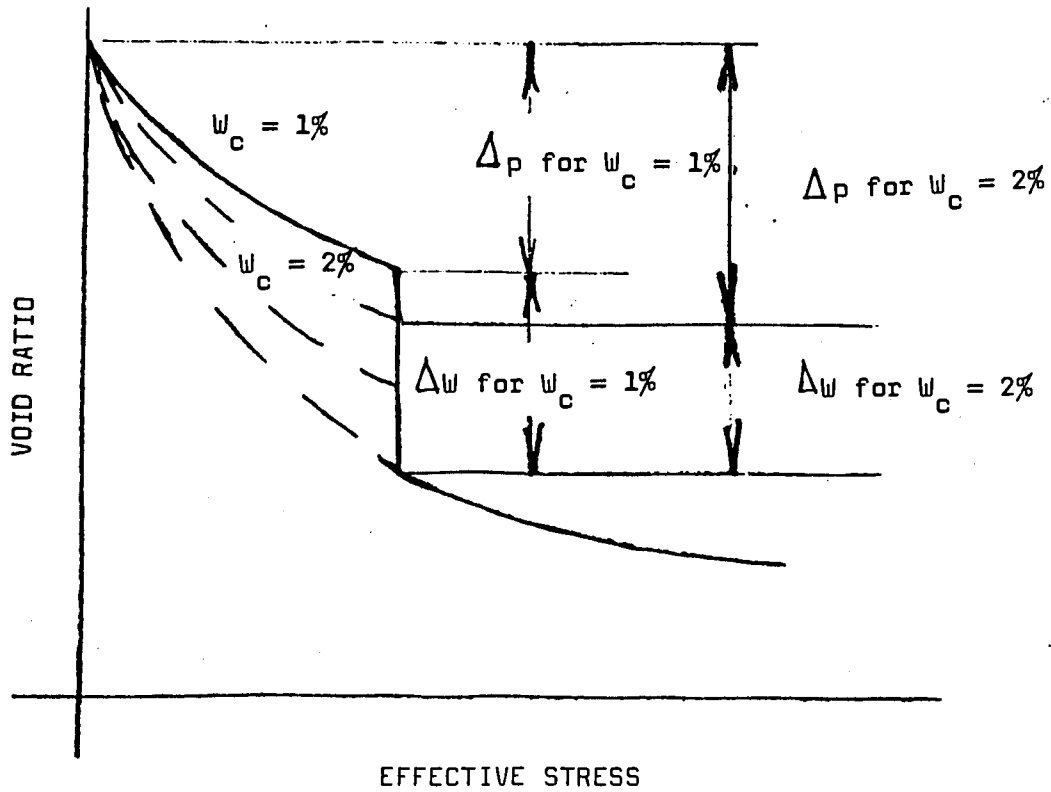


FIGURE 10.10 Definition of Δe_w and Δe_p

10.7 The accurate determination of moisture content throughout the test

a) Initially the following masses are noted:

Mass of consolidometer ring and sample at natural initial water content

Mass of consolidometer ring

Mass of porous plates

Dry mass of filter papers, clean plastic sheet

b) At the end of the test the following masses are noted:

Mass of consolidometer ring plus moistened sample

Mass of moist porous plates, moist filter papers etc

Mass of oven dried sample

- c) The clean plastic sheet is used to enclose the consolidometer sample in a moisture-tight system. To find the mass of other water present in this consolidometer system at the end of the test a piece of dry filter paper is weighed; the container, plastic sheet and enclosed fittings are thoroughly wiped dry and the filter paper is quickly weighed once more.
- d) Once the sample has been oven-dried the initial and final moisture contents of the sample can be exactly determined.
- e) A separate check is maintained of the water mass increments added via the syringe. Inevitably there will be a difference in this total and the change of mass of the sample (e.g. due to water lost from the system and on to fittings). The difference in the initial and final masses of the porous plates, filter papers and plastic will be the total mass of water retained by them. This mass of water is added to the amount of water (by mass) added to the sample as found in step (d). The difference between this mass of water and the mass of water added by the syringe represents the water lost during the experiment. This value varied from 0,3 to 1,0 ml over a period of about two to three weeks.
- f) When estimating intermediate water contents from the initial water content and the syringe increments, it is necessary to deduct some portions of this small mass of water which has been lost from the system.

These corrections can be made by assuming that the amount of water lost from the system in a certain period is either:

- i) Proportional to the length of period, or
- ii) Proportional to the total mass of water present in the system during this period, or
- iii) Proportional to the product of the length of period and the total mass of water present, or

- iv) Proportional to the amount of water added each time if water evaporates mainly when it is lying as a pool of free water which is being absorbed by the soil and porous plates via the filter paper.
- v) Proportional to the total mass of water in excess of natural or initial water content.

In certain research at UCT, the systems (i), (ii) or (iii) are used. The writer however decided to use method (v). Note that the correction values are very small and the method used does not significantly affect the results.

To find the intermediate values of moisture content a correction factor had to be applied. This correction had to take into account the difference in water masses described. For each time period, this factor was assumed to be directly proportional to the total mass of water in excess of the natural water content at the beginning of the time period.

$$C_f = \text{Correction factor} = \frac{\begin{array}{l} (\text{initial mass of water in sample} + \\ \text{the mass water added by syringe}) - \\ (\text{final mass of water in sample}) - \\ (\text{water mass in porous plates, filter} \\ \text{paper}) \end{array}}{(\text{Total mass of water added by syringe})}$$

This correction factor is per millilitre of water added. Therefore the actual amount of water in the sample at any stage is;

$$[(\text{the initial mass of the water in the sample}) + (\text{the total mass of water added by syringe}) - (\text{the total mass of water added}) \times (\text{the correction factor})]$$

$$\text{Actual amount of water in the sample} = \text{Initial mass of water in the sample} + (1 - C_f) \times \text{mass of water added to the initial condition.}$$

10.8 Computer program for the results

A computer program was drawn up to process the results of the tests. The program can be seen in Appendix B (page B/24)

The input data consists of the masses described, the number of stages associated with the test, the masses of water added and the deflection dial gauge readings. The output data includes the initial masses, volume and moisture content of the sample, the corrected moisture contents, the void ratios, the loading descriptions and the deflection dial gauge readings.

10.9 Conclusion

The advantages of this type of consolidometer test as compared to that of the double consolidometer test are listed at the beginning of the Chapter. The amount of information gained from a single test is not only plentiful, but also of great importance to the geotechnical engineer. The test procedure is simple, and the results are easy to interpret. The test helps to clearly define the range of water contents over which collapse settlement will, or will not occur due to wetting. In addition the method provides approximate void ratio versus effective pressure field curves for a large range of water contents.

CHAPTER 11

TRIAXIAL TESTS

11.1 Introduction

Tests were performed to find the soil parameters and settlement characteristics of collapsing soils. The tests departed in many cases from standard procedures. The versatility of the triaxial machine was emphasized.

11.2 Stress path tests for settlement prediction

Stress paths were followed to satisfy settlement requirements for 1 x 1 metre, 2 x 2 metre and 3 x 3 metre square footings (all at one metre founding depth). The stress paths and the approximated stress paths are shown in Figure 11.1. The validity of using the approximated stress paths is discussed in chapters 4 and 7.

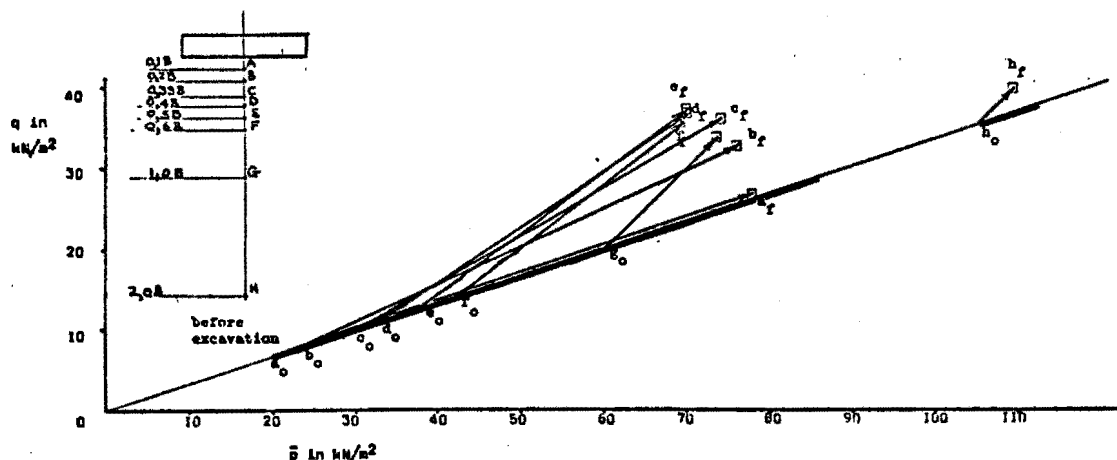


FIGURE 11.1 *Actual and approximated stress paths.*

To follow the shown stress path, the triaxial test must be a K_0 consolidated drained test. In Appendix B the grouping of data for the tests can be seen. This grouping is justified because the field stress path during consolidation is similar to the stress

path for the drained section of the K_0 drained triaxial test. (See Figure 11.2)(Ref. Errera B.Sc.Thesis) This grouping of data enables the absolute minimum amount of samples to be tested.

Theoretically the values of σ_1 and σ_3 should be altered simultaneously throughout this K_0 test so that no lateral strain occurs. If lateral strain is prevented by using suitable σ_3 values, then no shear will be developed across the ends of the sample. This should produce a uniform axial and volumetric strain throughout the sample length.

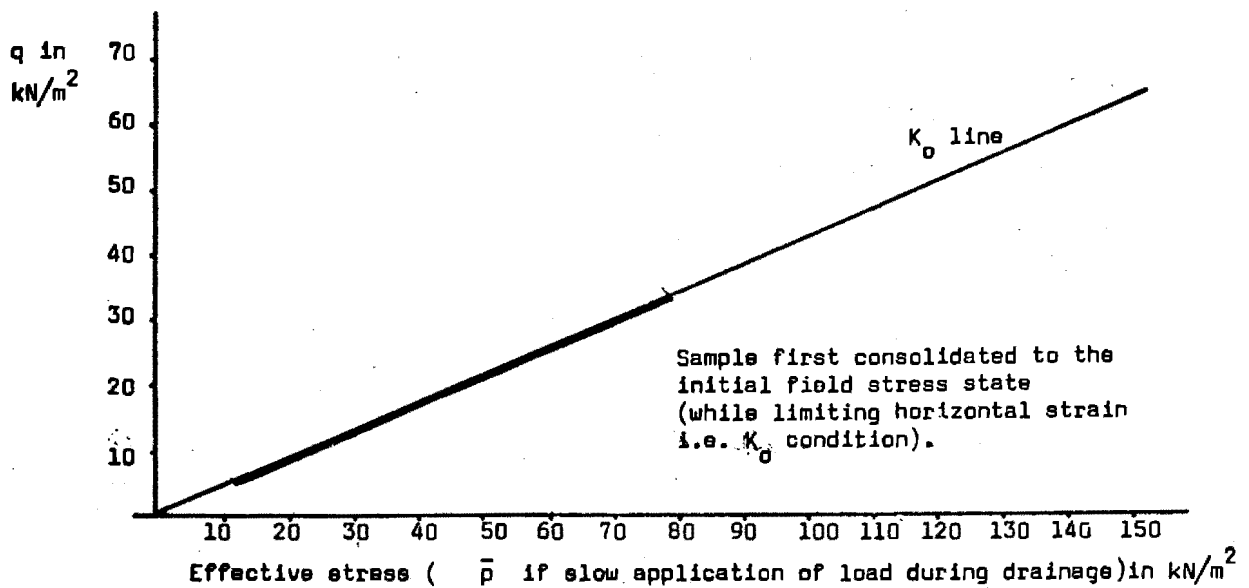


FIGURE 11.2 *Stress paths during K_0 consolidation (i.e. drained test).*

In all the tests performed an adjustment to the external cell pressure was first carried out. This adjustment was one half of the theoretical (K_0) adjustment necessary to produce zero horizontal strain for that particular load increment. This adjustment causes a very minor reduction in the diameter of the sample which is resisted by the end restraints. As the vertical and horizontal stresses are then increased the sample will tend to revert to its original horizontal dimensions. This horizontal movement is once again resisted near the sample ends by the end restraints and by the cell pressure σ_3 . The effects are shown in Figure 11.3.

(Ref. 9 Bishop and Henkel)

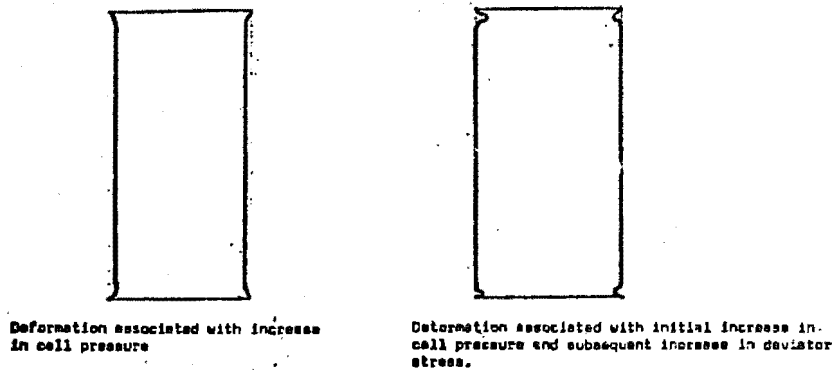


FIGURE 11.3 *End effects due to end restraints.*

The apparatus used for the K_0 testing was not the usual triaxial machine. The reason for this is that the proving ring cannot provide a constant vertical pressure while the sample consolidates, i.e. it does not follow the field stress path. The field stress path has a constant vertical total pressure throughout the time necessary for deformation to occur. This is especially relevant when the soil collapses. It was therefore decided to apply the deviator stress via dead load masses which are directly supported by the test sample. (See Figure 11.4).

The masses used for loading are related directly to the stress variations in the field. The stresses they cause are in terms of kN/m^2 . The deviator stresses vary from 1 kN/m^2 to 50 kN/m^2 . These stresses are related to the masses via the cross-sectional area of the sample.

A lateral strain indicator was used to limit the lateral strain to zero. It is of the mercury bulb type. (See Figure 11.5.)

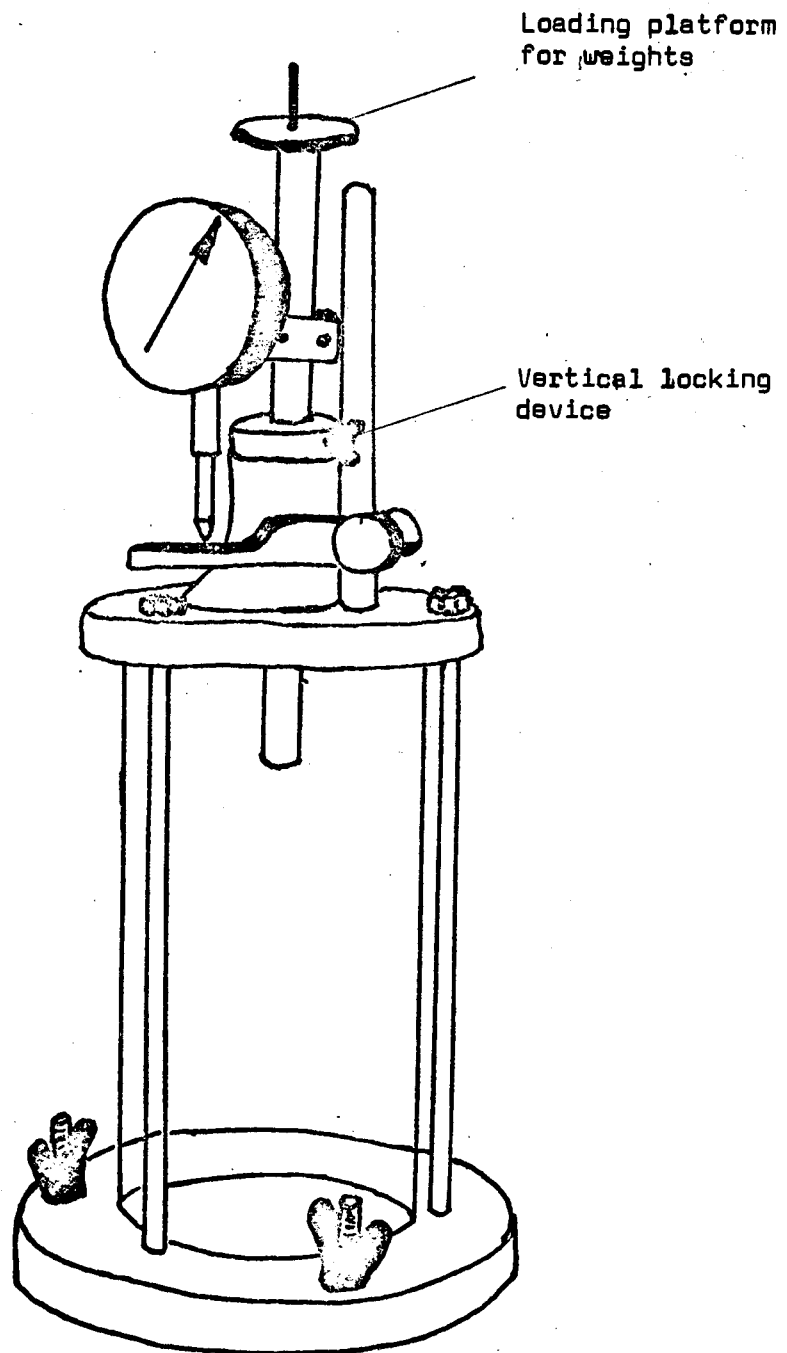


FIGURE 11.4 *Stress path apparatus (for K_0 tests).*

Drainage at both top and bottom porous plates was allowed. To facilitate this drainage, vertical filter paper drains were placed at intervals around the sample. Each end of a vertical drain terminated at the centre of a porous plate where filter end caps were placed.

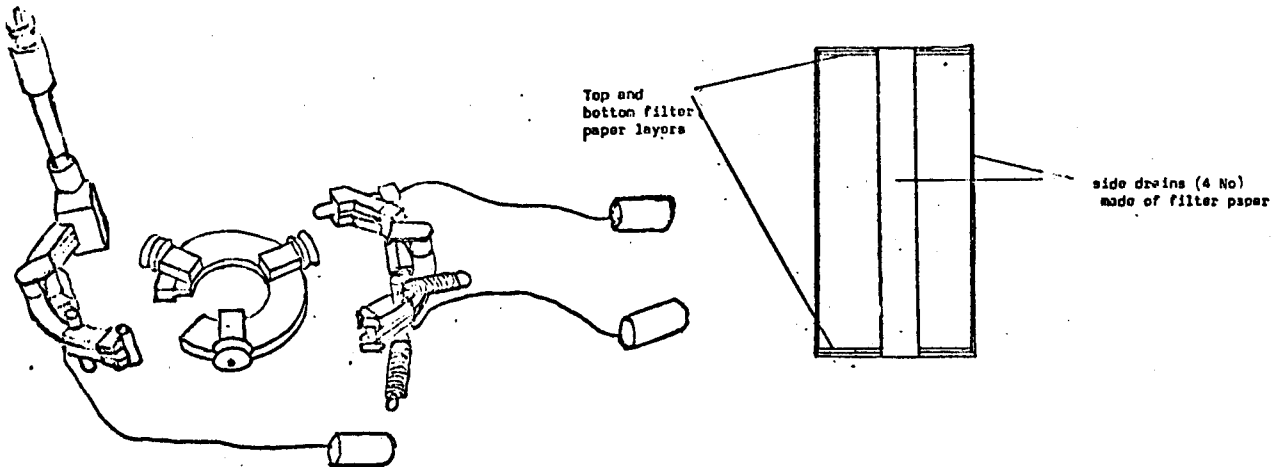


FIGURE 11.5

FIGURE 11.6 *Drainage facilities for the triaxial sample.*

The initial moist masses of the samples were measured. For each sample the moisture content was kept constant throughout the K_0 test. Each K_0 test consisted of a series of increments of vertical pressure with a corresponding manual change of the lateral cell pressure. Water was added to the moistened samples before the test was started. The amount of water added depended on the final estimated moisture content required. The water was added by syringe at numerous points on the surface of the sample. The sample was then surrounded with moist filter paper and allowed to soak for 24 hours in a cool place before being subjected to the K_0 test.

For each increment in deviator stress, readings of the required cell pressure for K_0 deformation and vertical deflections were taken. From the laboratory vertical deflection readings, strain depth curves for anticipated field settlement calculations can be drawn.

11.3 Triaxial tests for the determination of strength parameters

After the settlement tests the samples were tested to failure. The mode of failure for the moist collapsing soils was not the development of a failure plane, but rather a sudden excessive strain. No failure plane was seen in a dry natural soil of high void ratio and low strength from the Sishen area.

Figure 11.7 shows a typical stress strain curve for a clean, dry sand. It is difficult to define point A accurately.

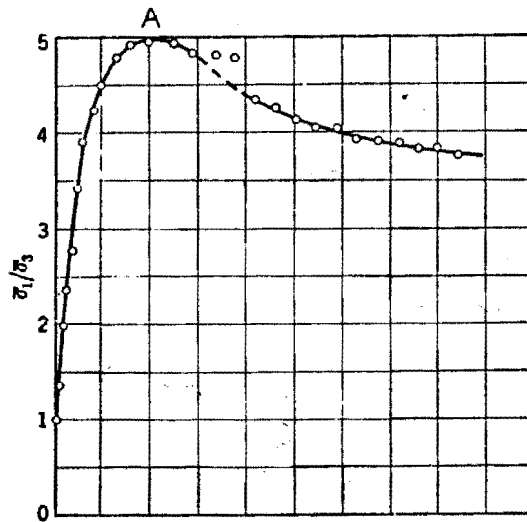


FIGURE 11.7 *The σ_1/σ_3 versus strain ϵ curve for a triaxial sample.*

Bishop and Henkel and Lambe refer to a certain strain value after which the sample is defined as failing. This was used as a guide during experimental stages, but in reality a small increase in load can take the strain from a value below this defined limit to a value which far exceeds it. Therefore the writer looked at the failure as occurring when a small load increment caused an exceptionally large strain. The failure strain value usually varied around the value given by Lambe and Bishop and Henkel.

TABLE 11.1 *Percentage strain values at failure of drained triaxial samples.*

Sample	Clay Content	Void Ratio	Moist Content during Shear	% Strain At Failure	Drained Shear Strength	
					c	ϕ
Feathers	6%	0,918	13%	10%	13kN/m ²	29°
Sishen	9%	0,802	2%	10%	26kN/m ²	22°
Sishen	9%	0,802	10%	8%	17kN/m ²	23°

From the final stress path point in Figure 11.2 on the K_0 line, there are two methods of continuing the tests to determine c and ϕ . The first method is to merely increase the deviator stress until failure (at constant cell pressure) as in Figure 11.8.

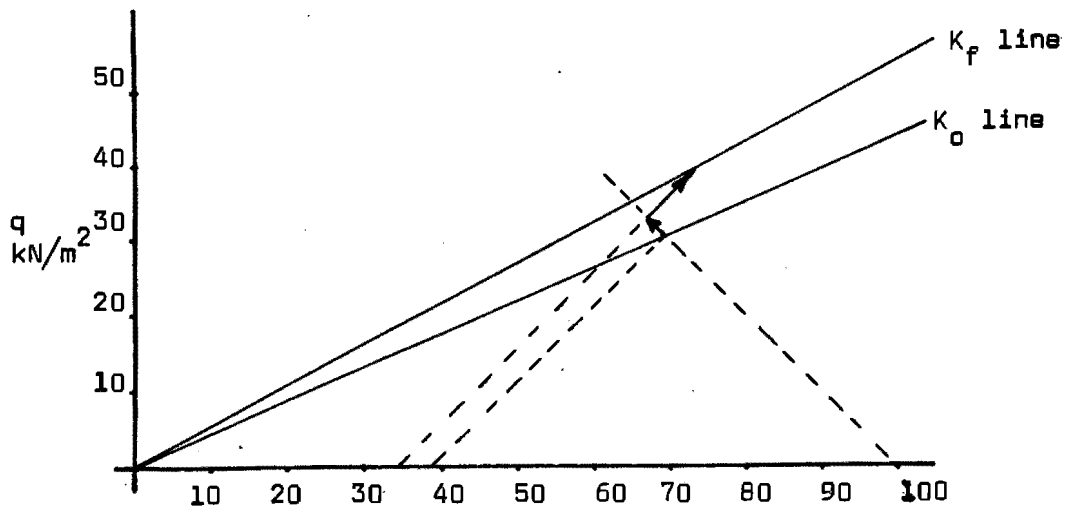


FIGURE 11.8 *The stress path followed during failure testing using method 1.*

The load increments were kept very small. As soon as the strain started becoming appreciable, load increments of deviation stress were confined to 1 kN/m².

The second method was to first vary the cell pressure for each sample prior to shearing. This is necessary to obtain a distribution of points on the K_f curves (i.e. one point for each sample tested). The cell pressure was varied slowly and magnitudes were such that they did not cause any large lateral deformation. Thereafter the deviator stress was increased to cause failure.

Bishop and Henkel state that for samples with ratio of length to diameter in the range of $1\frac{1}{2}$ to $2\frac{1}{2}$, the effect of end restraints on strength characteristics is not significant. They further state that if the strength results are related to the initial void ratio of the sample, then for sands, the non-uniformity of the void ratio within a sample at failure does not influence the consistency of the strength results (when plotted with respect to initial void ratio).

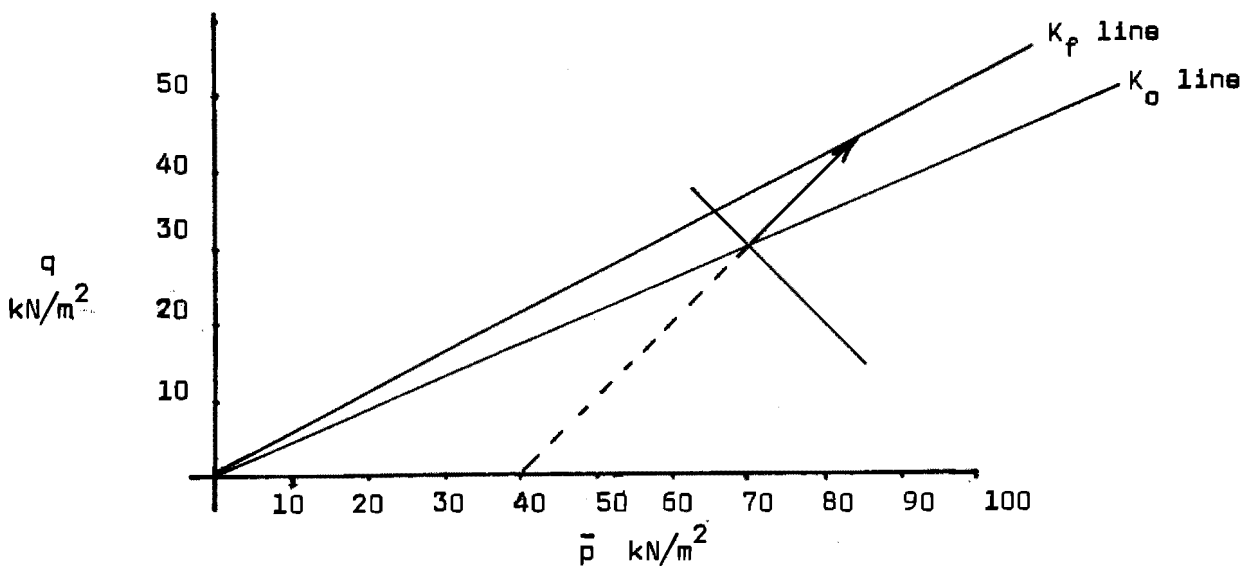


FIGURE 11.9 One of the stress paths followed using method 2.

11.4 Tests for E and μ with varying moisture content

The values of E and μ vary with moisture content (see chapters 7 and 10). The values of μ can be found for various water contents by performing K_o tests on soil samples of different water contents (Section 11.2). The value of μ can be found in each case from the K_o value ($\mu = K_o / (1 + K_o)$)

The Young's modules E can be estimated by measuring the vertical and lateral strains of a soil sample subjected to a small lateral pressure and then using the μ values in the calculations to find E . The problem which now arises is can these soil parameters be determined at several moisture contents with economical usage of soil samples. The essential difference in testing procedures is therefore that the moisture content must be varied during the test (see Figure 11.10a and 11.10b). This test was devised at U.C.T.

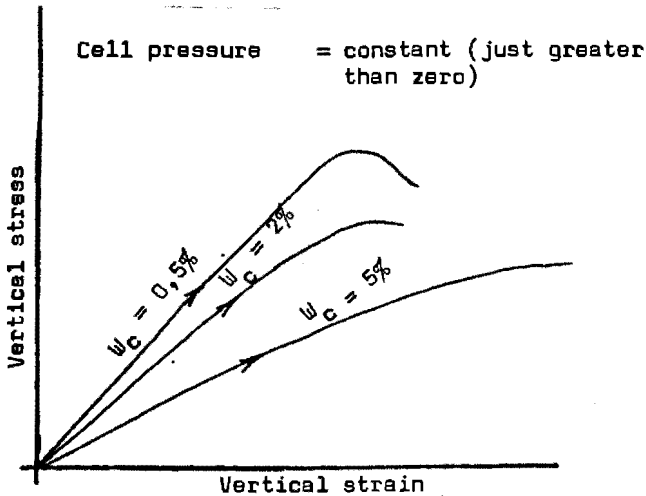


FIGURE 11.10a Results using many samples.

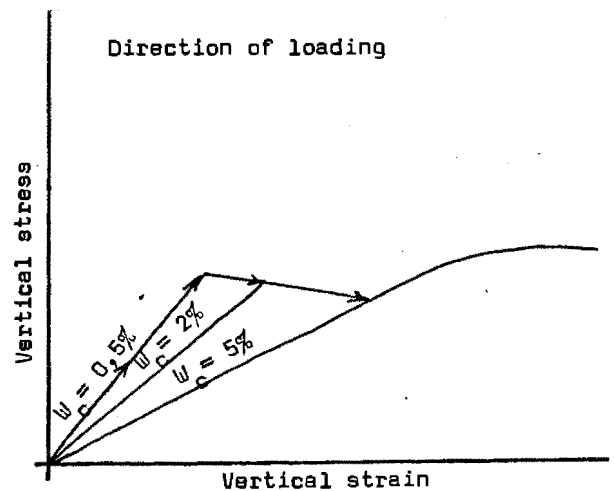


FIGURE 11.10b Results using a single sample.

In order to obtain a set of curves as shown in Figure 11.10b, a controlled volume of water must be allowed to enter the sample after each stage in the test. The additional water was allowed in at Point A (Figure 11.12). Point A is the drainage tap for the bottom hole. This tap was connected to a burette.

Initially the dry sample was put into the triaxial cell. A slight cell pressure of 10^{-4} was applied by connecting the water pressure connection of the cell to a tube. The level of the water in this tube was kept constant. A vertical stress was now applied to the sample. The final deflection readings were noted and the vertical strain was then limited by the clamping device (see Figure 11.12). A small, known volume of water was now added to the sample.

The de-aired cold water was allowed through to the sample by opening both the tap of the burette and the triaxial cell tap (i.e. the exit for air). The open end of the burette was plugged with cottonwool to prevent evaporation. There must be no air bubbles in the connection from the burette to the sample. The difference in burette readings was taken as the additional volume of water. The water passed through the bottom drainage hole, through a perspex disc, through the bottom filter paper and to the sample. No porous plates were used so that the water storage outside the soil would be very small.

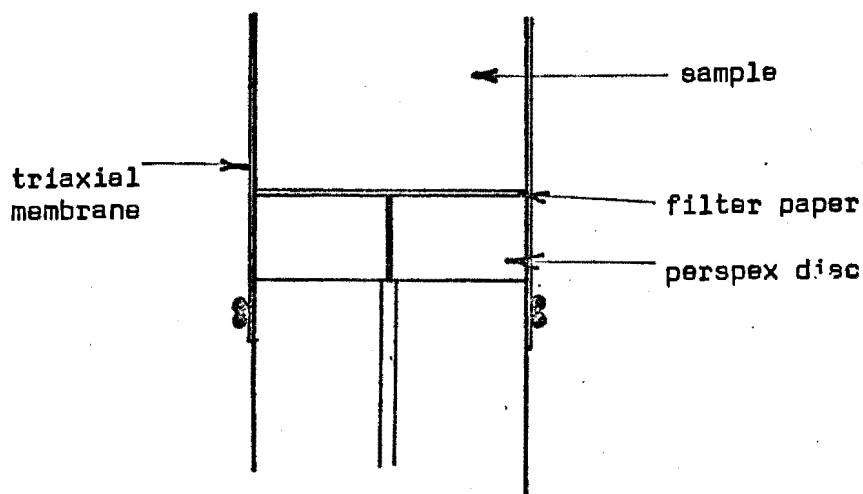


FIGURE 11.11 *Path of water from the bottom drainage hole to the soil sample.*

After a 24-hour period of soaking, the clamping device was released and further settlement was allowed. After the deflection readings had been noted the sample was once more clamped. Water was again added. The process was repeated until the sample was saturated.

Once the sample was saturated it was loaded to failure. The horizontal strain readings were measured on a band of light foil. A telescope was used to obtain the best readings on the foil.



FIGURE 11.12 *Apparatus for tests for E and μ .*

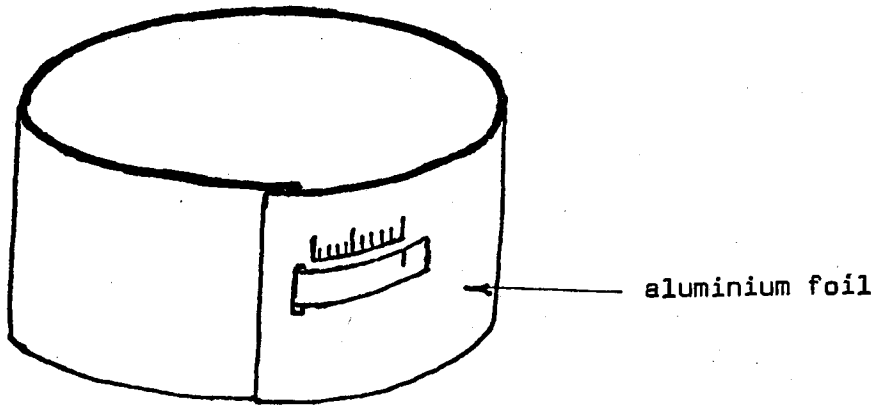


FIGURE 11.13 *Lateral strain gauge.*

$$\text{Horizontal strain} \quad \epsilon_h = \frac{1}{E}[\sigma_h - \mu(\sigma_h + \sigma_v)]$$

$$\text{Vertical strain} \quad \epsilon_v = \frac{1}{E}[\sigma_v - 2\mu\sigma_h]$$

$$\text{therefore} \quad \frac{\epsilon_h}{\epsilon_v} = \frac{\sigma_h - \mu(\sigma_h + \sigma_v)}{\sigma_v - 2\mu\sigma_h}$$

If σ_h is negligible then:

$$\frac{\epsilon_h}{\epsilon_v} = -\mu$$

In the above case E was estimated by using a sample which was not restrained laterally. The horizontal pressure was small. The values of E and μ can also be found from a K_o test in which σ_h , σ_v and the vertical strain ϵ_v are observed:-

- a) Poisson's ratio μ can be found from $\mu = \left(\frac{K_o}{1+K_o}\right)$,
where $K_o = \sigma_h/\sigma_v$
- b) Young's modulus E can then be estimated as the only unknown in the formula

$$\epsilon_v = \frac{1}{E}[\sigma_v - 2\mu\sigma_h]$$

Professor Sparks has suggested that the above methods can be modified so that one dry soil sample may be subjected to K_0 triaxial conditions and, thereafter, known increments of water volume are added each time to this collapsing soil sample while the vertical collapse settlement is restrained by the clamp in Figure 11.12. When the new water content has been established throughout the sample, the sample is permitted to settle further under K_0 conditions which require a reduction in horizontal cell pressure or an increase in vertical pressure. Hence after each known increment of water, the soil consolidates to a new K_0 line corresponding to this new water content. (See Figure 11.14b or Figure 11.14a)

The horizontal strain will always be made to remain approximately zero, by varying σ_h and hence μ can be calculated at each water content from each new K_0 value ($\mu = K_0 / (1 + K_0)$). At each K_0 condition the vertical stress can be increased by an amount $\Delta\sigma_v$ under K_0 conditions causing changes of $\Delta\epsilon_v$ and $\Delta\sigma_h$, while the moisture content remains constant. (The sample is not saturated.) (See Figure 11.14a.)

The Poisson's ratio μ and the measured values of $\Delta\sigma_v$ and $\Delta\sigma_h$ at the end of each collapse stage can be used with $\Delta\epsilon_v$ to estimate the value of E , which applies if the soil is loaded in a moist condition.

$$\left(\text{Use } \Delta\epsilon_v = \frac{1}{E} [\Delta\sigma_v - 2\mu\Delta\sigma_h] \right)$$

Alternatively one need not apply the above incremental K_0 step. In this case ϵ_v is measured from the state of zero load and σ_h and σ_v are measured at the end of each collapse stage. The value of E is now an approximate effective value of E which applies only if the soil is loaded in a moist condition from the known initial void ratio at a zero stress state to the new stress condition.

It will be noticed that because ϵ_v increases as the water content is increased, it follows that the value of E will decrease in the following formula if the other parameters remain approximately unaltered:-

$$\epsilon_v = \frac{1}{E}[\sigma_v - 2\mu\sigma_h]$$

It is known that E does decrease with an increase in water content.

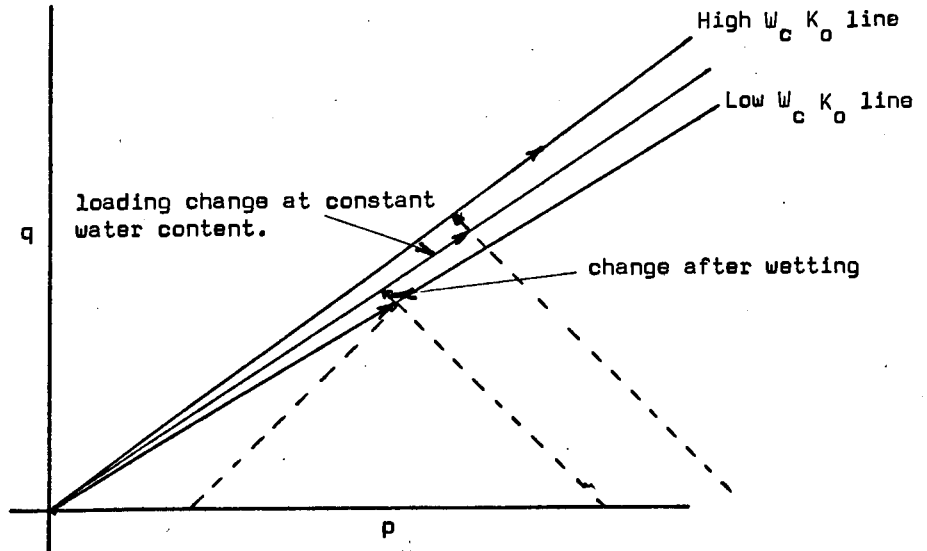


FIGURE 11.14a A possible incremental method for estimating E and μ at different water contents using a single soil sample.

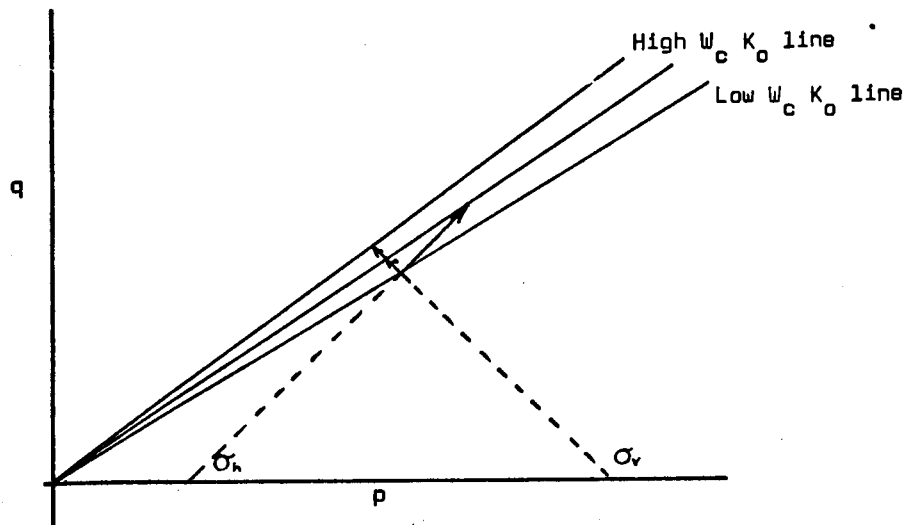


FIGURE 11.14b A method for finding μ and an effective E at different water contents, from a single sample.

11.5 Conclusion

The triaxial machine and the variation used by the writer are extremely versatile machines. The various tests used do not incorporate the most sophisticated test procedures in use today, but they do permit the anticipated insitu stress paths of the soil to be accurately followed.

CONCLUSION

12.1 The Stress Path Method of Settlement Prediction

The stress path method of settlement prediction (as presented by Lambe) has been described and investigated. The writer however believes that Lambe's stress path method should rather be considered to be a sub-division of a more general stress path approach. (i.e. It would fall into a block of the flow chart as presented in Chapter 3.) The flow chart (Fig. 3.1) describes a "stress path approach to settlement prediction".

This stress path approach is divided into three sections:

- i) the investigation of possible stress paths for different soil elements in the particular design problem
- ii) the comparison of predicted actual stress paths (e.g. using Boussinesq elastic theory for both horizontal and vertical stress increments) and approximated stress paths, (i.e. by using K_0 for estimating increases in horizontal stresses from estimated vertical stresses. The latter stresses are estimated by using Boussinesq theory.)
- iii) the preselection of laboratory procedures and the performing of laboratory tests.

The investigation of possible stress paths includes the definition of the actual (Boussinesq) and the approximated (K_0 theory) field stress paths. These two types of calculated stress paths can now be compared with available laboratory stress paths in order to decide which laboratory technique should be used for the settlement prediction. This comparison will also indicate the best method of analysis which should be used for the settlement prediction. The best method might not necessarily be the triaxial stress path method, and in fact the normal consolidometer test might be adequate.

Local authorities could on a grid basis produce proposed design stress paths for soils in their areas. On these charts case

The formula quoted by Simons (Ref. 52) is similar to the settlement formula as used by Terzaghi. The only difference is the constant μ . This constant depends upon A (pore pressure parameter) and the footing shape. The Terzaghi settlement value ($s = \Sigma(m_v \sigma_z D_z)$) is multiplied by this factor, μ , to predict the Skempton-Bjerrum settlement. Published test results (Ref. 6, Ref. 7, Ref. 52), using equation 12.1 compare more favourably with Lambe's or Simon's stress path methods than with the results from equation 12.2. This implies that equation 12.1, when used with the correct stress path, is the more accurate formula. (See Also Chapter 8.)

12.4 The triaxial tests

The triaxial tests as performed for this thesis allow the maximum number of results to be obtained with the minimum sample usage. These K_0 triaxial stress path tests allow the settlement prediction to be calculated. From the same section of the tests the K_0 value is calculated. Once the K_0 value is known, μ (Poisson's ratio) can be calculated. After the stress path test is completed the sample is loaded until failure occurs.

Therefore from a set of six or seven samples in which one varies the initial water content, one can determine:

- the settlement values for different moisture contents
- the K_0 value for different moisture contents
- the value of μ for different moisture contents
- values of c and ϕ for drained samples at different moisture contents. (In this latter case at least two samples are needed for each moisture content.)

The importance of planning test procedures to obtain economical sample usage is emphasized. The laboratory technician should not blindly follow standard procedures. He should rather examine what information is required for the soil to be tested before deciding on any particular testing procedure.

12.5 Comparison of results

For this thesis two important comparisons of results were made. The first was the relationship between footing size and settlement. The results were conclusive in that for the

1,0 m x 1,0 m, 2,0 m x 2,0 m and the 3,0 m x 3,0 m footings a definite relationship was established. For the collapsing granitic soil at low water content, the following settlement results were obtained:

Footing Sizes (All with $D_f = 1$ m)	Predicted Settlements (From K_0 tests and stress path)
1,0 m x 1,0 m	- 9 mm
2,0 m x 2,0 m	- 18 mm
3,0 m x 3,0 m	- 26 mm

The second important comparison which was made was between the settlement values estimated from the different laboratory procedures. The settlement values from the consolidometer results were consistently greater than those based on the triaxial stress path method. For the samples tested at field moisture content (i.e. soil from Sishen and Constantia Nek), the calculated settlements based on consolidometer results were approximately thirty per cent greater than the settlements calculated from the triaxial stress path results. For the soaked samples, however, the calculated settlements from the consolidometer readings were about four per cent larger than the values obtained from the triaxial stress path.

The writer concludes that the large discrepancy in the dry sample results is perhaps a direct result of the sample shape. The supervisor of this thesis considers that an additional reason may be due to the fact that in the triaxial K_0 stress path test, the experimenter is forced to respond by increasing the confining pressure σ_3 after a noticeable lateral strain has occurred. This procedure can result in overcompensation (i.e. σ_3 value may be too high). If the σ_3 value is too high, this can restrict the vertical settlement. In the case of the wetter samples, this effect is not as noticeable.

In table 12.1 the settlements calculated from the consolidometer results and the triaxial stress path results are tabulated. The discrepancy (in millimeters between predicted settlement for the same footing size for the soaked and moist case) appears to remain constant for all the tests. If this difference is expressed as a percentage of the settlements predicted by the triaxial stress path tests, then for the larger settlements, the factor

$$\frac{(\text{Predicted } \Delta(\text{consol.}) - \text{Predicted } \Delta(\text{triaxial}))}{\text{Predicted } \Delta(\text{triaxial})} \times 100$$

approaches zero. Therefore for the larger predicted settlement values (i.e. for the soaked samples) the consolidometer and the triaxial stress path methods should give similar predicted settlement values.

The correlation (Table 12.3) between the observed settlements of model footing tests and the predicted settlements from the triaxial stress path method was less favourable. Figure 12.2 shows a typical q versus settlement curve for a 100 mm x 100 mm model footing on a collapsible residual granitic soil. Table 12.2 shows the observed settlements of the model footing tests done on the collapsing sand sample from Sishen. From these observed results it can be seen that the relationships between the observed settlements and the footing width (for q the same) of the different sized model footings was not even approximately linear. However, the predicted settlements of the larger footings using the stress path method of settlement prediction varied linearly with footing width (see first column, Table 12.3). The writer suggests that the 100 mm x 100 mm model footing should be the smallest sized model footing considered for an approximate predicted settlement for larger sized footings. The usual practice of using a 305 mm x 305 mm plate loading test is within this required size limit. Table 12.3 lists the predicted settlement values for the 1 m x 1 m, 2 m x 2 m and 3 m x 3 m footings using the three different methods of settlement prediction considered. The predicted settlements in the last column of Table 12.3 have been overestimated because a linear law was assumed between settlement and footing width for the figures in this column. Bearing pressure failures for the model footings occurred at values ranging from 40 kN/m^2 (for 50 mm x 50 mm footing on a collapsible granite at about 4% water content) to 113 kN/m^2 (for 50 mm x 50 mm footing on a collapsing sand at about 3% water content). These results are shown in Appendix B and Table 12.2.

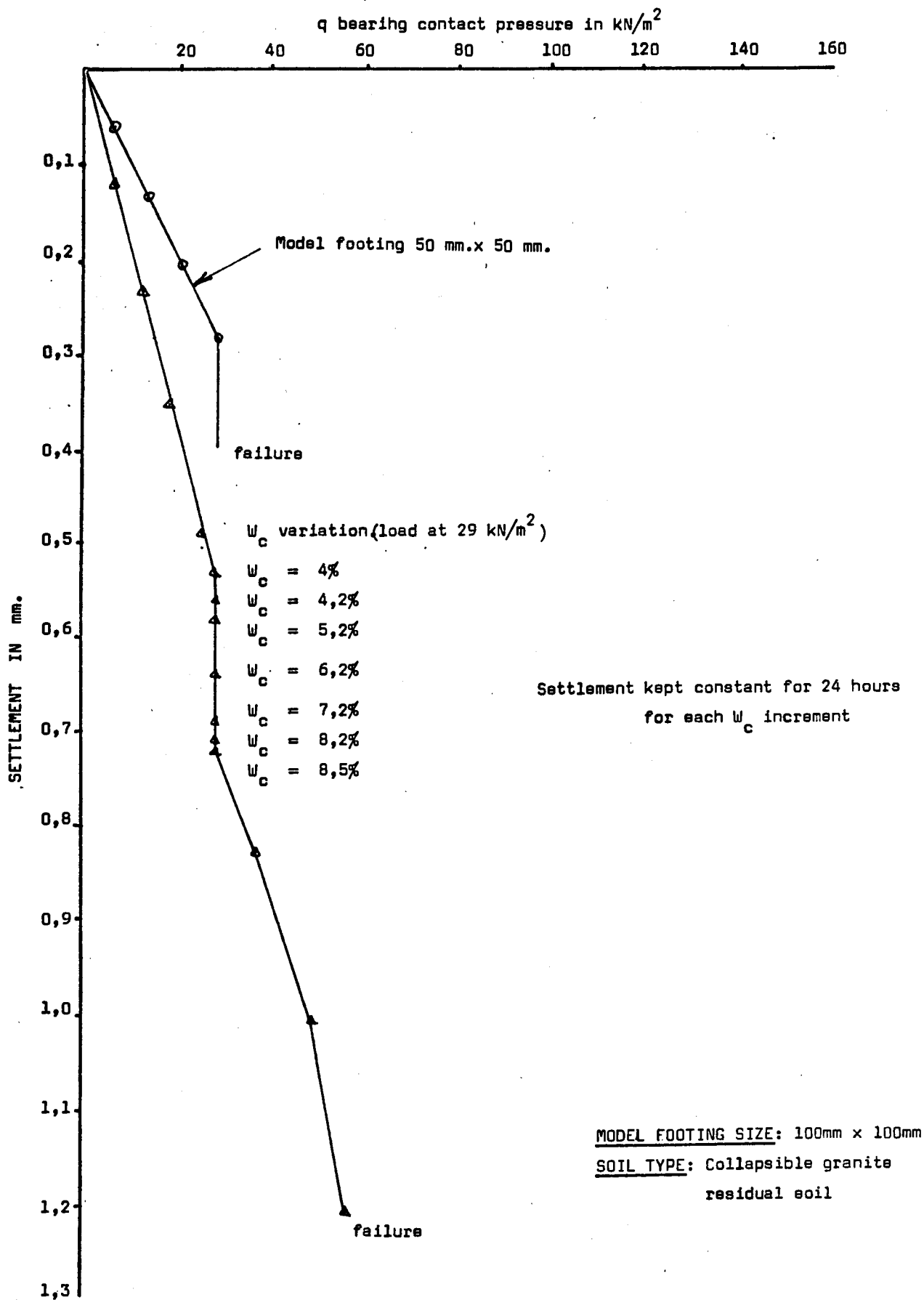


FIGURE 12.2 - q Versus settlement curve for model footings

TABLE 12.1 Predicted settlement values

Test used for Settlement Prediction	SOIL TYPE : Collapsing residual granite (Constantia Nek)			
	Field $w_c = 3\%$		Soaked $w_c = 12\%$	
TRIAXIAL CELL K_o and full drainage	Footing Size	<u>Predicted Settlements</u> for bearing pressure 100 kN/m ² (includes self wt. of footing)		
	1 m x 1 m plan founded at 1 m	9 x B = 9 mm	70 x B = 70 mm	
	2 m x 2 m plan founded at 1 m	9,1 x B = 18 mm	65 x B = 130 mm	
	3 m x 3 m plan founded at 1 m	8,7 x B = 26 mm	60 x B = 180 mm	
CONSOLIDOMETER with full drainage	1 m x 1 m plan founded at 1 m	14 x B = 14 mm	74 x B = 74 mm	
	2 m x 2 m plan founded at 1 m	13 x B = 26 mm	68 x B = 136 mm	
	3 m x 3 m plan founded at 1 m	12 x B = 36 mm	63 x B = 189 mm	
<u>Predicted Δ(Consol) - Predicted Δ(Triax)</u> <u>Predicted Δ(triaxial)</u> (i.e. for same size footing and same water content)		1m x 1m	55%	6%
		2m x 2m	44%	5%
		3m x 3m	38%	5%

TABLE 12.2 *Model footing results, Collapsing sand (Sishen)*

Model Footing Size	Settlement at bearing pressure at 25 kN/m ²	Settlement at bearing pressure of 100 kN/m ²	Maximum bearing pressure at failure	Linearly adjusted values of model footing settlements for 1,0 m x 1,0 m footing (for 25 kN/m ²)
50m x 50m	0,12 mm (w _c ≈ 2%)	0,27 mm (w _c ≈ 2%)	113 kN/m ²	10 mm
100m x 100m	0,15 mm (w _c ≈ 2%)		56 kN/m ² (w _c ÷ 12%)	6 mm

TABLE 12.3 *Settlement predictions for q = 100 kN/m², Collapsible Granite. (All at approximately 3% water content)*

Model Footing Size	Predicted Settlement triaxial stress path	Predicted Settlement consolidometer	Predicted settlements using linearly adjusted observed model footing settlements from 100 mm x 100 mm footing
1 m x 1 m	9 mm	14 mm	18 mm
2 m x 2 m	18 mm	26 mm	36 mm
3 m x 3 m	26 mm	36 mm	54 mm

12.6 Conclusion

This thesis covered most of the approaches to settlement prediction currently in use. Emphasis was given to the limitations of various methods of settlement prediction. It is important to preplan the laboratory procedures to take into account soil type, probable loading and pressures in nature, possible future variations in moisture content which might occur on the site, and the number and size of suitable samples and the availability of suitable testing apparatus.

APPENDIX A

JDHG ERREHA HORIZONTAL STRESSES IN SOILS USING ELASTIC FORMULAE

BRFOR, IS

RFOR 5.106 09/13-14:23-

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0001      0101:      DIMENSION Y(30), R(30), Z(12), COEFA(900), COEFB(900), COEFV(900),
0002      COEFA(900), ANSA(900), ANSB(900), ANSV(900), ANS(900), BSTR(900),
0003      CSTR(900), DSTR(900), ESTR(900), FSTR(900), GSTR(900), RA(30)
0004      0102:      WRITE (5,100)
0005      0103:      100 FORMAT (1H1,4X,*,Y(I),*,6X,*,RA(J),*,6X,*,Z(K),*,6X,*,BSTR(N),*,1X,
0006      CSTR(N),*,1X,*,DSTR(N),*,1X,*,ESTR(N),*,1X,*,FSTR(N),*,1X,*,GSTR(N),*)
0007      0104:      K=1
0008      0105:      Z(K)=0.1
0009      0106:      10 J=1
0010      0107:      L=1
0011      0108:      RA(J)=0.05
0012      0109:      9 I=1
0013      0110:      Y(I)=0.05
0014      0111:      M=1
0015      0112:      COEFA(M)=0
0016      0113:      COEFB(M)=0
0017      0114:      COEFV(M)=0
0018      0115:      COEFN(M)=0
0019      0116:      N=1
0020      0117:      2 R(I)=(RA(J)**2+Y(I)**2)**0.5
0021      0118:      ANSA(L)=(Y(I)**2/(R(I)**2+Y(I)**2))*(3*(R(I)**2)+Z(K)+3*(Y(I)**2)
0022      +Z(K))/(R(I)**2+Z(K)**2+Y(I)**2)**0.5)
0023      0119:      ANSB(L)=(Y(I)**2/(R(I)**2+Y(I)**2))/(R(I)**2+Z(K)**2+Y(I)**2+
0024      +Z(K)*(R(I)**2+Z(K)**2+Y(I)**2)**0.5)+(R(I)**2/(R(I)**2+Y(I)**2)
0025      +1)*(Z(K)/(R(I)**2+Z(K)**2+Y(I)**2)**0.5)-1/(R(I)**2+Z(K)**2
0026      +Y(I)**2+Z(K)*(R(I)**2+Z(K)**2+Y(I)**2)**0.5))
0027      0120:      ANSV(L)=(R(I)**2/(R(I)**2+Y(I)**2))*(3*(R(I)**2)+Z(K)+3*(Y(I)**2)
0028      +Z(K))/(R(I)**2+Z(K)**2+Y(I)**2)**0.5)
0029      0121:      ANS(L)=(R(I)**2/(R(I)**2+Y(I)**2))/(R(I)**2+Z(K)**2+Y(I)**2+
0030      +Z(K)*(R(I)**2+Z(K)**2+Y(I)**2)**0.5)+(Y(I)**2/(R(I)**2+Y(I)**2)
0031      +1)*(Z(K)/(R(I)**2+Z(K)**2+Y(I)**2)**0.5)-1/(R(I)**2+Z(K)**2
0032      +Y(I)**2+Z(K)*(R(I)**2+Z(K)**2+Y(I)**2)**0.5))
0033      0122:      COEFA(M+1)=COEFA(M)+ANSA(L)
0034      0123:      COEFB(M+1)=COEFB(M)+ANSB(L)
0035      0124:      COEFV(M+1)=COEFV(M)+ANSV(L)
0036      0125:      COEFN(M+1)=COEFN(M)+ANS(L)
0037      0126:      L=L+1
0038      0127:      M=M+1
0039      0128:      BSTR(N)=COEFA(M)-0.34*COEFB(M)
0040      0129:      CSTR(N)=COEFA(M)-0.4*COEFB(M)
0041      0130:      DSTR(N)=COEFA(M)-0.5*COEFB(M)
0042      0131:      ESTR(N)=COEFV(M)-0.34*COEFN(M)
0043      0132:      FSTR(N)=COEFV(M)-0.4*COEFN(M)
0044      0133:      GSTR(N)=COEFV(M)-0.5*COEFN(M)
0045      0134:      PRINT 200, ( Y(I), RA(J), Z(K), BSTR(N), CSTR(N), DSTR(N), ESTR(N),
0046      FSTR(N), GSTR(N) )
0047      0135:      200 FORMAT (9F10.3)
0048      0136:      N=N+1
0049      0137:      IF (I-J01 4,3,3)
0050      0138:      4 Y(I+1)=Y(I)+0.1
0051      0139:      I=I+1
0052      0140:      GO TO 2
0053      0141:      3 IF (J-30) 5,6,6
0054      0142:      5 RA(J+1)=RA(J)+0.1
    
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UCT

7	0057	0155:	6	IF (K-6) 40,81,82
8	0058	0156:	80	Z(K+1)=Z(K)+0.1
9	0059	0157:		K=K+1
10	0060	0160:		GO TO 10
11	0061	0161:	81	Z(K+1)=Z(K)+0.4
12	0062	0162:		K=K+1
13	0063	0163:		GO TO 10
14	0064	0164:	82	Z(K+1)=Z(K)+1.0
15	0065	0165:		K=K+1
16	0066	0166:		IF (K-12) 10,10,7
17	0067	0167:	7	STOP
18	0068	0170:		END
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	Y(I)	X(I,J)	Z(K)	GSTR(I)	GSTR(I)	GSTR(I)	ESTR(I)	GSTR(I)	GSTR(I)
	.050	.050	.100	12.410	11.233	9.538	28.441	26.927	24.402
	.150	.050	.100	17.045	18.578	16.466	36.514	34.754	31.821
	.250	.050	.100	22.218	20.098	18.597	38.930	37.106	34.066
	.350	.050	.100	23.190	21.848	19.612	39.905	38.056	34.975
	.450	.050	.100	23.670	22.318	20.065	40.384	38.523	35.422
	.550	.050	.100	23.940	22.582	20.319	40.652	38.785	35.673
	.650	.050	.100	24.106	22.744	20.475	40.817	38.946	35.828
	.750	.050	.100	24.215	22.851	20.527	40.925	39.052	35.929
	.850	.050	.100	24.290	22.924	20.619	41.000	39.125	35.999
	.950	.050	.100	24.344	22.977	20.699	41.054	39.177	36.049
	1.050	.050	.100	24.384	23.017	20.737	41.094	39.216	36.087
	1.150	.050	.100	24.415	23.046	20.766	41.124	39.246	36.116
	1.250	.050	.100	24.439	23.070	20.798	41.148	39.269	36.138
	1.350	.050	.100	24.458	23.088	20.806	41.167	39.288	36.156
	1.450	.050	.100	24.473	23.103	20.821	41.182	39.303	36.170
	1.550	.050	.100	24.486	23.116	20.833	41.195	39.315	36.182
	1.650	.050	.100	24.496	23.126	20.842	41.205	39.325	36.191
	1.750	.050	.100	24.505	23.135	20.851	41.214	39.334	36.200
	1.850	.050	.100	24.512	23.142	20.858	41.221	39.341	36.207
	1.950	.050	.100	24.517	23.148	20.864	41.228	39.347	36.212
	2.050	.050	.100	24.524	23.153	20.869	41.233	39.352	36.218
	2.150	.050	.100	24.529	23.158	20.873	41.238	39.357	36.222
	2.250	.050	.100	24.533	23.162	20.877	41.242	39.361	36.226
	2.350	.050	.100	24.537	23.165	20.880	41.246	39.364	36.229
	2.450	.050	.100	24.540	23.169	20.883	41.249	39.368	36.232
	2.550	.050	.100	24.543	23.171	20.886	41.252	39.370	36.235
	2.650	.050	.100	24.545	23.174	20.888	41.254	39.373	36.237
	2.750	.050	.100	24.547	23.176	20.891	41.256	39.375	36.239
	2.850	.050	.100	24.549	23.178	20.892	41.258	39.377	36.241
	2.950	.050	.100	24.551	23.180	20.894	41.260	39.379	36.243
	.050	.150	.100	3.390	3.502	3.689	22.224	21.285	19.721
	.150	.150	.100	7.452	7.569	7.703	28.696	27.475	25.440
	.250	.150	.100	9.306	9.414	9.593	30.793	29.485	27.305
	.350	.150	.100	10.173	10.273	10.441	31.672	30.330	28.093
	.450	.150	.100	10.626	10.722	10.882	32.114	30.756	28.492
	.550	.150	.100	10.908	10.981	11.136	32.365	30.999	28.720
	.650	.150	.100	11.052	11.143	11.294	32.521	31.149	28.862
	.750	.150	.100	11.160	11.250	11.398	32.624	31.249	28.957
	.850	.150	.100	11.236	11.324	11.471	32.696	31.318	29.022
	.950	.150	.100	11.290	11.377	11.523	32.748	31.369	29.070
	1.050	.150	.100	11.330	11.417	11.562	32.786	31.406	29.106
	1.150	.150	.100	11.361	11.447	11.591	32.816	31.435	29.133
	1.250	.150	.100	11.385	11.471	11.614	32.839	31.457	29.154
	1.350	.150	.100	11.405	11.490	11.633	32.857	31.475	29.171
	1.450	.150	.100	11.420	11.505	11.647	32.872	31.490	29.185
	1.550	.150	.100	11.433	11.518	11.659	32.885	31.502	29.196
	1.650	.150	.100	11.443	11.528	11.669	32.895	31.511	29.206
	1.750	.150	.100	11.452	11.537	11.678	32.903	31.520	29.214
	1.850	.150	.100	11.460	11.544	11.685	32.911	31.527	29.220
	1.950	.150	.100	11.466	11.550	11.691	32.917	31.533	29.226
	2.050	.150	.100	11.472	11.555	11.696	32.922	31.538	29.231
	2.150	.150	.100	11.476	11.561	11.701	32.927	31.542	29.235
	2.250	.150	.100	11.480	11.565	11.705	32.931	31.546	29.239
	2.350	.150	.100	11.484	11.568	11.708	32.934	31.550	29.243
	2.450	.150	.100	11.487	11.571	11.711	32.937	31.553	29.245
	2.550	.150	.100	11.490	11.574	11.714	32.940	31.556	29.248
	2.650	.150	.100	11.493	11.577	11.716	32.943	31.558	29.250
	2.750	.150	.100	11.495	11.579	11.719	32.945	31.560	29.252
	2.850	.150	.100	11.497	11.581	11.721	32.947	31.562	29.254

UCT

3	2.950	.150	.100	11.199	11.533	11.722	32.949	31.564	29.256
5	.050	.250	.100	1.920	2.179	2.612	8.615	8.078	7.181
7	.150	.250	.100	3.981	4.352	4.922	12.524	11.726	10.394
9	.250	.250	.100	5.273	5.681	6.363	14.090	13.186	11.679
11	.350	.250	.100	5.990	6.411	7.113	14.807	13.856	12.273
13	.450	.250	.100	6.400	6.826	7.535	15.183	14.211	12.590
15	.550	.250	.100	6.649	7.076	7.788	15.404	14.419	12.777
17	.650	.250	.100	6.809	7.236	7.949	15.543	14.551	12.897
19	.750	.250	.100	6.916	7.344	8.056	15.637	14.640	12.978
21	.850	.250	.100	6.992	7.419	8.132	15.702	14.702	13.036
23	.950	.250	.100	7.047	7.474	8.186	15.750	14.748	13.078
25	1.050	.250	.100	7.088	7.515	8.226	15.786	14.783	13.110
27	1.150	.250	.100	7.119	7.546	8.257	15.814	14.809	13.135
29	1.250	.250	.100	7.144	7.570	8.281	15.836	14.830	13.154
31	1.350	.250	.100	7.163	7.590	8.300	15.853	14.847	13.170
33	1.450	.250	.100	7.179	7.605	8.316	15.867	14.860	13.183
35	1.550	.250	.100	7.192	7.618	8.328	15.879	14.872	13.193
37	1.650	.250	.100	7.203	7.629	8.339	15.889	14.881	13.202
39	1.750	.250	.100	7.212	7.638	8.348	15.897	14.889	13.209
41	1.850	.250	.100	7.220	7.645	8.355	15.904	14.896	13.216
43	1.950	.250	.100	7.226	7.652	8.361	15.910	14.901	13.221
45	2.050	.250	.100	7.232	7.657	8.367	15.915	14.906	13.226
47	2.150	.250	.100	7.237	7.662	8.372	15.919	14.911	13.230
49	2.250	.250	.100	7.241	7.666	8.376	15.923	14.915	13.233
51	2.350	.250	.100	7.245	7.670	8.379	15.927	14.918	13.237
53	2.450	.250	.100	7.248	7.673	8.382	15.930	14.921	13.239
55	2.550	.250	.100	7.251	7.676	8.385	15.932	14.923	13.242
57	2.650	.250	.100	7.253	7.679	8.388	15.935	14.926	13.244
59	2.750	.250	.100	7.256	7.681	8.390	15.937	14.928	13.246
61	2.850	.250	.100	7.258	7.683	8.392	15.939	14.930	13.248
63	2.950	.250	.100	7.260	7.685	8.394	15.941	14.931	13.249
65	.050	.350	.100	1.324	1.539	1.897	3.465	3.132	2.578
67	.150	.350	.100	2.571	2.917	3.492	5.549	5.006	4.100
69	.250	.350	.100	3.480	3.887	4.566	6.587	5.936	4.850
71	.350	.350	.100	4.560	4.996	5.222	7.119	6.414	5.238
73	.450	.350	.100	4.423	4.872	5.620	7.417	6.683	5.460
75	.550	.350	.100	4.656	5.111	5.871	7.598	6.848	5.598
77	.650	.350	.100	4.910	5.269	6.035	7.716	6.956	5.689
79	.750	.350	.100	4.916	5.378	6.146	7.796	7.030	5.753
81	.850	.350	.100	4.992	5.454	6.225	7.854	7.084	5.800
83	.950	.350	.100	5.048	5.511	6.292	7.896	7.123	5.835
85	1.050	.350	.100	5.089	5.553	6.325	7.929	7.154	5.862
87	1.150	.350	.100	5.122	5.595	6.358	7.954	7.177	5.883
89	1.250	.350	.100	5.147	5.610	6.383	7.974	7.196	5.900
91	1.350	.350	.100	5.167	5.631	6.404	7.990	7.211	5.913
93	1.450	.350	.100	5.183	5.647	6.420	8.003	7.223	5.924
95	1.550	.350	.100	5.196	5.660	6.433	8.014	7.234	5.934
97	1.650	.350	.100	5.209	5.671	6.444	8.023	7.242	5.942
99	1.750	.350	.100	5.217	5.681	6.454	8.030	7.250	5.948
101	1.850	.350	.100	5.225	5.688	6.461	8.037	7.256	5.954
103	1.950	.350	.100	5.231	5.695	6.468	8.043	7.261	5.959
105	2.050	.350	.100	5.237	5.701	6.474	8.047	7.266	5.963
107	2.150	.350	.100	5.242	5.706	6.479	8.052	7.270	5.967
109	2.250	.350	.100	5.247	5.710	6.483	8.055	7.274	5.970
111	2.350	.350	.100	5.250	5.714	6.487	8.059	7.277	5.973
113	2.450	.350	.100	5.254	5.717	6.490	8.062	7.279	5.976
115	2.550	.350	.100	5.257	5.720	6.493	8.064	7.282	5.978
117	2.650	.350	.100	5.259	5.723	6.496	8.066	7.284	5.980
119	2.750	.350	.100	5.262	5.725	6.498	8.069	7.286	5.982
121	2.850	.350	.100	5.264	5.728	6.500	8.070	7.288	5.984

UCT

3	2.950	.450	.100	5.266	3.729	6.502	8.072	7.290	5.985	4
5	.050	.450	.100	.959	1.122	1.374	1.527	1.305	.934	6
7	.150	.450	.100	1.626	2.106	2.574	2.607	2.222	1.578	8
9	.250	.450	.100	2.500	2.850	3.433	3.244	2.759	1.950	10
11	.350	.450	.100	2.973	3.360	4.006	3.610	3.067	2.163	12
13	.450	.450	.100	3.292	3.700	4.379	3.829	3.254	2.295	14
15	.550	.450	.100	3.507	3.926	4.625	3.969	3.374	2.382	16
17	.650	.450	.100	3.655	4.081	4.791	4.063	3.455	2.443	18
19	.750	.450	.100	3.730	4.190	4.907	4.128	3.513	2.488	20
21	.850	.450	.100	3.836	4.268	4.989	4.177	3.556	2.522	22
23	.950	.450	.100	3.892	4.326	5.050	4.213	3.588	2.548	24
25	1.050	.450	.100	3.934	4.370	5.095	4.240	3.614	2.569	26
27	1.150	.450	.100	3.967	4.403	5.130	4.262	3.634	2.585	28
29	1.250	.450	.100	3.993	4.430	5.158	4.280	3.650	2.599	30
31	1.350	.450	.100	4.014	4.451	5.179	4.294	3.663	2.610	32
33	1.450	.450	.100	4.031	4.468	5.197	4.306	3.673	2.619	34
35	1.550	.450	.100	4.045	4.482	5.211	4.316	3.683	2.627	36
37	1.650	.450	.100	4.056	4.494	5.223	4.324	3.690	2.634	38
39	1.750	.450	.100	4.066	4.504	5.233	4.331	3.697	2.640	40
41	1.850	.450	.100	4.074	4.512	5.241	4.337	3.702	2.645	42
43	1.950	.450	.100	4.081	4.519	5.249	4.342	3.707	2.649	44
45	2.050	.450	.100	4.087	4.525	5.255	4.347	3.711	2.653	46
47	2.150	.450	.100	4.092	4.530	5.260	4.351	3.715	2.656	48
49	2.250	.450	.100	4.097	4.536	5.264	4.354	3.718	2.659	50
51	2.350	.450	.100	4.101	4.539	5.268	4.357	3.721	2.662	52
53	2.450	.450	.100	4.104	4.542	5.272	4.360	3.724	2.664	54
55	2.550	.450	.100	4.107	4.545	5.275	4.362	3.726	2.666	56
57	2.650	.450	.100	4.110	4.548	5.278	4.364	3.728	2.668	58
59	2.750	.450	.100	4.112	4.550	5.280	4.366	3.730	2.670	60
61	2.850	.450	.100	4.115	4.553	5.283	4.368	3.732	2.671	62
63	2.950	.450	.100	4.117	4.555	5.284	4.370	3.733	2.673	64
65	.050	.550	.100	.719	.814	1.052	.715	.556	.293	66
67	.150	.550	.100	1.366	1.592	1.964	1.271	.986	.511	68
69	.250	.550	.100	1.894	2.134	2.667	1.641	1.269	.648	70
71	.350	.550	.100	2.286	2.617	3.169	1.875	1.447	.733	72
73	.450	.550	.100	2.556	2.923	3.517	2.025	1.562	.791	74
75	.550	.550	.100	2.765	3.136	3.756	2.126	1.641	.832	76
77	.650	.550	.100	2.907	3.237	3.922	2.196	1.696	.864	78
79	.750	.550	.100	3.009	3.346	4.041	2.246	1.737	.890	80
81	.850	.550	.100	3.084	3.476	4.127	2.284	1.769	.910	82
83	.950	.550	.100	3.141	3.535	4.191	2.313	1.793	.927	84
85	1.050	.550	.100	3.185	3.590	4.239	2.336	1.813	.941	86
87	1.150	.550	.100	3.219	3.615	4.277	2.354	1.829	.952	88
89	1.250	.550	.100	3.245	3.643	4.306	2.369	1.841	.962	90
91	1.350	.550	.100	3.267	3.665	4.329	2.381	1.852	.970	92
93	1.450	.550	.100	3.284	3.683	4.348	2.392	1.861	.977	94
95	1.550	.550	.100	3.299	3.698	4.364	2.400	1.869	.984	96
97	1.650	.550	.100	3.311	3.710	4.376	2.407	1.875	.989	98
99	1.750	.550	.100	3.321	3.721	4.387	2.414	1.881	.993	100
101	1.850	.550	.100	3.329	3.729	4.396	2.419	1.886	.997	102
103	1.950	.550	.100	3.336	3.737	4.404	2.424	1.890	1.001	104
105	2.050	.550	.100	3.343	3.743	4.410	2.428	1.894	1.004	106
107	2.150	.550	.100	3.348	3.749	4.416	2.431	1.897	1.007	108
109	2.250	.550	.100	3.353	3.753	4.421	2.434	1.900	1.010	110
111	2.350	.550	.100	3.357	3.757	4.425	2.437	1.903	1.012	112
113	2.450	.550	.100	3.361	3.761	4.429	2.440	1.905	1.014	114
115	2.550	.550	.100	3.364	3.764	4.432	2.442	1.907	1.016	116
117	2.650	.550	.100	3.367	3.767	4.435	2.444	1.909	1.017	118
119	2.750	.550	.100	3.369	3.770	4.438	2.446	1.911	1.019	120
121	2.850	.550	.100	3.371	3.772	4.440	2.448	1.912	1.020	122

UIC-T

1	2.950	.550	.100	3.324	3.774	4.442	2.449	1.214	1.021	
3	.050	.650	.100	.556	.655	.315	.305	.221	.025	
5	.150	.650	.100	1.003	1.272	1.541	.619	.401	.034	
7	.250	.650	.100	1.467	1.720	2.125	.822	.529	.041	
9	.350	.650	.100	1.817	2.098	2.556	.960	.616	.041	
11	.450	.650	.100	2.065	2.373	2.800	1.055	.675	.042	
13	.550	.650	.100	2.240	2.574	3.115	1.121	.718	.046	
15	.650	.650	.100	2.383	2.720	3.281	1.169	.750	.052	
17	.750	.650	.100	2.482	2.827	3.402	1.205	.775	.059	
19	.850	.650	.100	2.557	2.938	3.491	1.233	.796	.067	
21	.950	.650	.100	2.615	2.968	3.553	1.255	.812	.074	
23	1.050	.650	.100	2.659	3.015	3.609	1.273	.826	.081	
25	1.150	.650	.100	2.693	3.052	3.649	1.287	.837	.087	
27	1.250	.650	.100	2.721	3.081	3.680	1.299	.847	.093	
29	1.350	.650	.100	2.743	3.104	3.705	1.309	.855	.098	
31	1.450	.650	.100	2.761	3.123	3.726	1.317	.862	.103	
33	1.550	.650	.100	2.776	3.139	3.742	1.324	.868	.107	
35	1.650	.650	.100	2.799	3.152	3.756	1.331	.873	.111	
37	1.750	.650	.100	2.799	3.153	3.758	1.336	.878	.114	
39	1.850	.650	.100	2.808	3.172	3.777	1.340	.882	.117	
41	1.950	.650	.100	2.816	3.180	3.786	1.345	.885	.120	
43	2.050	.650	.100	2.822	3.185	3.793	1.348	.889	.123	
45	2.150	.650	.100	2.828	3.192	3.799	1.351	.891	.125	
47	2.250	.650	.100	2.833	3.197	3.804	1.354	.894	.127	
49	2.350	.650	.100	2.837	3.202	3.809	1.357	.896	.129	
51	2.450	.650	.100	2.841	3.205	3.813	1.359	.898	.130	
53	2.550	.650	.100	2.845	3.209	3.816	1.361	.900	.132	
55	2.650	.650	.100	2.848	3.212	3.819	1.363	.902	.133	
57	2.750	.650	.100	2.850	3.215	3.822	1.364	.903	.134	
59	2.850	.650	.100	2.853	3.217	3.825	1.366	.905	.136	
61	2.950	.650	.100	2.855	3.219	3.827	1.367	.906	.137	
63	.050	.750	.100	.442	.519	.648	.153	.062	-.090	
65	.150	.750	.100	.849	.979	1.236	.284	.112	-.173	
67	.250	.750	.100	1.196	1.377	1.723	.384	.148	-.243	
69	.350	.750	.100	1.481	1.719	2.115	.456	.173	-.297	
71	.450	.750	.100	1.701	1.950	2.409	.508	.192	-.335	
73	.550	.750	.100	1.869	2.153	2.627	.546	.206	-.360	
75	.650	.750	.100	1.996	2.294	2.790	.575	.219	-.376	
77	.750	.750	.100	2.093	2.400	2.911	.598	.229	-.384	
79	.850	.750	.100	2.167	2.480	3.002	.616	.239	-.389	
81	.950	.750	.100	2.224	2.542	3.071	.631	.248	-.391	
83	1.050	.750	.100	2.269	2.590	3.125	.644	.256	-.391	
85	1.150	.750	.100	2.304	2.628	3.167	.654	.263	-.389	
87	1.250	.750	.100	2.333	2.658	3.201	.663	.269	-.388	
89	1.350	.750	.100	2.356	2.683	3.228	.670	.274	-.386	
91	1.450	.750	.100	2.375	2.703	3.249	.677	.279	-.384	
93	1.550	.750	.100	2.390	2.719	3.267	.683	.284	-.382	
95	1.650	.750	.100	2.403	2.733	3.282	.686	.287	-.380	
97	1.750	.750	.100	2.414	2.744	3.294	.692	.291	-.378	
99	1.850	.750	.100	2.424	2.754	3.305	.696	.294	-.376	
101	1.950	.750	.100	2.432	2.762	3.314	.699	.297	-.374	
103	2.050	.750	.100	2.435	2.769	3.321	.702	.299	-.372	
105	2.150	.750	.100	2.444	2.776	3.328	.705	.302	-.371	
107	2.250	.750	.100	2.445	2.781	3.334	.707	.304	-.369	
109	2.350	.750	.100	2.454	2.786	3.339	.710	.306	-.368	
111	2.450	.750	.100	2.458	2.790	3.343	.712	.307	-.367	
113	2.550	.750	.100	2.462	2.793	3.347	.713	.309	-.365	
115	2.650	.750	.100	2.465	2.797	3.350	.715	.310	-.364	
117	2.750	.750	.100	2.467	2.800	3.353	.716	.312	-.362	
119	2.850	.750	.100	2.470	2.802	3.356	.718	.313	-.362	

UCT

2.950	.750	.100	2.472	2.334	3.358	.719	.314	-.362
.350	.850	.100	.358	.421	.526	.055	-.017	-.138
.150	.850	.100	.692	.812	1.012	.103	-.034	-.264
.250	.850	.100	.785	1.152	1.429	.141	-.051	-.372
.350	.850	.100	1.229	1.432	1.770	.169	-.066	-.457
.450	.850	.100	1.428	1.655	2.038	.190	-.076	-.521
.550	.850	.100	1.580	1.829	2.244	.206	-.084	-.567
.650	.850	.100	1.700	1.963	2.401	.220	-.087	-.599
.750	.850	.100	1.793	2.066	2.522	.231	-.089	-.621
.850	.850	.100	1.866	2.146	2.614	.240	-.088	-.636
.950	.850	.100	1.923	2.209	2.685	.249	-.087	-.646
1.050	.850	.100	1.958	2.258	2.741	.256	-.084	-.652
1.150	.850	.100	2.034	2.297	2.785	.263	-.082	-.656
1.250	.850	.100	2.033	2.328	2.821	.269	-.079	-.659
1.350	.850	.100	2.057	2.354	2.849	.274	-.076	-.660
1.450	.850	.100	2.076	2.375	2.872	.279	-.073	-.660
1.550	.850	.100	2.093	2.392	2.892	.283	-.071	-.660
1.650	.850	.100	2.106	2.407	2.907	.287	-.068	-.660
1.750	.850	.100	2.118	2.419	2.921	.290	-.066	-.659
1.850	.850	.100	2.127	2.429	2.932	.293	-.064	-.659
1.950	.850	.100	2.136	2.438	2.942	.296	-.062	-.658
2.050	.850	.100	2.143	2.446	2.950	.298	-.060	-.657
2.150	.850	.100	2.149	2.452	2.957	.300	-.058	-.656
2.250	.850	.100	2.155	2.458	2.963	.302	-.057	-.655
2.350	.850	.100	2.157	2.463	2.968	.304	-.055	-.655
2.450	.850	.100	2.164	2.467	2.973	.306	-.054	-.654
2.550	.850	.100	2.167	2.471	2.977	.307	-.053	-.653
2.650	.850	.100	2.171	2.474	2.981	.309	-.052	-.652
2.750	.850	.100	2.173	2.477	2.984	.310	-.051	-.652
2.850	.850	.100	2.176	2.480	2.987	.311	-.050	-.651
2.950	.850	.100	2.178	2.483	2.990	.312	-.049	-.650
.050	.950	.100	.295	.348	.435	.003	-.056	-.154
.150	.950	.100	.575	.675	.842	.005	-.109	-.297
.250	.950	.100	.824	.965	1.200	.004	-.155	-.422
.350	.950	.100	1.036	1.210	1.500	.004	-.194	-.523
.450	.950	.100	1.212	1.411	1.744	.003	-.225	-.603
.550	.950	.100	1.363	1.572	1.937	.002	-.247	-.664
.650	.950	.100	1.458	1.699	2.088	.003	-.264	-.708
.750	.950	.100	1.556	1.800	2.206	.004	-.275	-.741
.850	.950	.100	1.627	1.879	2.299	.007	-.263	-.765
.950	.950	.100	1.663	1.941	2.371	.009	-.287	-.782
1.050	.950	.100	1.728	1.991	2.429	.012	-.290	-.794
1.150	.950	.100	1.765	2.031	2.475	.015	-.292	-.803
1.250	.950	.100	1.795	2.063	2.512	.018	-.292	-.809
1.350	.950	.100	1.819	2.090	2.542	.021	-.292	-.813
1.450	.950	.100	1.839	2.112	2.566	.024	-.291	-.817
1.550	.950	.100	1.856	2.130	2.587	.026	-.291	-.819
1.650	.950	.100	1.870	2.145	2.604	.029	-.290	-.820
1.750	.950	.100	1.882	2.158	2.618	.031	-.288	-.821
1.850	.950	.100	1.892	2.169	2.630	.033	-.287	-.821
1.950	.950	.100	1.901	2.178	2.640	.035	-.286	-.822
2.050	.950	.100	1.908	2.186	2.649	.037	-.285	-.822
2.150	.950	.100	1.915	2.191	2.657	.039	-.284	-.822
2.250	.950	.100	1.921	2.199	2.663	.040	-.283	-.822
2.350	.950	.100	1.926	2.204	2.669	.042	-.282	-.821
2.450	.950	.100	1.930	2.209	2.674	.043	-.281	-.821
2.550	.950	.100	1.934	2.213	2.679	.044	-.280	-.821
2.650	.950	.100	1.937	2.217	2.683	.045	-.279	-.820
2.750	.950	.100	1.940	2.220	2.686	.046	-.278	-.820
2.850	.950	.100	1.943	2.223	2.689	.047	-.278	-.819

UIC-T

1	1.250	1.250	1.100	1.945	2.226	2.692	-.648	-.277	-.819
3	1.050	1.150	1.100	1.249	1.292	1.365	-.026	-.074	-.156
5	1.150	1.150	1.100	1.465	1.599	1.710	-.150	-.145	-.302
7	1.250	1.150	1.100	1.692	1.819	1.620	-.073	-.207	-.432
9	1.350	1.150	1.100	1.925	1.935	1.289	-.092	-.261	-.591
11	1.450	1.150	1.100	1.112	1.216	1.507	-.108	-.304	-.630
13	1.550	1.150	1.100	1.172	1.365	1.687	-.121	-.338	-.699
15	1.650	1.150	1.100	1.279	1.485	1.831	-.130	-.363	-.753
17	1.750	1.150	1.100	1.363	1.532	1.946	-.136	-.383	-.794
19	1.850	1.150	1.100	1.432	1.659	2.038	-.140	-.397	-.824
21	1.950	1.150	1.100	1.484	1.721	2.111	-.143	-.407	-.847
23	1.050	1.050	1.100	1.533	1.772	2.169	-.144	-.414	-.865
25	1.150	1.050	1.100	1.570	1.812	2.217	-.144	-.419	-.878
27	1.250	1.050	1.100	1.600	1.846	2.255	-.144	-.423	-.888
29	1.350	1.050	1.100	1.625	1.873	2.286	-.144	-.425	-.895
31	1.450	1.050	1.100	1.645	1.896	2.312	-.143	-.427	-.901
33	1.550	1.050	1.100	1.663	1.914	2.334	-.142	-.428	-.905
35	1.650	1.050	1.100	1.677	1.930	2.352	-.140	-.428	-.908
37	1.750	1.050	1.100	1.690	1.944	2.367	-.139	-.428	-.910
39	1.850	1.050	1.100	1.700	1.955	2.380	-.138	-.428	-.912
41	1.950	1.050	1.100	1.710	1.965	2.391	-.137	-.428	-.914
43	2.050	1.050	1.100	1.717	1.974	2.401	-.136	-.428	-.915
45	2.150	1.050	1.100	1.724	1.991	2.409	-.134	-.427	-.915
47	2.250	1.050	1.100	1.730	1.997	2.416	-.133	-.427	-.916
49	2.350	1.050	1.100	1.735	1.993	2.422	-.132	-.426	-.916
51	2.450	1.050	1.100	1.740	1.998	2.427	-.131	-.426	-.916
53	2.550	1.050	1.100	1.744	2.002	2.432	-.130	-.425	-.916
55	2.650	1.050	1.100	1.748	2.006	2.437	-.130	-.425	-.916
57	2.750	1.050	1.100	1.751	2.010	2.440	-.129	-.424	-.916
59	2.850	1.050	1.100	1.754	2.013	2.444	-.128	-.424	-.916
61	2.950	1.050	1.100	1.757	2.015	2.447	-.127	-.423	-.916
63	1.050	1.150	1.100	1.212	1.249	1.311	-.041	-.082	-.151
65	1.150	1.150	1.100	1.414	1.486	1.607	-.080	-.160	-.294
67	1.250	1.150	1.100	1.599	1.703	1.877	-.116	-.231	-.422
69	1.350	1.150	1.100	1.764	1.895	1.113	-.147	-.292	-.533
71	1.450	1.150	1.100	1.965	1.058	1.313	-.173	-.343	-.626
73	1.550	1.150	1.100	1.124	1.195	1.480	-.194	-.384	-.700
75	1.650	1.150	1.100	1.123	1.309	1.617	-.210	-.416	-.760
77	1.750	1.150	1.100	1.264	1.461	1.728	-.223	-.442	-.806
79	1.850	1.150	1.100	1.271	1.476	1.818	-.232	-.461	-.843
81	1.950	1.150	1.100	1.326	1.538	1.891	-.239	-.476	-.871
83	1.050	1.150	1.100	1.375	1.538	1.951	-.244	-.487	-.892
85	1.150	1.150	1.100	1.467	1.629	1.999	-.247	-.496	-.909
87	1.250	1.150	1.100	1.433	1.653	2.038	-.250	-.502	-.922
89	1.350	1.150	1.100	1.483	1.691	2.071	-.251	-.507	-.933
91	1.450	1.150	1.100	1.464	1.714	2.098	-.252	-.510	-.941
93	1.550	1.150	1.100	1.502	1.734	2.121	-.252	-.513	-.947
95	1.650	1.150	1.100	1.517	1.751	2.140	-.253	-.515	-.952
97	1.750	1.150	1.100	1.530	1.765	2.156	-.252	-.516	-.955
99	1.850	1.150	1.100	1.551	1.777	2.170	-.252	-.517	-.958
101	1.950	1.150	1.100	1.561	1.787	2.181	-.252	-.518	-.961
103	2.050	1.150	1.100	1.659	1.796	2.191	-.251	-.518	-.963
105	2.150	1.150	1.100	1.655	1.809	2.200	-.251	-.518	-.964
107	2.250	1.150	1.100	1.672	1.811	2.208	-.250	-.518	-.965
109	2.350	1.150	1.100	1.673	1.816	2.214	-.249	-.518	-.966
111	2.450	1.150	1.100	1.683	1.822	2.220	-.249	-.518	-.967
113	2.550	1.150	1.100	1.697	1.826	2.225	-.249	-.518	-.967
115	2.650	1.150	1.100	1.691	1.830	2.230	-.248	-.518	-.968
117	2.750	1.150	1.100	1.694	1.834	2.234	-.247	-.517	-.968
119	2.850	1.150	1.100	1.697	1.837	2.238	-.246	-.517	-.968

UET

1	2.750	1.150	.100	1.600	1.840	2.241	-.246	-.517	-.969	2
2	.350	1.250	.100	.162	.214	.268	-.099	-.084	-.142	4
3	.150	1.250	.100	.157	.420	.524	-.096	-.164	-.278	6
4	.250	1.250	.100	.520	.610	.761	-.139	-.238	-.403	8
5	.350	1.250	.100	.566	.780	.971	-.176	-.302	-.512	10
6	.450	1.250	.100	.793	.928	1.154	-.209	-.357	-.605	12
7	.550	1.250	.100	.902	1.055	1.308	-.236	-.403	-.682	14
8	.650	1.250	.100	.995	1.161	1.438	-.258	-.440	-.745	16
9	.750	1.250	.100	1.072	1.249	1.544	-.275	-.470	-.796	18
10	.850	1.250	.100	1.136	1.322	1.632	-.289	-.494	-.836	20
11	.950	1.250	.100	1.189	1.382	1.704	-.299	-.512	-.868	22
12	1.050	1.250	.100	1.233	1.432	1.764	-.307	-.527	-.894	24
13	1.150	1.250	.100	1.270	1.473	1.813	-.313	-.538	-.914	26
14	1.250	1.250	.100	1.301	1.508	1.853	-.318	-.547	-.930	28
15	1.350	1.250	.100	1.326	1.536	1.887	-.321	-.554	-.942	30
16	1.450	1.250	.100	1.348	1.560	1.915	-.324	-.559	-.952	32
17	1.550	1.250	.100	1.366	1.581	1.938	-.325	-.564	-.960	34
18	1.650	1.250	.100	1.382	1.598	1.958	-.327	-.567	-.967	36
19	1.750	1.250	.100	1.395	1.613	1.975	-.328	-.569	-.972	38
20	1.850	1.250	.100	1.406	1.625	1.990	-.328	-.571	-.976	40
21	1.950	1.250	.100	1.416	1.636	2.002	-.328	-.573	-.980	42
22	2.050	1.250	.100	1.425	1.645	2.013	-.329	-.574	-.983	44
23	2.150	1.250	.100	1.432	1.653	2.022	-.329	-.575	-.985	46
24	2.250	1.250	.100	1.439	1.661	2.030	-.328	-.575	-.987	48
25	2.350	1.250	.100	1.445	1.667	2.037	-.328	-.576	-.988	50
26	2.450	1.250	.100	1.450	1.672	2.043	-.328	-.576	-.990	52
27	2.550	1.250	.100	1.454	1.677	2.049	-.328	-.576	-.991	54
28	2.650	1.250	.100	1.459	1.682	2.054	-.328	-.576	-.991	56
29	2.750	1.250	.100	1.462	1.685	2.058	-.327	-.576	-.992	58
30	2.850	1.250	.100	1.465	1.689	2.062	-.327	-.576	-.993	60
31	2.950	1.250	.100	1.469	1.692	2.065	-.327	-.576	-.993	62
32	3.050	1.350	.100	1.150	1.186	.233	-.052	-.083	-.133	64
33	.150	1.350	.100	.311	.366	.457	-.103	-.162	-.261	66
34	.250	1.350	.100	.455	.534	.636	-.149	-.235	-.379	68
35	.350	1.350	.100	.585	.686	.855	-.191	-.301	-.485	70
36	.450	1.350	.100	.700	.820	1.021	-.227	-.358	-.576	72
37	.550	1.350	.100	.801	.937	1.164	-.258	-.407	-.654	74
38	.650	1.350	.100	.887	1.036	1.205	-.284	-.447	-.719	76
39	.750	1.350	.100	.960	1.120	1.387	-.305	-.480	-.772	78
40	.850	1.350	.100	1.021	1.190	1.472	-.321	-.506	-.815	80
41	.950	1.350	.100	1.073	1.249	1.543	-.335	-.528	-.850	82
42	1.050	1.350	.100	1.116	1.298	1.602	-.345	-.545	-.878	84
43	1.150	1.350	.100	1.153	1.340	1.651	-.354	-.559	-.901	86
44	1.250	1.350	.100	1.183	1.374	1.692	-.360	-.570	-.920	88
45	1.350	1.350	.100	1.209	1.403	1.727	-.366	-.579	-.934	90
46	1.450	1.350	.100	1.231	1.428	1.756	-.370	-.586	-.947	92
47	1.550	1.350	.100	1.250	1.449	1.740	-.373	-.592	-.956	94
48	1.650	1.350	.100	1.265	1.466	1.801	-.375	-.596	-.964	96
49	1.750	1.350	.100	1.279	1.481	1.819	-.377	-.600	-.971	98
50	1.850	1.350	.100	1.291	1.495	1.834	-.378	-.603	-.976	100
51	1.950	1.350	.100	1.301	1.506	1.847	-.379	-.605	-.981	102
52	2.050	1.350	.100	1.310	1.516	1.858	-.380	-.607	-.984	104
53	2.150	1.350	.100	1.316	1.524	1.868	-.381	-.608	-.988	106
54	2.250	1.350	.100	1.325	1.532	1.877	-.381	-.609	-.990	108
55	2.350	1.350	.100	1.331	1.538	1.884	-.381	-.610	-.992	110
56	2.450	1.350	.100	1.336	1.544	1.891	-.382	-.611	-.994	112
57	2.550	1.350	.100	1.341	1.549	1.897	-.382	-.612	-.995	114
58	2.650	1.350	.100	1.345	1.554	1.902	-.382	-.612	-.997	116
59	2.750	1.350	.100	1.349	1.558	1.906	-.382	-.613	-.998	118
60	2.850	1.350	.100	1.352	1.561	1.910	-.381	-.613	-.999	120

HIRSH

1	2.750	1.350	.100	1.355	1.865	1.914	-.391	-.613	-.999	4
2	.150	1.450	.150	1.137	.163	.204	-.053	-.080	-.124	6
3	.150	1.450	.150	.274	.322	.402	-.104	-.156	-.243	8
4	.250	1.450	.100	.401	.471	.588	-.152	-.228	-.354	10
5	.350	1.450	.100	.514	.607	.757	-.196	-.293	-.455	12
6	.450	1.450	.100	.622	.730	.909	-.234	-.351	-.544	14
7	.550	1.450	.100	.715	.837	1.041	-.268	-.400	-.621	16
8	.650	1.450	.100	.795	.930	1.155	-.296	-.442	-.686	18
9	.750	1.450	.100	.864	1.009	1.252	-.319	-.477	-.740	20
10	.850	1.450	.100	.923	1.077	1.334	-.338	-.506	-.785	22
11	.950	1.450	.100	.973	1.134	1.404	-.354	-.530	-.823	24
12	1.050	1.450	.100	1.015	1.183	1.462	-.367	-.549	-.853	26
13	1.150	1.450	.100	1.051	1.223	1.511	-.377	-.565	-.878	28
14	1.250	1.450	.100	1.081	1.258	1.552	-.386	-.578	-.899	30
15	1.350	1.450	.100	1.107	1.287	1.587	-.392	-.589	-.915	32
16	1.450	1.450	.100	1.129	1.312	1.617	-.398	-.597	-.929	34
17	1.550	1.450	.100	1.149	1.333	1.642	-.402	-.604	-.941	36
18	1.650	1.450	.100	1.165	1.352	1.663	-.406	-.610	-.950	38
19	1.750	1.450	.100	1.179	1.357	1.682	-.408	-.615	-.958	40
20	1.850	1.450	.100	1.191	1.361	1.697	-.411	-.618	-.965	42
21	1.950	1.450	.100	1.201	1.362	1.711	-.412	-.621	-.970	44
22	2.050	1.450	.100	1.210	1.403	1.723	-.414	-.624	-.974	46
23	2.150	1.450	.100	1.219	1.412	1.733	-.415	-.626	-.978	48
24	2.250	1.450	.100	1.225	1.419	1.742	-.416	-.628	-.982	50
25	2.350	1.450	.100	1.232	1.426	1.750	-.416	-.629	-.984	52
26	2.450	1.450	.100	1.237	1.432	1.757	-.417	-.631	-.987	54
27	2.550	1.450	.100	1.242	1.438	1.764	-.417	-.632	-.988	56
28	2.650	1.450	.100	1.247	1.443	1.769	-.418	-.632	-.990	58
29	2.750	1.450	.100	1.251	1.447	1.774	-.418	-.633	-.992	60
30	2.850	1.450	.100	1.254	1.451	1.778	-.418	-.634	-.993	62
31	2.950	1.450	.100	1.257	1.454	1.782	-.418	-.634	-.994	64
32	.050	1.550	.100	.123	.145	.181	-.052	-.076	-.115	66
33	.150	1.550	.100	.243	.285	.356	-.103	-.149	-.226	68
34	.250	1.550	.100	.355	.418	.522	-.151	-.218	-.330	70
35	.350	1.550	.100	.451	.541	.675	-.195	-.282	-.426	72
36	.450	1.550	.100	.555	.663	.813	-.235	-.338	-.511	74
37	.550	1.550	.100	.641	.752	.936	-.269	-.388	-.586	76
38	.650	1.550	.100	.716	.839	1.043	-.299	-.431	-.650	78
39	.750	1.550	.100	.781	.914	1.135	-.324	-.467	-.705	80
40	.850	1.550	.100	.837	.979	1.214	-.345	-.497	-.751	82
41	.950	1.550	.100	.885	1.034	1.281	-.363	-.523	-.790	84
42	1.050	1.550	.100	.927	1.081	1.339	-.377	-.544	-.822	86
43	1.150	1.550	.100	.962	1.122	1.397	-.389	-.562	-.849	88
44	1.250	1.550	.100	.992	1.156	1.429	-.399	-.576	-.871	90
45	1.350	1.550	.100	1.018	1.185	1.464	-.407	-.588	-.890	92
46	1.450	1.550	.100	1.041	1.211	1.494	-.414	-.598	-.905	94
47	1.550	1.550	.100	1.060	1.232	1.520	-.419	-.606	-.918	96
48	1.650	1.550	.100	1.075	1.251	1.542	-.424	-.613	-.929	98
49	1.750	1.550	.100	1.090	1.267	1.561	-.427	-.619	-.938	100
50	1.850	1.550	.100	1.103	1.281	1.577	-.430	-.623	-.945	102
51	1.950	1.550	.100	1.114	1.293	1.591	-.433	-.627	-.951	104
52	2.050	1.550	.100	1.123	1.303	1.604	-.435	-.630	-.957	106
53	2.150	1.550	.100	1.132	1.313	1.615	-.436	-.633	-.961	108
54	2.250	1.550	.100	1.139	1.321	1.624	-.438	-.636	-.965	110
55	2.350	1.550	.100	1.145	1.328	1.632	-.439	-.637	-.969	112
56	2.450	1.550	.100	1.151	1.334	1.640	-.440	-.639	-.971	114
57	2.550	1.550	.100	1.155	1.340	1.646	-.440	-.640	-.974	116
58	2.650	1.550	.100	1.161	1.345	1.652	-.441	-.642	-.976	118
59	2.750	1.550	.100	1.165	1.350	1.657	-.441	-.643	-.978	120
60	2.850	1.550	.100	1.169	1.354	1.662	-.442	-.643	-.979	122

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2.950	1.550	.100	1.172	1.337	1.666	-.442	-.644	-.981
.950	1.550	.100	.139	.129	.161	-.051	-.072	-.106
.150	1.550	.100	.218	.254	.318	-.101	-.141	-.209
.250	1.550	.100	.313	.374	.467	-.143	-.207	-.307
.350	1.550	.100	.413	.485	.606	-.191	-.268	-.397
.450	1.550	.100	.500	.597	.732	-.230	-.324	-.479
.550	1.550	.100	.579	.679	.845	-.265	-.372	-.551
.650	1.550	.100	.648	.760	.945	-.296	-.415	-.614
.750	1.550	.100	.710	.831	1.033	-.322	-.452	-.669
.850	1.550	.100	.763	.893	1.109	-.345	-.484	-.715
.950	1.550	.100	.810	.946	1.174	-.364	-.510	-.755
1.050	1.550	.100	.850	.992	1.230	-.379	-.533	-.788
1.150	1.550	.100	.884	1.032	1.278	-.393	-.552	-.816
1.250	1.550	.100	.914	1.066	1.319	-.404	-.567	-.840
1.350	1.550	.100	.940	1.095	1.355	-.413	-.581	-.860
1.450	1.550	.100	.962	1.121	1.385	-.421	-.592	-.876
1.550	1.550	.100	.981	1.143	1.411	-.427	-.601	-.890
1.650	1.550	.100	.993	1.161	1.434	-.433	-.609	-.902
1.750	1.550	.100	1.013	1.176	1.453	-.437	-.615	-.912
1.850	1.550	.100	1.025	1.192	1.470	-.441	-.621	-.921
1.950	1.550	.100	1.035	1.205	1.485	-.444	-.625	-.928
2.050	1.550	.100	1.043	1.215	1.498	-.446	-.629	-.934
2.150	1.550	.100	1.055	1.225	1.509	-.449	-.633	-.939
2.250	1.550	.100	1.062	1.233	1.519	-.450	-.635	-.944
2.350	1.550	.100	1.069	1.241	1.528	-.452	-.638	-.948
2.450	1.550	.100	1.075	1.248	1.535	-.453	-.640	-.951
2.550	1.550	.100	1.080	1.253	1.542	-.454	-.642	-.954
2.650	1.550	.100	1.085	1.259	1.548	-.455	-.643	-.957
2.750	1.550	.100	1.089	1.263	1.554	-.456	-.644	-.959
2.850	1.550	.100	1.093	1.268	1.559	-.456	-.646	-.961
2.950	1.550	.100	1.096	1.271	1.563	-.457	-.646	-.962
.050	1.750	.100	.093	.115	.144	-.049	-.067	-.098
.150	1.750	.100	.194	.228	.265	-.097	-.133	-.194
.250	1.750	.100	.266	.336	.420	-.142	-.196	-.285
.350	1.750	.100	.372	.438	.546	-.185	-.254	-.370
.450	1.750	.100	.452	.531	.662	-.224	-.308	-.447
.550	1.750	.100	.525	.615	.767	-.259	-.356	-.517
.650	1.750	.100	.593	.671	.861	-.289	-.398	-.579
.750	1.750	.100	.647	.730	.943	-.316	-.435	-.632
.850	1.750	.100	.698	.817	1.016	-.340	-.467	-.679
.950	1.750	.100	.743	.869	1.079	-.359	-.494	-.719
1.050	1.750	.100	.782	.914	1.134	-.376	-.518	-.753
1.150	1.750	.100	.815	.952	1.181	-.391	-.537	-.782
1.250	1.750	.100	.845	.986	1.222	-.403	-.554	-.807
1.350	1.750	.100	.870	1.015	1.257	-.413	-.569	-.828
1.450	1.750	.100	.892	1.041	1.283	-.422	-.581	-.845
1.550	1.750	.100	.912	1.063	1.314	-.429	-.591	-.860
1.650	1.750	.100	.929	1.082	1.337	-.435	-.600	-.873
1.750	1.750	.100	.943	1.098	1.357	-.440	-.607	-.884
1.850	1.750	.100	.956	1.113	1.374	-.445	-.613	-.894
1.950	1.750	.100	.967	1.126	1.389	-.448	-.618	-.902
2.050	1.750	.100	.977	1.137	1.403	-.452	-.623	-.909
2.150	1.750	.100	.986	1.147	1.414	-.454	-.627	-.915
2.250	1.750	.100	.994	1.155	1.425	-.456	-.630	-.920
2.350	1.750	.100	1.001	1.163	1.434	-.458	-.633	-.924
2.450	1.750	.100	1.007	1.170	1.442	-.460	-.635	-.928
2.550	1.750	.100	1.012	1.176	1.449	-.461	-.638	-.931
2.650	1.750	.100	1.017	1.182	1.456	-.463	-.639	-.934
2.750	1.750	.100	1.022	1.187	1.461	-.464	-.641	-.937
2.850	1.750	.100	1.025	1.191	1.466	-.464	-.642	-.939

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2.950	1.750	.100	1.329	1.175	1.471	-.465	-.643	-.941
.950	1.550	.100	.333	.104	.130	-.047	-.063	-.091
.150	1.350	.100	.175	.210	.257	-.093	-.125	-.180
.250	1.550	.100	.253	.334	.300	-.136	-.185	-.265
.350	1.550	.100	.337	.476	.495	-.178	-.240	-.345
.450	1.550	.100	.410	.432	.601	-.216	-.292	-.418
.550	1.550	.100	.477	.550	.699	-.250	-.338	-.485
.650	1.550	.100	.533	.631	.786	-.281	-.380	-.544
.750	1.550	.100	.593	.695	.865	-.308	-.416	-.597
.850	1.550	.100	.641	.751	.934	-.331	-.448	-.643
.950	1.550	.100	.684	.830	.994	-.352	-.476	-.683
1.050	1.550	.100	.721	.844	1.048	-.370	-.500	-.717
1.150	1.550	.100	.754	.881	1.094	-.385	-.521	-.747
1.250	1.550	.100	.783	.915	1.134	-.398	-.538	-.772
1.350	1.550	.100	.804	.944	1.169	-.409	-.553	-.794
1.450	1.550	.100	.832	.969	1.200	-.418	-.566	-.813
1.550	1.550	.100	.849	.991	1.227	-.426	-.577	-.829
1.650	1.550	.100	.865	1.010	1.250	-.433	-.587	-.843
1.750	1.550	.100	.881	1.027	1.270	-.439	-.595	-.855
1.850	1.550	.100	.894	1.042	1.288	-.444	-.602	-.865
1.950	1.550	.100	.906	1.055	1.303	-.448	-.608	-.874
2.050	1.550	.100	.915	1.066	1.317	-.452	-.613	-.881
2.150	1.550	.100	.925	1.076	1.329	-.455	-.617	-.888
2.250	1.550	.100	.933	1.085	1.340	-.458	-.621	-.893
2.350	1.550	.100	.940	1.093	1.349	-.460	-.624	-.898
2.450	1.550	.100	.945	1.100	1.358	-.462	-.627	-.903
2.550	1.550	.100	.952	1.107	1.365	-.464	-.630	-.906
2.650	1.550	.100	.957	1.113	1.372	-.465	-.632	-.910
2.750	1.550	.100	.961	1.118	1.378	-.466	-.634	-.913
2.850	1.550	.100	.965	1.122	1.383	-.467	-.635	-.915
2.950	1.550	.100	.969	1.126	1.388	-.468	-.637	-.917
.050	1.750	.100	.380	.894	.118	-.045	-.059	-.084
.150	1.750	.100	.159	.187	.233	-.088	-.118	-.167
.250	1.750	.100	.235	.276	.345	-.130	-.174	-.246
.350	1.750	.100	.307	.361	.450	-.170	-.227	-.321
.450	1.750	.100	.374	.440	.548	-.207	-.276	-.391
.550	1.750	.100	.435	.512	.639	-.240	-.321	-.455
.650	1.750	.100	.493	.579	.721	-.270	-.361	-.512
.750	1.750	.100	.549	.638	.795	-.297	-.397	-.563
.850	1.750	.100	.605	.692	.861	-.321	-.429	-.608
.950	1.750	.100	.631	.739	.919	-.342	-.457	-.648
1.050	1.750	.100	.667	.731	.971	-.361	-.481	-.682
1.150	1.750	.100	.699	.818	1.016	-.376	-.502	-.712
1.250	1.750	.100	.727	.850	1.056	-.390	-.521	-.739
1.350	1.750	.100	.752	.879	1.093	-.402	-.536	-.761
1.450	1.750	.100	.774	.904	1.121	-.412	-.550	-.780
1.550	1.750	.100	.793	.926	1.147	-.420	-.562	-.797
1.650	1.750	.100	.810	.945	1.171	-.428	-.572	-.812
1.750	1.750	.100	.825	.962	1.191	-.434	-.581	-.824
1.850	1.750	.100	.835	.977	1.209	-.440	-.588	-.835
1.950	1.750	.100	.850	.991	1.225	-.445	-.595	-.845
2.050	1.750	.100	.865	1.004	1.239	-.449	-.600	-.853
2.150	1.750	.100	.869	1.013	1.252	-.452	-.605	-.860
2.250	1.750	.100	.877	1.022	1.263	-.455	-.609	-.866
2.350	1.750	.100	.885	1.030	1.273	-.458	-.613	-.872
2.450	1.750	.100	.891	1.038	1.281	-.460	-.616	-.876
2.550	1.750	.100	.897	1.044	1.289	-.462	-.619	-.881
2.650	1.750	.100	.902	1.050	1.296	-.464	-.622	-.884
2.750	1.750	.100	.907	1.055	1.302	-.466	-.624	-.888
2.850	1.750	.100	.911	1.060	1.308	-.467	-.626	-.890

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3	2.950	1.950	.100	.715	1.064	1.313	-.458	-.627	-.893
5	.050	2.050	.100	.073	.036	.107	-.042	-.056	-.078
	.150	2.050	.100	.145	.170	.213	-.084	-.111	-.155
	.250	2.050	.100	.214	.252	.314	-.124	-.163	-.230
	.350	2.050	.100	.280	.329	.411	-.162	-.214	-.300
8	.450	2.050	.100	.342	.402	.502	-.197	-.260	-.366
	.550	2.050	.100	.400	.470	.586	-.230	-.304	-.426
11	.650	2.050	.100	.453	.532	.663	-.260	-.343	-.481
	.750	2.050	.100	.501	.588	.733	-.286	-.378	-.531
12	.850	2.050	.100	.545	.639	.796	-.310	-.410	-.575
	.950	2.050	.100	.584	.684	.852	-.331	-.437	-.614
15	1.050	2.050	.100	.619	.725	.902	-.350	-.462	-.649
	1.150	2.050	.100	.650	.761	.946	-.366	-.483	-.679
17	1.250	2.050	.100	.677	.793	.985	-.380	-.502	-.705
	1.350	2.050	.100	.702	.821	1.019	-.392	-.518	-.728
18	1.450	2.050	.100	.723	.846	1.049	-.403	-.533	-.748
	1.550	2.050	.100	.742	.867	1.076	-.412	-.545	-.766
21	1.650	2.050	.100	.759	.883	1.099	-.420	-.556	-.781
	1.750	2.050	.100	.774	.904	1.120	-.427	-.565	-.794
23	1.850	2.050	.100	.787	.919	1.138	-.433	-.573	-.805
	1.950	2.050	.100	.797	.932	1.154	-.439	-.580	-.815
25	2.050	2.050	.100	.810	.944	1.169	-.443	-.586	-.824
	2.150	2.050	.100	.819	.955	1.181	-.447	-.591	-.832
27	2.250	2.050	.100	.827	.964	1.193	-.450	-.596	-.839
	2.350	2.050	.100	.835	.973	1.203	-.453	-.600	-.844
29	2.450	2.050	.100	.841	.980	1.212	-.456	-.604	-.850
	2.550	2.050	.100	.847	.987	1.220	-.458	-.607	-.854
31	2.650	2.050	.100	.853	.993	1.227	-.460	-.610	-.858
	2.750	2.050	.100	.858	.997	1.234	-.462	-.612	-.862
33	2.850	2.050	.100	.862	1.004	1.240	-.464	-.614	-.865
	2.950	2.050	.100	.866	1.008	1.245	-.465	-.616	-.868
35	.050	2.150	.100	.057	.078	.098	-.040	-.052	-.073
	.150	2.150	.100	.132	.156	.174	-.079	-.104	-.145
37	.250	2.150	.100	.195	.230	.268	-.118	-.154	-.214
	.350	2.150	.100	.257	.302	.377	-.154	-.201	-.280
39	.450	2.150	.100	.314	.370	.461	-.188	-.246	-.342
	.550	2.150	.100	.358	.433	.540	-.220	-.287	-.400
41	.650	2.150	.100	.418	.491	.612	-.244	-.325	-.453
	.750	2.150	.100	.463	.544	.678	-.275	-.360	-.501
43	.850	2.150	.100	.505	.592	.738	-.298	-.390	-.544
	.950	2.150	.100	.542	.635	.791	-.320	-.418	-.582
45	1.050	2.150	.100	.575	.674	.839	-.338	-.442	-.616
	1.150	2.150	.100	.606	.709	.882	-.355	-.464	-.646
47	1.250	2.150	.100	.632	.740	.920	-.369	-.483	-.673
	1.350	2.150	.100	.655	.766	.954	-.382	-.500	-.696
49	1.450	2.150	.100	.677	.792	.984	-.393	-.514	-.717
	1.550	2.150	.100	.696	.814	1.010	-.403	-.527	-.734
51	1.650	2.150	.100	.713	.833	1.034	-.411	-.538	-.750
	1.750	2.150	.100	.728	.851	1.055	-.419	-.548	-.764
53	1.850	2.150	.100	.741	.866	1.073	-.425	-.557	-.776
	1.950	2.150	.100	.753	.879	1.089	-.431	-.564	-.786
55	2.050	2.150	.100	.754	.891	1.104	-.436	-.571	-.796
	2.150	2.150	.100	.773	.912	1.117	-.440	-.576	-.804
57	2.250	2.150	.100	.782	.912	1.129	-.444	-.581	-.811
	2.350	2.150	.100	.789	.920	1.139	-.447	-.586	-.817
59	2.450	2.150	.100	.795	.924	1.148	-.450	-.590	-.823
	2.550	2.150	.100	.802	.935	1.157	-.452	-.593	-.828
61	2.650	2.150	.100	.808	.941	1.164	-.455	-.596	-.832
	2.750	2.150	.100	.813	.947	1.171	-.457	-.599	-.836
63	2.850	2.150	.100	.817	.952	1.177	-.458	-.601	-.840

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3	2.250	2.150	.100	.321	.937	1.102	-.160	-.603	-.843	2
5	.350	2.250	.100	.351	.972	.990	-.030	-.049	-.068	4
7	.150	2.250	.100	.121	.193	.170	-.075	-.098	-.135	6
9	.250	2.250	.100	.180	.212	.264	-.111	-.145	-.200	8
11	.350	2.250	.100	.235	.276	.317	-.146	-.190	-.262	10
13	.450	2.250	.100	.290	.341	.425	-.179	-.232	-.321	12
15	.550	2.250	.100	.340	.399	.498	-.209	-.272	-.376	14
17	.650	2.250	.100	.386	.454	.566	-.238	-.308	-.426	16
19	.750	2.250	.100	.429	.504	.628	-.263	-.342	-.472	18
21	.850	2.250	.100	.464	.550	.685	-.286	-.372	-.514	20
23	.950	2.250	.100	.501	.591	.737	-.307	-.399	-.552	22
25	1.050	2.250	.100	.536	.629	.783	-.326	-.423	-.585	24
27	1.150	2.250	.100	.565	.663	.824	-.343	-.445	-.615	26
29	1.250	2.250	.100	.592	.693	.862	-.357	-.464	-.642	28
31	1.350	2.250	.100	.615	.720	.895	-.370	-.481	-.665	30
33	1.450	2.250	.100	.636	.744	.924	-.382	-.496	-.686	32
35	1.550	2.250	.100	.654	.765	.951	-.392	-.509	-.704	34
37	1.650	2.250	.100	.671	.785	.974	-.401	-.521	-.720	36
39	1.750	2.250	.100	.686	.802	.995	-.409	-.531	-.734	38
41	1.850	2.250	.100	.699	.817	1.013	-.415	-.540	-.747	40
43	1.950	2.250	.100	.711	.831	1.030	-.421	-.548	-.758	42
45	2.050	2.250	.100	.722	.843	1.045	-.427	-.555	-.768	44
47	2.150	2.250	.100	.731	.854	1.058	-.431	-.561	-.776	46
49	2.250	2.250	.100	.740	.864	1.070	-.435	-.566	-.784	48
51	2.350	2.250	.100	.748	.872	1.080	-.439	-.571	-.790	50
53	2.450	2.250	.100	.754	.880	1.090	-.442	-.575	-.796	52
55	2.550	2.250	.100	.761	.887	1.096	-.445	-.579	-.802	54
57	2.650	2.250	.100	.765	.894	1.106	-.448	-.582	-.806	56
59	2.750	2.250	.100	.772	.900	1.113	-.450	-.585	-.811	58
61	2.850	2.250	.100	.776	.905	1.119	-.452	-.588	-.814	60
63	2.950	2.250	.100	.780	.910	1.125	-.453	-.590	-.818	62
65	3.050	2.250	.100	.785	.915	1.133	-.455	-.593	-.822	
67	3.150	2.250	.100	.789	.920	1.140	-.457	-.595	-.825	
69	3.250	2.250	.100	.793	.925	1.147	-.459	-.597	-.828	
71	3.350	2.250	.100	.797	.930	1.154	-.461	-.599	-.831	
73	3.450	2.250	.100	.801	.935	1.161	-.463	-.601	-.834	
75	3.550	2.250	.100	.805	.940	1.168	-.465	-.603	-.837	
77	3.650	2.250	.100	.809	.945	1.175	-.467	-.605	-.840	
79	3.750	2.250	.100	.813	.950	1.182	-.469	-.607	-.843	
81	3.850	2.250	.100	.817	.955	1.189	-.471	-.609	-.846	
83	3.950	2.250	.100	.821	.960	1.196	-.473	-.611	-.849	
85	4.050	2.250	.100	.825	.965	1.203	-.475	-.613	-.852	
87	4.150	2.250	.100	.829	.970	1.210	-.477	-.615	-.855	
89	4.250	2.250	.100	.833	.975	1.217	-.479	-.617	-.858	
91	4.350	2.250	.100	.837	.980	1.224	-.481	-.619	-.861	
93	4.450	2.250	.100	.841	.985	1.231	-.483	-.621	-.864	
95	4.550	2.250	.100	.845	.990	1.238	-.485	-.623	-.867	
97	4.650	2.250	.100	.849	.995	1.245	-.487	-.625	-.870	
99	4.750	2.250	.100	.853	.100	1.252	-.489	-.627	-.873	
101	4.850	2.250	.100	.857	.105	1.259	-.491	-.629	-.876	
103	4.950	2.250	.100	.861	.110	1.266	-.493	-.631	-.879	
105	5.050	2.250	.100	.865	.115	1.273	-.495	-.633	-.882	
107	5.150	2.250	.100	.869	.120	1.280	-.497	-.635	-.885	
109	5.250	2.250	.100	.873	.125	1.287	-.499	-.637	-.888	
111	5.350	2.250	.100	.877	.130	1.294	-.501	-.639	-.891	
113	5.450	2.250	.100	.881	.135	1.301	-.503	-.641	-.894	
115	5.550	2.250	.100	.885	.140	1.308	-.505	-.643	-.897	
117	5.650	2.250	.100	.889	.145	1.315	-.507	-.645	-.900	
119	5.750	2.250	.100	.893	.150	1.322	-.509	-.647	-.903	
121	5.850	2.250	.100	.897	.155	1.329	-.511	-.649	-.906	
123	5.950	2.250	.100	.901	.160	1.336	-.513	-.651	-.909	
125	6.050	2.250	.100	.905	.165	1.343	-.515	-.653	-.912	
127	6.150	2.250	.100	.909	.170	1.350	-.517	-.655	-.915	
129	6.250	2.250	.100	.913	.175	1.357	-.519	-.657	-.918	
131	6.350	2.250	.100	.917	.180	1.364	-.521	-.659	-.921	
133	6.450	2.250	.100	.921	.185	1.371	-.523	-.661	-.924	
135	6.550	2.250	.100	.925	.190	1.378	-.525	-.663	-.927	
137	6.650	2.250	.100	.929	.195	1.385	-.527	-.665	-.930	
139	6.750	2.250	.100	.933	.200	1.392	-.529	-.667	-.933	
141	6.850	2.250	.100	.937	.205	1.399	-.531	-.669	-.936	
143	6.950	2.250	.100	.941	.210	1.406	-.533	-.671	-.939	
145	7.050	2.250	.100	.945	.215	1.413	-.535	-.673	-.942	
147	7.150	2.250	.100	.949	.220	1.420	-.537	-.675	-.945	
149	7.250	2.250	.100	.953	.225	1.427	-.539	-.677	-.948	
151	7.350	2.250	.100	.957	.230	1.434	-.541	-.679	-.951	
153	7.450	2.250	.100	.961	.235	1.441	-.543	-.681	-.954	
155	7.550	2.250	.100	.965	.240	1.448	-.545	-.683	-.957	
157	7.650	2.250	.100	.969	.245	1.455	-.547	-.685	-.960	
159	7.750	2.250	.100	.973	.250	1.462	-.549	-.687	-.963	
161	7.850	2.250	.100	.977	.255	1.469	-.551	-.689	-.966	
163	7.950	2.250	.100	.981	.260	1.476	-.553	-.691	-.969	
165	8.050	2.250	.100	.985	.265	1.483	-.555	-.693	-.972	
167	8.150	2.250	.100	.989	.270	1.490	-.557	-.695	-.975	
169	8.250	2.250	.100	.993	.275	1.497	-.559	-.697	-.978	
171	8.350	2.250	.100	.997	.280	1.504	-.561	-.699	-.981	
173	8.450	2.250	.100	1.001	.285	1.511	-.563	-.701	-.984	
175	8.550	2.250	.100	1.005	.290	1.518	-.565	-.703	-.987	
177	8.650	2.250	.100	1.009	.295	1.525	-.567	-.705	-.990	
179	8.750	2.250	.100	1.013	.300	1.532	-.569	-.707	-.993	
181	8.850	2.250	.100	1.017	.305	1.539	-.571	-.709	-.996	
183	8.950	2.250	.100	1.021	.310	1.546	-.573	-.711	-.999	
185	9.050	2.250	.100	1.025	.315	1.553	-.575	-.713	1.002	
187	9.150	2.250	.100	1.029	.320	1.560	-.577	-.715	1.005	
189	9.250	2.250	.100	1.033	.325	1.567	-.579	-.717	1.008	
191	9.350	2.250	.100	1.037	.330	1.574	-.581	-.719	1.011	
193	9.450	2.250	.100	1.041	.335	1.581	-.583	-.721	1.014	
195	9.550	2.250	.100	1.045	.340	1.588	-.585	-.723	1.017	
197	9.650	2.250	.100	1.049	.345	1.595	-.587	-.725	1.020	
199	9.750	2.250	.100	1.053	.350	1.602	-.589	-.727	1.023	
201	9.850	2.250	.100	1.057	.355	1.609	-.591	-.729	1.026	
203	9.950	2.250	.100	1.061	.360	1.616	-.593	-.731	1.029	
205	10.050	2.250	.100	1.065	.365	1.623	-.595	-.733	1.032	
207	10.150	2.250	.100	1.069	.370	1.630	-.597	-.735	1.035	
209	10.250	2.250	.100	1.073	.375	1.637	-.599	-.737	1.038	
211	10.350	2.250	.100	1.077	.380	1.644	-.601	-.739	1.041	
213	10.450	2.250	.100	1.081	.385	1.651	-.603	-.741	1.044	
215	10.550	2.250	.100	1.085	.390	1.658	-.605	-.743	1.047	
217	10.650	2.250	.100	1.089	.395	1.665	-.607	-.745	1.050	
219	10.750	2.250	.100	1.093	.400	1.672	-.609	-.747	1.053	
221	10.850	2.250	.100	1.097	.405	1.679	-.611	-.749	1.056	
223	10.950	2.250	.100	1.101	.410	1.686	-.613	-.751	1.059	
225	11.050	2.250	.100	1.105	.415	1.693	-.615	-.753	1.062	
227	11.150	2.250	.100	1.109	.420	1.700	-.617	-.755	1.065	
229	11.250	2.250	.100	1.113	.425	1.707	-.619	-.757	1.068	
231	11.350	2.250	.100	1.117	.430	1.714	-.621	-.759	1.071	
233	11.450	2.250	.100	1.121	.435	1.721	-.623	-.761	1.074	
235	11.550	2.250	.100	1.125	.440	1.728	-.625	-.763	1.077	
237	11.650	2.250	.100	1.129	.445	1.735	-.627	-.765	1.080	
239	11.750	2.250	.100	1.133	.450	1.742	-.629	-.767	1.083	
241	11.850	2.250	.100	1.137	.455	1.749	-.631	-.769	1.086	
243	11.950	2.250	.100	1.141	.460	1.756	-.633	-.771	1.089	
245	12.050	2.250	.100	1.145	.465	1.763	-.635	-.773	1.092	
247	12.150	2.250	.100	1.149	.470	1.770	-.637	-.775	1.095	
249	12.250	2.250	.100	1.153	.475					

3	2.750	2.450	.100	.741	.856	1.072	-.446	-.576	-.793
5	.750	2.150	.100	.352	.461	.676	-.034	-.044	-.059
7	.150	2.450	.100	.193	.122	.152	-.067	-.087	-.118
9	.250	2.450	.100	.153	.139	.226	-.100	-.128	-.175
11	.350	2.450	.100	.202	.237	.297	-.132	-.169	-.231
13	.450	2.450	.100	.248	.292	.364	-.162	-.207	-.283
15	.550	2.450	.100	.292	.343	.428	-.190	-.243	-.332
17	.650	2.450	.100	.333	.391	.488	-.216	-.277	-.379
19	.750	2.450	.100	.371	.436	.544	-.241	-.308	-.421
21	.850	2.450	.100	.407	.478	.595	-.263	-.337	-.460
23	.950	2.450	.100	.439	.515	.643	-.283	-.363	-.496
25	1.050	2.450	.100	.469	.550	.685	-.302	-.387	-.528
27	1.150	2.450	.100	.496	.582	.724	-.318	-.408	-.557
29	1.250	2.450	.100	.521	.610	.759	-.333	-.427	-.583
31	1.350	2.450	.100	.543	.636	.791	-.346	-.444	-.607
33	1.450	2.450	.100	.563	.659	.820	-.358	-.459	-.628
35	1.550	2.450	.100	.581	.680	.845	-.369	-.473	-.646
37	1.650	2.450	.100	.597	.699	.869	-.378	-.485	-.663
39	1.750	2.450	.100	.612	.716	.889	-.387	-.496	-.678
41	1.850	2.450	.100	.625	.731	.908	-.394	-.506	-.691
43	1.950	2.450	.100	.637	.745	.925	-.401	-.514	-.703
45	2.050	2.450	.100	.648	.757	.940	-.407	-.522	-.713
47	2.150	2.450	.100	.657	.764	.953	-.412	-.528	-.723
49	2.250	2.450	.100	.665	.778	.965	-.417	-.534	-.731
51	2.350	2.450	.100	.674	.787	.976	-.421	-.540	-.738
53	2.450	2.450	.100	.681	.796	.986	-.424	-.545	-.745
55	2.550	2.450	.100	.688	.803	.995	-.428	-.549	-.751
57	2.650	2.450	.100	.693	.810	1.003	-.431	-.553	-.756
59	2.750	2.450	.100	.699	.816	1.011	-.433	-.556	-.761
61	2.850	2.450	.100	.704	.821	1.017	-.436	-.559	-.765
63	2.950	2.450	.100	.708	.826	1.023	-.438	-.562	-.769
65	.050	2.550	.100	.048	.057	.071	-.032	-.041	-.056
67	.150	2.550	.100	.046	.113	.141	-.064	-.082	-.111
69	.250	2.550	.100	.142	.167	.209	-.095	-.121	-.165
71	.350	2.550	.100	.137	.220	.275	-.125	-.159	-.217
73	.450	2.550	.100	.231	.271	.339	-.154	-.196	-.266
75	.550	2.550	.100	.272	.319	.399	-.181	-.230	-.313
77	.650	2.550	.100	.310	.365	.455	-.206	-.263	-.357
79	.750	2.550	.100	.347	.407	.508	-.230	-.293	-.398
81	.850	2.550	.100	.380	.446	.557	-.251	-.321	-.436
83	.950	2.550	.100	.411	.483	.602	-.271	-.346	-.470
85	1.050	2.550	.100	.440	.516	.643	-.290	-.369	-.502
87	1.150	2.550	.100	.468	.546	.681	-.306	-.390	-.531
89	1.250	2.550	.100	.490	.574	.715	-.321	-.409	-.556
91	1.350	2.550	.100	.511	.599	.746	-.334	-.426	-.580
93	1.450	2.550	.100	.531	.622	.774	-.346	-.442	-.601
95	1.550	2.550	.100	.548	.642	.799	-.357	-.455	-.619
97	1.650	2.550	.100	.565	.661	.822	-.367	-.468	-.636
99	1.750	2.550	.100	.579	.678	.843	-.375	-.479	-.651
101	1.850	2.550	.100	.592	.693	.861	-.383	-.489	-.665
103	1.950	2.550	.100	.604	.707	.878	-.390	-.497	-.677
105	2.050	2.550	.100	.615	.719	.893	-.396	-.505	-.687
107	2.150	2.550	.100	.624	.730	.907	-.401	-.512	-.697
109	2.250	2.550	.100	.633	.740	.919	-.406	-.519	-.706
111	2.350	2.550	.100	.641	.750	.930	-.411	-.524	-.713
113	2.450	2.550	.100	.649	.758	.940	-.415	-.529	-.720
115	2.550	2.550	.100	.655	.765	.949	-.418	-.534	-.726
117	2.650	2.550	.100	.661	.772	.957	-.421	-.538	-.732
119	2.750	2.550	.100	.667	.778	.965	-.424	-.541	-.737
121	2.850	2.550	.100	.671	.784	.972	-.427	-.544	-.742

HRT

1	2.750	2.650	.100	.674	.739	.978	-.429	-.548	-.746
5	2.750	2.650	.100	.715	.653	.866	-.330	-.037	-.052
9	2.750	2.650	.100	.752	.615	.731	-.061	-.077	-.104
13	2.750	2.650	.100	.789	.576	.595	-.193	-.114	-.155
17	2.750	2.650	.100	.826	.538	.456	-.319	-.151	-.204
21	2.750	2.650	.100	.863	.501	.316	-.446	-.185	-.251
25	2.750	2.650	.100	.900	.463	.172	-.572	-.218	-.296
29	2.750	2.650	.100	.937	.425	.025	-.697	-.249	-.338
33	2.750	2.650	.100	.974	.387	.125	-.822	-.278	-.377
37	2.750	2.650	.100	.956	.350	.222	-.947	-.305	-.413
41	2.750	2.650	.100	.919	.313	.319	-.1068	-.330	-.447
45	2.750	2.650	.100	.882	.275	.416	-.231	-.353	-.477
49	2.750	2.650	.100	.845	.238	.513	-.356	-.373	-.505
53	2.750	2.650	.100	.808	.200	.610	-.481	-.392	-.531
57	2.750	2.650	.100	.771	.163	.707	-.606	-.409	-.554
61	2.750	2.650	.100	.734	.125	.804	-.731	-.424	-.575
65	2.750	2.650	.100	.697	.088	.901	-.856	-.438	-.593
69	2.750	2.650	.100	.660	.050	.998	-.981	-.451	-.610
73	2.750	2.650	.100	.623	.013	.095	-.1003	-.462	-.625
77	2.750	2.650	.100	.586	.075	.192	-.225	-.472	-.639
81	2.750	2.650	.100	.549	.138	.289	-.350	-.481	-.651
85	2.750	2.650	.100	.512	.200	.386	-.475	-.489	-.662
89	2.750	2.650	.100	.475	.263	.483	-.600	-.496	-.672
93	2.750	2.650	.100	.438	.325	.580	-.725	-.503	-.681
97	2.750	2.650	.100	.401	.388	.677	-.850	-.509	-.689
101	2.750	2.650	.100	.364	.450	.774	-.975	-.514	-.696
105	2.750	2.650	.100	.327	.513	.871	-.1000	-.519	-.703
109	2.750	2.650	.100	.290	.575	.968	-.125	-.523	-.709
113	2.750	2.650	.100	.253	.638	.065	-.250	-.527	-.714
117	2.750	2.650	.100	.216	.700	.162	-.375	-.530	-.719
121	2.750	2.650	.100	.179	.763	.259	-.500	-.533	-.723
125	2.750	2.650	.100	.142	.825	.356	-.625	-.537	-.728
129	2.750	2.650	.100	.105	.888	.453	-.750	-.540	-.733
133	2.750	2.650	.100	.068	.950	.550	-.875	-.543	-.738
137	2.750	2.650	.100	.031	.013	.647	-.1000	-.546	-.743
141	2.750	2.650	.100	.094	.175	.744	-.225	-.549	-.748
145	2.750	2.650	.100	.157	.238	.841	-.350	-.552	-.753
149	2.750	2.650	.100	.220	.300	.938	-.475	-.555	-.758
153	2.750	2.650	.100	.283	.363	.035	-.600	-.558	-.763
157	2.750	2.650	.100	.346	.425	.132	-.725	-.561	-.768
161	2.750	2.650	.100	.409	.488	.229	-.850	-.564	-.773
165	2.750	2.650	.100	.472	.550	.326	-.975	-.567	-.778
169	2.750	2.650	.100	.535	.613	.423	-.1000	-.570	-.783
173	2.750	2.650	.100	.598	.675	.520	-.125	-.573	-.788
177	2.750	2.650	.100	.661	.738	.617			

1	2.750	2.750	.100	.619	.723	.576	-.410	-.519	-.701
2	.750	2.850	.100	.609	.676	.537	-.027	-.035	-.046
3	.150	2.950	.100	.577	.671	.514	-.055	-.069	-.092
4	.250	2.950	.100	.515	.636	.459	-.081	-.102	-.138
5	.350	2.850	.100	.452	.579	.424	-.107	-.135	-.161
6	.450	2.450	.100	.408	.521	.376	-.132	-.166	-.224
7	.550	2.850	.100	.322	.461	.326	-.156	-.197	-.264
8	.650	2.850	.100	.254	.379	.279	-.179	-.225	-.302
9	.750	2.850	.100	.285	.335	.248	-.200	-.252	-.338
10	.850	2.850	.100	.314	.309	.241	-.220	-.277	-.372
11	.950	2.850	.100	.341	.281	.200	-.230	-.300	-.403
12	1.050	2.850	.100	.365	.240	.156	-.256	-.322	-.432
13	1.150	2.850	.100	.390	.195	.100	-.271	-.342	-.459
14	1.250	2.850	.100	.411	.142	.031	-.286	-.360	-.484
15	1.350	2.850	.100	.431	.085	.030	-.299	-.377	-.506
16	1.450	2.850	.100	.449	.027	.056	-.311	-.392	-.526
17	1.550	2.850	.100	.466	.046	.030	-.322	-.406	-.545
18	1.650	2.850	.100	.481	.034	.000	-.332	-.418	-.562
19	1.750	2.850	.100	.495	.010	.022	-.341	-.430	-.577
20	1.850	2.850	.100	.508	.005	.000	-.349	-.440	-.591
21	1.950	2.850	.100	.519	.008	.000	-.357	-.449	-.604
22	2.050	2.850	.100	.530	.021	.000	-.363	-.458	-.615
23	2.150	2.850	.100	.540	.032	.000	-.369	-.465	-.625
24	2.250	2.850	.100	.549	.042	.000	-.375	-.472	-.635
25	2.350	2.850	.100	.557	.051	.000	-.380	-.478	-.643
26	2.450	2.850	.100	.564	.060	.000	-.384	-.484	-.651
27	2.550	2.850	.100	.571	.068	.000	-.388	-.489	-.658
28	2.650	2.850	.100	.577	.075	.000	-.392	-.494	-.664
29	2.750	2.850	.100	.583	.081	.000	-.395	-.498	-.670
30	2.850	2.850	.100	.588	.087	.000	-.399	-.502	-.675
31	2.950	2.850	.100	.593	.093	.000	-.401	-.505	-.679
32	3.050	2.850	.100	.598	.098	.000	-.402	-.505	-.679
33	3.150	2.850	.100	.603	.103	.000	-.402	-.505	-.679
34	3.250	2.850	.100	.607	.107	.000	-.402	-.505	-.679
35	3.350	2.850	.100	.611	.111	.000	-.401	-.505	-.679
36	3.450	2.850	.100	.615	.115	.000	-.400	-.505	-.679
37	3.550	2.850	.100	.619	.119	.000	-.399	-.505	-.679
38	3.650	2.850	.100	.623	.123	.000	-.397	-.505	-.679
39	3.750	2.850	.100	.627	.127	.000	-.397	-.505	-.679
40	3.850	2.850	.100	.631	.131	.000	-.395	-.505	-.679
41	3.950	2.850	.100	.635	.135	.000	-.395	-.505	-.679
42	4.050	2.850	.100	.639	.139	.000	-.395	-.505	-.679
43	4.150	2.850	.100	.643	.143	.000	-.395	-.505	-.679
44	4.250	2.850	.100	.647	.147	.000	-.395	-.505	-.679
45	4.350	2.850	.100	.651	.151	.000	-.395	-.505	-.679
46	4.450	2.850	.100	.655	.155	.000	-.395	-.505	-.679
47	4.550	2.850	.100	.659	.159	.000	-.395	-.505	-.679
48	4.650	2.850	.100	.663	.163	.000	-.395	-.505	-.679
49	4.750	2.850	.100	.667	.167	.000	-.395	-.505	-.679
50	4.850	2.850	.100	.671	.171	.000	-.395	-.505	-.679
51	4.950	2.850	.100	.675	.175	.000	-.395	-.505	-.679
52	5.050	2.850	.100	.679	.179	.000	-.395	-.505	-.679
53	5.150	2.850	.100	.683	.183	.000	-.395	-.505	-.679
54	5.250	2.850	.100	.687	.187	.000	-.395	-.505	-.679
55	5.350	2.850	.100	.691	.191	.000	-.395	-.505	-.679
56	5.450	2.850	.100	.695	.195	.000	-.395	-.505	-.679
57	5.550	2.850	.100	.699	.199	.000	-.395	-.505	-.679
58	5.650	2.850	.100	.703	.203	.000	-.395	-.505	-.679
59	5.750	2.850	.100	.707	.207	.000	-.395	-.505	-.679
60	5.850	2.850	.100	.711	.211	.000	-.395	-.505	-.679
61	5.950	2.850	.100	.715	.215	.000	-.395	-.505	-.679
62	6.050	2.850	.100	.719	.219	.000	-.395	-.505	-.679
63	6.150	2.850	.100	.723	.223	.000	-.395	-.505	-.679

1	2.250	2.250	.100	.533	.533	.323	-1.391	-1.492	-1.659
3	.150	.150	.200	-1.234	-1.234	-1.560	2.467	2.061	1.051
5	.150	.150	.200	-1.234	-1.234	-1.560	2.467	2.061	1.051
7	.250	.250	.200	7.403	5.942	5.109	13.307	9.870	8.307
9	.350	.350	.200	6.317	7.999	6.452	12.273	11.295	9.665
11	.450	.350	.200	9.643	8.725	7.197	13.974	12.076	10.412
13	.550	.350	.200	10.117	7.109	7.641	13.550	12.540	10.857
15	.650	.350	.200	10.419	7.493	7.924	13.852	12.835	11.139
17	.750	.350	.200	10.522	7.631	8.119	14.355	13.033	11.329
19	.850	.350	.200	10.764	7.820	8.248	14.197	13.172	11.462
21	.950	.350	.200	10.463	7.921	8.345	14.300	13.272	11.559
23	1.050	.350	.200	10.945	7.997	8.417	14.378	13.348	11.632
25	1.150	.350	.200	11.004	10.355	8.473	14.437	13.406	11.687
27	1.250	.350	.200	11.051	10.101	8.517	14.483	13.451	11.731
29	1.350	.350	.200	11.053	10.137	8.552	14.521	13.487	11.766
31	1.450	.350	.200	11.119	10.153	8.586	14.551	13.517	11.794
33	1.550	.350	.200	11.143	10.190	8.613	14.575	13.541	11.817
35	1.650	.350	.200	11.153	10.211	8.625	14.596	13.561	11.836
37	1.750	.350	.200	11.151	10.227	8.637	14.613	13.578	11.852
39	1.850	.350	.200	11.175	10.242	8.653	14.629	13.592	11.866
41	1.950	.350	.200	11.208	10.259	8.664	14.643	13.604	11.878
43	2.050	.350	.200	11.218	10.264	8.674	14.651	13.615	11.888
45	2.150	.350	.200	11.224	10.274	8.683	14.660	13.624	11.897
47	2.250	.350	.200	11.234	10.282	8.691	14.668	13.632	11.904
49	2.350	.350	.200	11.243	10.289	8.698	14.676	13.639	11.911
51	2.450	.350	.200	11.253	10.295	8.704	14.682	13.645	11.917
53	2.550	.350	.200	11.255	10.310	8.719	14.688	13.651	11.922
55	2.650	.350	.200	11.263	10.335	8.714	14.693	13.656	11.927
57	2.750	.350	.200	11.265	10.310	8.718	14.697	13.660	11.931
59	2.850	.350	.200	11.269	10.314	8.722	14.701	13.664	11.935
61	2.950	.350	.200	11.272	10.317	8.725	14.705	13.667	11.939
63	.050	.150	.200	.071	-1.140	-1.442	9.790	9.517	8.729
65	.150	.150	.200	3.002	7.680	2.142	15.319	15.116	13.946
67	.250	.150	.200	5.172	7.798	4.174	19.525	17.826	16.496
69	.350	.150	.200	6.906	5.020	6.353	20.333	19.190	17.786
71	.450	.150	.200	7.137	5.742	6.350	20.906	19.940	18.498
73	.550	.150	.200	7.305	7.132	5.470	21.257	20.398	19.924
75	.650	.150	.200	7.385	7.487	6.751	21.561	20.674	19.196
77	.750	.150	.200	6.394	7.661	6.936	21.757	20.866	19.379
79	.850	.150	.200	6.234	7.776	7.871	21.898	21.002	19.509
81	.950	.150	.200	6.325	7.898	7.167	21.999	21.100	19.603
83	1.050	.150	.200	6.913	7.973	7.240	22.075	21.174	19.673
85	1.150	.150	.200	6.472	7.931	7.295	22.133	21.231	19.728
87	1.250	.150	.200	6.519	3.076	7.340	22.179	21.276	19.771
89	1.350	.150	.200	6.563	1.112	7.375	22.216	21.312	19.805
91	1.450	.150	.200	6.585	3.112	7.403	22.246	21.341	19.832
93	1.550	.150	.200	6.613	3.156	7.426	22.270	21.364	19.855
95	1.650	.150	.200	6.653	3.136	7.446	22.290	21.384	19.874
97	1.750	.150	.200	6.647	3.234	7.462	22.307	21.401	19.890
99	1.850	.150	.200	6.682	1.217	7.476	22.322	21.415	19.903
101	1.950	.150	.200	6.675	6.200	7.486	22.334	21.427	19.915
103	2.050	.150	.200	6.655	3.243	7.493	22.345	21.437	19.925
105	2.150	.150	.200	6.695	3.249	7.507	22.354	21.446	19.934
107	2.250	.150	.200	6.703	3.257	7.515	22.362	21.454	19.941
109	2.350	.150	.200	6.713	3.254	7.521	22.369	21.461	19.948
111	2.450	.150	.200	6.717	3.271	7.527	22.376	21.467	19.954
113	2.550	.150	.200	6.722	3.275	7.533	22.381	21.473	19.959
115	2.650	.150	.200	6.727	3.281	7.534	22.386	21.478	19.964
117	2.750	.150	.200	6.732	3.286	7.542	22.391	21.482	19.968
119	2.850	.150	.200	6.735	3.289	7.546	22.395	21.486	19.972

1105

1	2.250	.100	.200	8.219	7.223	7.517	22.193	21.490	19.975
3	.250	.200	.200	7.257	6.353	6.337	1.403	9.067	7.513
5	.150	.200	.200	1.925	1.433	1.355	13.174	12.840	11.951
7	.250	.200	.200	4.357	3.326	3.275	15.352	15.220	14.166
9	.350	.200	.200	4.353	4.299	4.233	17.131	16.449	15.313
11	.150	.200	.200	4.984	4.418	4.041	17.846	17.137	15.956
13	.550	.200	.200	5.369	5.313	5.234	18.278	17.554	16.347
15	.650	.200	.200	5.640	5.586	5.496	18.556	17.822	16.599
17	.750	.200	.200	5.920	5.772	5.677	19.745	18.004	16.771
19	.350	.200	.200	5.983	5.935	5.807	18.678	18.133	16.893
21	.750	.200	.200	6.063	6.003	5.903	18.975	18.220	16.982
23	1.350	.200	.200	6.138	5.977	5.976	19.349	18.299	17.049
25	1.150	.200	.200	6.197	6.135	6.032	19.105	18.354	17.101
27	1.250	.200	.200	6.243	6.180	6.076	19.150	18.397	17.142
29	1.350	.200	.200	6.279	6.216	6.111	19.186	18.432	17.175
31	1.750	.200	.200	6.337	6.275	6.173	19.214	18.460	17.201
33	1.550	.200	.200	6.334	6.270	6.163	19.230	18.483	17.223
35	1.650	.200	.200	6.353	6.290	6.183	19.258	18.502	17.242
37	1.750	.200	.200	6.372	6.307	6.177	19.275	18.518	17.257
39	1.350	.200	.200	6.367	6.322	6.213	19.289	18.532	17.270
41	1.950	.200	.200	6.397	6.334	6.225	19.301	18.544	17.282
43	2.350	.200	.200	6.410	6.344	6.235	19.312	18.554	17.291
45	2.150	.200	.200	6.419	6.354	6.244	19.321	18.563	17.300
47	2.250	.200	.200	6.423	6.362	6.252	19.327	18.571	17.307
49	2.350	.200	.200	6.435	6.369	6.259	19.336	18.577	17.314
51	2.450	.200	.200	6.441	6.375	6.263	19.342	18.583	17.319
53	2.550	.200	.200	6.447	6.381	6.271	19.347	18.589	17.324
55	2.650	.200	.200	6.452	6.386	6.275	19.352	18.594	17.329
57	2.750	.200	.200	6.456	6.390	6.280	19.357	18.598	17.333
59	2.850	.200	.200	6.461	6.394	6.284	19.361	18.602	17.337
61	2.950	.200	.200	6.464	6.393	6.287	19.364	18.605	17.340
63	.350	.300	.200	.464	.528	.527	5.202	4.968	4.577
65	.150	.300	.200	1.366	1.463	1.524	8.709	8.310	7.646
67	.250	.300	.200	2.357	2.423	2.612	10.675	10.182	9.359
69	.350	.300	.200	3.010	3.150	3.361	11.763	11.217	10.307
71	.450	.300	.200	3.553	3.675	3.877	12.396	11.820	10.859
73	.550	.300	.200	3.936	4.029	4.233	12.787	12.193	11.202
75	.650	.300	.200	4.153	4.275	4.479	13.043	12.437	11.427
77	.750	.300	.200	4.329	4.450	4.653	13.219	12.605	11.582
79	.850	.300	.200	4.457	4.578	4.780	13.344	12.725	11.694
81	.950	.300	.200	4.563	4.674	4.875	13.436	12.813	11.776
83	1.350	.300	.200	4.523	4.717	4.917	13.536	12.880	11.838
85	1.150	.300	.200	4.634	4.804	5.003	13.560	12.932	11.887
87	1.250	.300	.200	4.730	4.819	5.047	13.602	12.973	11.925
89	1.350	.300	.200	4.763	4.835	5.083	13.636	13.006	11.956
91	1.450	.300	.200	4.796	4.919	5.111	13.664	13.033	11.981
93	1.550	.300	.200	4.821	4.937	5.135	13.687	13.055	12.002
95	1.650	.300	.200	4.831	4.959	5.155	13.706	13.074	12.019
97	1.750	.300	.200	4.839	4.976	5.172	13.723	13.089	12.034
99	1.850	.300	.200	4.873	4.971	5.180	13.736	13.103	12.047
101	1.950	.300	.200	4.886	5.033	5.170	13.748	13.114	12.057
103	2.350	.300	.200	4.857	5.014	5.209	13.758	13.124	12.067
105	2.150	.300	.200	4.905	5.023	5.210	13.767	13.133	12.075
107	2.250	.300	.200	4.915	5.031	5.226	13.775	13.140	12.082
109	2.350	.300	.200	4.922	5.039	5.233	13.782	13.147	12.088
111	2.450	.300	.200	4.928	5.045	5.239	13.780	13.153	12.094
113	2.550	.300	.200	4.934	5.051	5.245	13.793	13.158	12.099
115	2.650	.300	.200	4.939	5.056	5.250	13.798	13.163	12.103
117	2.750	.300	.200	4.944	5.060	5.254	13.803	13.167	12.107
119	2.850	.300	.200	4.949	5.064	5.258	13.806	13.171	12.111

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1	2.750	.350	.200	4.952	5.263	5.261	13.310	13.174	12.114
2	.750	.400	.200	4.460	5.112	5.653	3.073	2.903	2.620
3	.750	.450	.200	4.068	4.960	5.401	5.475	5.073	4.571
4	.750	.500	.200	3.676	4.808	5.149	5.828	6.441	5.795
5	.750	.550	.200	3.284	4.656	4.997	6.180	7.263	6.529
6	.750	.600	.200	2.892	4.504	4.845	6.511	7.767	6.979
7	.750	.650	.200	2.500	4.352	4.693	6.843	8.090	7.267
8	.750	.700	.200	2.108	4.200	4.541	7.174	8.306	7.461
9	.750	.750	.200	1.716	4.048	4.389	7.506	8.456	7.597
10	.750	.800	.200	1.324	3.896	4.237	7.837	8.565	7.696
11	.750	.850	.200	0.932	3.744	4.085	8.169	8.646	7.769
12	.750	.900	.200	0.540	3.592	3.933	8.500	8.708	7.826
13	.750	.950	.200	0.148	3.440	3.781	8.832	8.756	7.870
14	.750	1.000	.200	0.000	3.288	3.629	9.164	8.794	7.905
15	.750	1.050	.200	0.000	3.136	3.477	9.496	8.825	7.933
16	.750	1.100	.200	0.000	2.984	3.325	9.828	8.850	7.957
17	.750	1.150	.200	0.000	2.832	3.173	10.160	8.871	7.976
18	.750	1.200	.200	0.000	2.680	3.021	10.492	8.884	7.992
19	.750	1.250	.200	0.000	2.528	2.869	10.824	8.894	8.006
20	.750	1.300	.200	0.000	2.376	2.717	11.156	8.916	8.018
21	.750	1.350	.200	0.000	2.224	2.565	11.488	8.927	8.028
22	.750	1.400	.200	0.000	2.072	2.413	11.820	8.937	8.037
23	.750	1.450	.200	0.000	1.920	2.261	12.152	8.945	8.045
24	.750	1.500	.200	0.000	1.768	2.109	12.484	8.952	8.051
25	.750	1.550	.200	0.000	1.616	1.957	12.816	8.959	8.057
26	.750	1.600	.200	0.000	1.464	1.805	13.148	8.964	8.063
27	.750	1.650	.200	0.000	1.312	1.653	13.480	8.969	8.067
28	.750	1.700	.200	0.000	1.160	1.501	13.812	8.974	8.072
29	.750	1.750	.200	0.000	1.008	1.349	14.144	8.978	8.075
30	.750	1.800	.200	0.000	0.856	1.197	14.476	8.982	8.079
31	.750	1.850	.200	0.000	0.704	1.045	14.808	8.985	8.082
32	.750	1.900	.200	0.000	0.552	0.893	15.140	8.989	8.086
33	.750	1.950	.200	0.000	0.400	0.741	15.472	8.992	8.089
34	.750	2.000	.200	0.000	0.248	0.589	15.804	8.995	8.092
35	.750	2.050	.200	0.000	0.096	0.437	16.136	8.998	8.095
36	.750	2.100	.200	0.000	0.000	0.285	16.468	8.999	8.097
37	.750	2.150	.200	0.000	0.000	0.133	16.800	8.999	8.098
38	.750	2.200	.200	0.000	0.000	0.000	17.132	8.999	8.099
39	.750	2.250	.200	0.000	0.000	0.000	17.464	8.999	8.100
40	.750	2.300	.200	0.000	0.000	0.000	17.796	8.999	8.101
41	.750	2.350	.200	0.000	0.000	0.000	18.128	8.999	8.102
42	.750	2.400	.200	0.000	0.000	0.000	18.460	8.999	8.103
43	.750	2.450	.200	0.000	0.000	0.000	18.792	8.999	8.104
44	.750	2.500	.200	0.000	0.000	0.000	19.124	8.999	8.105
45	.750	2.550	.200	0.000	0.000	0.000	19.456	8.999	8.106
46	.750	2.600	.200	0.000	0.000	0.000	19.788	8.999	8.107
47	.750	2.650	.200	0.000	0.000	0.000	20.120	8.999	8.108
48	.750	2.700	.200	0.000	0.000	0.000	20.452	8.999	8.109
49	.750	2.750	.200	0.000	0.000	0.000	20.784	8.999	8.110
50	.750	2.800	.200	0.000	0.000	0.000	21.116	8.999	8.111
51	.750	2.850	.200	0.000	0.000	0.000	21.448	8.999	8.112
52	.750	2.900	.200	0.000	0.000	0.000	21.780	8.999	8.113
53	.750	2.950	.200	0.000	0.000	0.000	22.112	8.999	8.114
54	.750	3.000	.200	0.000	0.000	0.000	22.444	8.999	8.115
55	.750	3.050	.200	0.000	0.000	0.000	22.776	8.999	8.116
56	.750	3.100	.200	0.000	0.000	0.000	23.108	8.999	8.117
57	.750	3.150	.200	0.000	0.000	0.000	23.440	8.999	8.118
58	.750	3.200	.200	0.000	0.000	0.000	23.772	8.999	8.119
59	.750	3.250	.200	0.000	0.000	0.000	24.104	8.999	8.120
60	.750	3.300	.200	0.000	0.000	0.000	24.436	8.999	8.121
61	.750	3.350	.200	0.000	0.000	0.000	24.768	8.999	8.122
62	.750	3.400	.200	0.000	0.000	0.000	25.100	8.999	8.123
63	.750	3.450	.200	0.000	0.000	0.000	25.432	8.999	8.124

UCT

	1.250	.750	.200	2.250	2.650	1.033	3.110	3.042	2.428
5	1.250	.750	.200	2.250	2.306	1.311	.484	.421	.316
	1.250	.750	.200	2.250	2.317	.613	.717	.799	.596
	1.250	.750	.200	2.250	2.312	1.033	1.200	1.110	.627
	1.250	.750	.200	2.250	2.312	1.378	1.559	1.350	1.004
	1.250	.750	.200	1.130	1.340	1.627	1.768	1.531	1.135
	1.250	.750	.200	1.345	1.523	1.932	1.924	1.665	1.232
11	1.250	.750	.200	1.443	1.674	1.997	2.091	1.765	1.304
	1.250	.750	.200	1.596	1.796	2.130	2.129	1.840	1.360
13	1.250	.750	.200	1.697	1.973	2.236	2.196	1.899	1.403
	1.250	.750	.200	1.761	1.971	2.321	2.249	1.945	1.437
15	1.250	.750	.200	1.822	2.035	2.370	2.291	1.981	1.464
	1.250	.750	.200	1.672	2.037	2.445	2.325	2.011	1.487
17	1.250	.750	.200	1.913	2.130	2.491	2.352	2.035	1.506
	1.250	.750	.200	1.947	2.155	2.529	2.375	2.055	1.522
19	1.250	.750	.200	1.976	2.175	2.555	2.394	2.072	1.535
	1.250	.750	.200	2.033	2.223	2.566	2.410	2.086	1.546
21	1.250	.750	.200	2.020	2.241	2.568	2.424	2.099	1.556
	1.250	.750	.200	2.033	2.259	2.567	2.435	2.109	1.565
23	1.250	.750	.200	2.074	2.274	2.543	2.445	2.113	1.573
	1.250	.750	.200	2.065	2.248	2.557	2.454	2.126	1.579
25	1.250	.750	.200	2.077	2.279	2.569	2.462	2.133	1.585
	1.250	.750	.200	2.097	2.279	2.566	2.469	2.139	1.590
27	1.250	.750	.200	2.099	2.318	2.634	2.475	2.145	1.595
	1.250	.750	.200	2.103	2.326	2.697	2.480	2.150	1.599
29	1.250	.750	.200	2.110	2.333	2.704	2.485	2.154	1.603
	1.250	.750	.200	2.116	2.337	2.710	2.489	2.158	1.607
31	1.250	.750	.200	2.122	2.345	2.716	2.493	2.162	1.610
	1.250	.750	.200	2.127	2.350	2.721	2.497	2.165	1.612
33	1.250	.750	.200	2.131	2.354	2.726	2.500	2.168	1.616
	1.250	.750	.200	2.135	2.356	2.730	2.503	2.171	1.617
35	1.250	.750	.200	2.24	2.36	2.329	2.325	2.273	1.86
	1.250	.750	.200	2.44	2.519	2.445	2.623	2.522	2.355
37	1.250	.750	.200	2.652	2.753	2.936	2.877	2.734	2.496
	1.250	.750	.200	2.813	2.975	3.195	3.081	2.904	2.608
39	1.250	.750	.200	2.912	3.154	3.417	3.290	3.036	2.694
	1.250	.750	.200	3.155	3.425	3.523	3.363	3.137	2.760
41	1.250	.750	.200	3.262	3.650	3.756	3.456	3.214	2.810
	1.250	.750	.200	3.34	3.571	3.881	3.529	3.274	2.850
43	1.250	.750	.200	3.469	3.662	3.933	3.585	3.321	2.881
	1.250	.750	.200	3.519	3.737	3.966	3.633	3.359	2.906
45	1.250	.750	.200	3.577	3.776	3.933	3.666	3.389	2.926
	1.250	.750	.200	3.645	3.849	3.933	3.695	3.413	2.944
47	1.250	.750	.200	3.666	3.871	3.933	3.719	3.439	2.958
	1.250	.750	.200	3.719	3.927	3.927	3.739	3.451	2.971
49	1.250	.750	.200	3.747	3.956	3.904	3.756	3.466	2.981
	1.250	.750	.200	3.771	3.931	3.931	3.771	3.478	2.991
51	1.250	.750	.200	3.772	3.932	3.933	3.793	3.489	2.999
	1.250	.750	.200	3.809	3.921	3.923	3.794	3.498	3.005
53	1.250	.750	.200	3.821	3.936	3.934	3.803	3.506	3.012
	1.250	.750	.200	3.833	3.950	3.934	3.811	3.513	3.018
55	1.250	.750	.200	3.819	3.952	3.916	3.818	3.520	3.023
	1.250	.750	.200	3.857	3.972	3.927	3.824	3.525	3.027
57	1.250	.750	.200	3.863	3.931	3.936	3.830	3.530	3.031
	1.250	.750	.200	3.875	3.909	3.945	3.835	3.535	3.035
59	1.250	.750	.200	3.883	3.976	3.932	3.839	3.539	3.038
	1.250	.750	.200	3.897	3.932	3.959	3.843	3.542	3.041
61	1.250	.750	.200	3.894	3.938	3.954	3.847	3.546	3.044
	1.250	.750	.200	3.894	3.913	3.976	3.850	3.549	3.047
63	1.250	.750	.200	3.904	3.910	3.974	3.853	3.551	3.049

UCT

2	2.950	1.950	2.00	1.938	2.132	2.479	1.356	1.554	1.051
4	1.150	1.050	2.00	1.199	1.727	2.285	1.271	1.177	1.194
6	1.150	1.050	2.00	1.330	1.150	2.280	1.427	1.342	1.200
8	1.250	1.050	2.00	1.504	1.650	1.815	1.607	1.485	1.282
10	1.350	1.050	2.00	1.730	1.218	1.244	1.756	1.603	1.349
12	1.450	1.050	2.00	1.377	1.016	1.244	1.675	1.697	1.401
14	1.550	1.050	2.00	1.309	1.160	1.413	1.970	1.772	1.442
16	1.650	1.050	2.00	1.120	1.293	1.556	1.044	1.630	1.474
18	1.750	1.050	2.00	1.214	1.397	1.674	1.102	1.876	1.499
20	1.850	1.050	2.00	1.293	1.473	1.771	1.149	1.913	1.519
22	1.950	1.050	2.00	1.360	1.544	1.851	1.186	1.942	1.536
24	1.050	1.050	2.00	1.415	1.633	1.916	1.217	1.967	1.551
26	1.150	1.050	2.00	1.461	1.653	1.973	1.241	1.987	1.563
28	1.250	1.050	2.00	1.500	1.675	2.018	1.262	1.004	1.573
30	1.350	1.050	2.00	1.533	1.729	2.056	1.280	1.010	1.582
32	1.450	1.050	2.00	1.561	1.759	2.088	1.294	1.030	1.590
34	1.550	1.050	2.00	1.585	1.784	2.115	1.307	1.041	1.597
36	1.650	1.050	2.00	1.605	1.805	2.139	1.318	1.050	1.604
38	1.750	1.050	2.00	1.623	1.824	2.158	1.327	1.058	1.609
40	1.850	1.050	2.00	1.636	1.840	2.175	1.335	1.065	1.614
42	1.950	1.050	2.00	1.651	1.853	2.190	1.343	1.071	1.619
44	2.050	1.050	2.00	1.663	1.865	2.203	1.349	1.077	1.623
46	2.150	1.050	2.00	1.673	1.875	2.214	1.355	1.082	1.627
48	2.250	1.050	2.00	1.682	1.885	2.224	1.360	1.086	1.630
50	2.350	1.050	2.00	1.690	1.893	2.232	1.364	1.090	1.633
52	2.450	1.050	2.00	1.697	1.931	2.240	1.368	1.094	1.636
54	2.550	1.050	2.00	1.703	1.937	2.247	1.372	1.097	1.638
56	2.650	1.050	2.00	1.709	1.913	2.253	1.376	1.100	1.641
58	2.750	1.050	2.00	1.714	1.918	2.258	1.379	1.103	1.643
60	2.850	1.050	2.00	1.718	1.923	2.263	1.381	1.105	1.645
62	2.950	1.050	2.00	1.722	1.927	2.267	1.384	1.107	1.647
64	1.050	1.150	2.00	1.170	1.200	1.249	1.152	1.115	1.052
66	1.150	1.150	2.00	1.335	1.393	1.490	1.295	1.222	1.101
68	1.250	1.150	2.00	1.493	1.576	1.715	1.422	1.317	1.142
70	1.350	1.150	2.00	1.639	1.744	1.919	1.530	1.397	1.177
72	1.450	1.150	2.00	1.770	1.894	1.099	1.618	1.463	1.204
74	1.550	1.150	2.00	1.837	1.925	1.254	1.690	1.516	1.225
76	1.650	1.150	2.00	1.935	1.137	1.337	1.743	1.558	1.242
78	1.750	1.150	2.00	1.975	1.233	1.498	1.794	1.592	1.255
80	1.850	1.150	2.00	1.149	1.315	1.591	1.332	1.620	1.267
82	1.950	1.150	2.00	1.211	1.393	1.664	1.352	1.643	1.276
84	1.050	1.150	2.00	1.264	1.440	1.734	1.387	1.661	1.285
86	1.150	1.150	2.00	1.339	1.498	1.788	1.408	1.677	1.292
88	1.250	1.150	2.00	1.417	1.529	1.833	1.426	1.691	1.299
90	1.350	1.150	2.00	1.379	1.554	1.872	1.441	1.702	1.305
92	1.450	1.150	2.00	1.406	1.593	1.904	1.453	1.712	1.310
94	1.550	1.150	2.00	1.433	1.618	1.931	1.464	1.721	1.315
96	1.650	1.150	2.00	1.450	1.639	1.955	1.474	1.728	1.320
98	1.750	1.150	2.00	1.459	1.658	1.975	1.482	1.735	1.324
100	1.850	1.150	2.00	1.463	1.674	1.992	1.489	1.741	1.327
102	1.950	1.150	2.00	1.466	1.686	2.008	1.496	1.746	1.331
104	2.050	1.150	2.00	1.508	1.700	2.021	1.001	1.751	1.334
106	2.150	1.150	2.00	1.510	1.711	2.032	1.006	1.755	1.337
108	2.250	1.150	2.00	1.527	1.720	2.042	1.011	1.759	1.340
110	2.350	1.150	2.00	1.535	1.729	2.051	1.015	1.763	1.342
112	2.450	1.150	2.00	1.542	1.736	2.059	1.019	1.766	1.344
114	2.550	1.150	2.00	1.549	1.743	2.066	1.022	1.769	1.346
116	2.650	1.150	2.00	1.554	1.749	2.072	1.025	1.771	1.348
118	2.750	1.150	2.00	1.560	1.754	2.078	1.028	1.774	1.350
120	2.850	1.150	2.00	1.564	1.759	2.083	1.030	1.776	1.352

2.750	1.250	.200	1.338	1.755	2.200	1.333	.770	.353
.950	1.250	.200	1.149	1.175	.219	1.104	.072	.019
.150	1.250	.200	.225	.140	.432	.271	.191	.938
.250	1.250	.200	.434	.598	.632	.293	.202	.050
.350	1.250	.200	.533	.557	.819	.370	.254	.061
.450	1.250	.200	.631	.772	.977	.435	.293	.070
.550	1.250	.200	.736	.911	1.120	.489	.334	.076
.650	1.250	.200	.978	1.015	1.243	.533	.364	.081
.750	1.250	.200	.959	1.105	1.348	.569	.388	.085
.850	1.250	.200	1.027	1.151	1.437	.599	.407	.089
.950	1.250	.200	1.037	1.246	1.512	.623	.424	.092
1.050	1.250	.200	1.137	1.301	1.575	.643	.438	.095
1.150	1.250	.200	1.150	1.335	1.629	.660	.450	.099
1.250	1.250	.200	1.217	1.335	1.674	.675	.460	.102
1.350	1.250	.200	1.249	1.422	1.712	.687	.469	.105
1.450	1.250	.200	1.276	1.451	1.744	.693	.476	.107
1.550	1.250	.200	1.287	1.476	1.772	.707	.483	.110
1.650	1.250	.200	1.319	1.478	1.796	.715	.489	.113
1.750	1.250	.200	1.337	1.517	1.817	.722	.495	.116
1.850	1.250	.200	1.352	1.533	1.834	.729	.499	.118
1.950	1.250	.200	1.355	1.547	1.850	.734	.504	.120
2.050	1.250	.200	1.377	1.559	1.863	.739	.508	.123
2.150	1.250	.200	1.387	1.570	1.875	.743	.511	.125
2.250	1.250	.200	1.377	1.550	1.886	.747	.515	.127
2.350	1.250	.200	1.405	1.544	1.895	.751	.518	.129
2.450	1.250	.200	1.412	1.594	1.783	.754	.520	.130
2.550	1.250	.200	1.418	1.533	1.910	.757	.523	.132
2.650	1.250	.200	1.424	1.509	1.917	.760	.525	.134
2.750	1.250	.200	1.429	1.619	1.923	.763	.527	.135
2.850	1.250	.200	1.434	1.619	1.928	.765	.529	.136
2.950	1.250	.200	1.435	1.625	1.933	.767	.531	.138
3.050	1.350	.200	.152	.159	.174	.071	.043	-.003
3.150	1.350	.200	.201	.337	.333	.139	.085	-.007
3.250	1.350	.200	.305	.451	.551	.201	.122	-.011
3.350	1.350	.200	.500	.555	.725	.256	.154	-.015
3.450	1.350	.200	.666	.775	.875	.303	.182	-.021
3.550	1.350	.200	.751	.815	1.005	.342	.204	-.026
3.650	1.350	.200	.795	.911	1.125	.375	.223	-.030
3.750	1.350	.200	.865	.975	1.219	.402	.239	-.034
3.850	1.350	.200	.925	1.067	1.309	.425	.252	-.037
3.950	1.350	.200	.951	1.127	1.373	.449	.263	-.039
4.050	1.350	.200	1.027	1.132	1.438	.460	.272	-.040
4.150	1.350	.200	1.071	1.225	1.490	.473	.280	-.041
4.250	1.350	.200	1.106	1.257	1.535	.485	.288	-.041
4.350	1.350	.200	1.137	1.301	1.575	.495	.294	-.041
4.450	1.350	.200	1.154	1.329	1.605	.503	.300	-.040
4.550	1.350	.200	1.167	1.359	1.633	.511	.305	-.039
4.650	1.350	.200	1.207	1.378	1.557	.518	.309	-.038
4.750	1.350	.200	1.224	1.395	1.675	.524	.313	-.037
4.850	1.350	.200	1.240	1.411	1.698	.527	.317	-.036
4.950	1.350	.200	1.253	1.425	1.712	.534	.321	-.035
5.050	1.350	.200	1.265	1.438	1.726	.538	.324	-.033
5.150	1.350	.200	1.275	1.449	1.736	.542	.327	-.032
5.250	1.350	.200	1.285	1.459	1.749	.546	.329	-.031
5.350	1.350	.200	1.293	1.467	1.758	.549	.332	-.030
5.450	1.350	.200	1.300	1.475	1.767	.552	.334	-.028
5.550	1.350	.200	1.317	1.482	1.774	.554	.336	-.027
5.650	1.450	.200	1.313	1.435	1.741	.557	.338	-.026
5.750	1.450	.200	1.315	1.473	1.747	.559	.340	-.025
5.850	1.450	.200	1.320	1.479	1.770	.561	.342	-.024

UCT

3	2.950	1.330	.200	1.327	1.539	1.220	.363	.343	-.023
5	.050	1.450	.200	.118	.138	.173	.340	.023	-.018
7	.150	1.450	.200	.233	.273	.341	.394	.046	-.035
9	.250	1.450	.200	.343	.403	.501	.436	.066	-.052
11	.350	1.450	.200	.447	.523	.650	.474	.083	-.068
13	.450	1.450	.200	.543	.634	.786	.506	.098	-.082
15	.550	1.450	.200	.630	.734	.907	.534	.111	-.095
17	.650	1.450	.200	.708	.822	1.013	.550	.121	-.107
19	.750	1.450	.200	.777	.900	1.107	.578	.130	-.117
21	.850	1.450	.200	.837	.969	1.188	.594	.137	-.125
23	.950	1.450	.200	.890	1.024	1.257	.609	.143	-.132
25	1.050	1.450	.200	.938	1.079	1.317	.621	.149	-.137
27	1.150	1.450	.200	.976	1.123	1.368	.631	.154	-.141
29	1.250	1.450	.200	1.011	1.161	1.412	.640	.158	-.144
31	1.350	1.450	.200	1.041	1.194	1.450	.648	.162	-.146
33	1.450	1.450	.200	1.067	1.223	1.483	.655	.166	-.148
35	1.550	1.450	.200	1.090	1.248	1.511	.661	.170	-.149
37	1.650	1.450	.200	1.110	1.269	1.535	.666	.173	-.149
39	1.750	1.450	.200	1.127	1.284	1.556	.671	.176	-.150
41	1.850	1.450	.200	1.142	1.305	1.575	.675	.179	-.150
43	1.950	1.450	.200	1.155	1.319	1.591	.679	.181	-.149
45	2.050	1.450	.200	1.168	1.332	1.605	.683	.183	-.149
47	2.150	1.450	.200	1.179	1.343	1.618	.686	.186	-.149
49	2.250	1.450	.200	1.188	1.353	1.629	.689	.189	-.148
51	2.350	1.450	.200	1.196	1.362	1.638	.692	.190	-.147
53	2.450	1.450	.200	1.203	1.370	1.647	.695	.192	-.147
55	2.550	1.450	.200	1.210	1.377	1.655	.697	.193	-.146
57	2.650	1.450	.200	1.216	1.383	1.662	.699	.195	-.145
59	2.750	1.450	.200	1.221	1.389	1.668	.701	.196	-.145
61	2.850	1.450	.200	1.226	1.394	1.674	.703	.198	-.144
63	2.950	1.450	.200	1.231	1.399	1.679	.704	.199	-.143
65	.050	1.550	.200	.105	.124	.155	.331	.009	-.027
67	.150	1.550	.200	.207	.245	.306	.361	.018	-.053
69	.250	1.550	.200	.308	.361	.450	.407	.026	-.078
71	.350	1.550	.200	.402	.471	.586	.414	.033	-.102
73	.450	1.550	.200	.499	.572	.709	.435	.039	-.123
75	.550	1.550	.200	.599	.663	.821	.454	.043	-.143
77	.650	1.550	.200	.690	.745	.921	.470	.047	-.160
79	.750	1.550	.200	.785	.819	1.009	.484	.050	-.174
81	.850	1.550	.200	.872	.885	1.086	.496	.052	-.187
83	.950	1.550	.200	.942	.940	1.153	.506	.055	-.197
85	1.050	1.550	.200	.996	.989	1.211	.514	.057	-.206
87	1.150	1.550	.200	.994	1.032	1.261	.522	.059	-.213
89	1.250	1.550	.200	.929	1.069	1.304	.528	.061	-.218
91	1.350	1.550	.200	.957	1.101	1.342	.534	.063	-.223
93	1.450	1.550	.200	.963	1.129	1.374	.540	.065	-.226
95	1.550	1.550	.200	1.005	1.154	1.402	.544	.067	-.229
97	1.650	1.550	.200	1.025	1.175	1.427	.548	.069	-.231
99	1.750	1.550	.200	1.042	1.194	1.448	.552	.070	-.233
101	1.850	1.550	.200	1.057	1.211	1.467	.556	.072	-.234
103	1.950	1.550	.200	1.071	1.225	1.484	.559	.074	-.235
105	2.050	1.550	.200	1.083	1.236	1.498	.562	.075	-.235
107	2.150	1.550	.200	1.093	1.250	1.510	.564	.077	-.236
109	2.250	1.550	.200	1.103	1.259	1.522	.567	.079	-.236
111	2.350	1.550	.200	1.111	1.269	1.532	.569	.080	-.236
113	2.450	1.550	.200	1.119	1.277	1.541	.571	.081	-.236
115	2.550	1.550	.200	1.126	1.284	1.549	.573	.083	-.235
117	2.650	1.550	.200	1.131	1.291	1.556	.575	.084	-.235
119	2.750	1.550	.200	1.137	1.297	1.562	.577	.085	-.235
121	2.850	1.550	.200	1.142	1.302	1.566	.578	.086	-.235

1125

1	2.750	1.550	.200	1.147	1.307	1.573	.280	.007	-.234
2	.750	1.550	.200	.345	.112	.137	.119	-.000	-.033
3	.150	1.550	.200	.138	.221	.275	.137	-.001	-.065
4	.250	1.550	.200	.279	.326	.407	.054	-.002	-.095
5	.350	1.550	.200	.363	.425	.533	.169	-.003	-.124
6	.450	1.550	.200	.442	.518	.643	.383	-.005	-.150
7	.550	1.550	.200	.516	.602	.747	.694	-.006	-.174
8	.650	1.550	.200	.592	.679	.840	.105	-.008	-.195
9	.750	1.550	.200	.642	.717	.923	.113	-.009	-.214
10	.850	1.550	.200	.696	.809	.996	.121	-.011	-.229
11	.950	1.550	.200	.713	.862	1.060	.127	-.012	-.243
12	1.050	1.550	.200	.735	.909	1.116	.133	-.012	-.254
13	1.150	1.550	.200	.722	.951	1.165	.138	-.013	-.264
14	1.250	1.550	.200	.655	.987	1.208	.142	-.013	-.272
15	1.350	1.550	.200	.603	1.019	1.245	.146	-.013	-.278
16	1.450	1.550	.200	.558	1.047	1.277	.150	-.013	-.283
17	1.550	1.550	.200	.530	1.071	1.305	.153	-.012	-.288
18	1.650	1.550	.200	.500	1.072	1.330	.156	-.011	-.291
19	1.750	1.550	.200	.467	1.111	1.351	.159	-.011	-.294
20	1.850	1.550	.200	.432	1.128	1.370	.162	-.010	-.296
21	1.950	1.550	.200	.396	1.142	1.387	.164	-.009	-.298
22	2.050	1.550	.200	.358	1.155	1.402	.166	-.008	-.299
23	2.150	1.550	.200	.318	1.167	1.415	.168	-.007	-.300
24	2.250	1.550	.200	.278	1.177	1.426	.170	-.006	-.301
25	2.350	1.550	.200	.234	1.185	1.437	.172	-.005	-.302
26	2.450	1.550	.200	.184	1.195	1.446	.174	-.005	-.302
27	2.550	1.550	.200	.131	1.202	1.454	.176	-.004	-.302
28	2.650	1.550	.200	.077	1.207	1.461	.177	-.003	-.303
29	2.750	1.550	.200	.022	1.215	1.466	.178	-.002	-.303
30	2.850	1.550	.200	.069	1.220	1.474	.180	-.001	-.303
31	2.950	1.550	.200	.012	1.225	1.479	.181	-.000	-.303
32	.050	1.750	.200	.336	.131	.126	.010	-.007	-.036
33	.150	1.750	.200	.175	.230	.250	.019	-.015	-.072
34	.250	1.750	.200	.252	.276	.349	.028	-.022	-.106
35	.350	1.750	.200	.327	.336	.481	.036	-.029	-.138
36	.450	1.750	.200	.402	.471	.536	.043	-.036	-.168
37	.550	1.750	.200	.470	.517	.682	.050	-.042	-.194
38	.650	1.750	.200	.532	.621	.769	.055	-.046	-.218
39	.750	1.750	.200	.588	.635	.847	.059	-.053	-.240
40	.850	1.750	.200	.638	.742	.917	.063	-.057	-.258
41	.950	1.750	.200	.683	.774	.978	.067	-.061	-.274
42	1.050	1.750	.200	.723	.839	1.032	.070	-.064	-.288
43	1.150	1.750	.200	.759	.879	1.080	.073	-.067	-.299
44	1.250	1.750	.200	.777	.914	1.121	.075	-.069	-.309
45	1.350	1.750	.200	.813	.915	1.158	.078	-.070	-.317
46	1.450	1.750	.200	.842	.973	1.170	.080	-.072	-.324
47	1.550	1.750	.200	.864	.997	1.218	.082	-.072	-.330
48	1.650	1.750	.200	.883	1.013	1.243	.084	-.073	-.334
49	1.750	1.750	.200	.900	1.037	1.264	.086	-.073	-.338
50	1.850	1.750	.200	.915	1.053	1.285	.087	-.073	-.342
51	1.950	1.750	.200	.927	1.054	1.300	.089	-.073	-.344
52	2.050	1.750	.200	.941	1.081	1.315	.091	-.073	-.346
53	2.150	1.750	.200	.951	1.093	1.326	.092	-.073	-.348
54	2.250	1.750	.200	.961	1.103	1.340	.093	-.073	-.350
55	2.350	1.750	.200	.970	1.113	1.351	.095	-.072	-.351
56	2.450	1.750	.200	.977	1.121	1.360	.096	-.072	-.352
57	2.550	1.750	.200	.984	1.128	1.369	.098	-.071	-.353
58	2.650	1.750	.200	.990	1.135	1.376	.099	-.071	-.353
59	2.750	1.750	.200	.995	1.141	1.383	.100	-.070	-.354
60	2.850	1.750	.200	1.001	1.147	1.389	.101	-.069	-.354

LIST

2.750	1.750	.200	.394	1.027	1.249	-.312	-.155	-.421
.750	2.050	.200	.365	.977	.996	-.305	-.010	-.639
.150	2.350	.200	.129	.152	.190	-.110	-.035	-.675
.250	2.050	.200	.192	.228	.232	-.315	-.053	-.115
.350	2.050	.200	.252	.278	.309	-.320	-.069	-.151
.450	2.050	.200	.309	.363	.452	-.324	-.084	-.185
.550	2.050	.200	.361	.428	.510	-.329	-.099	-.216
.650	2.050	.200	.413	.484	.601	-.333	-.112	-.244
.750	2.050	.200	.459	.537	.667	-.336	-.124	-.270
.850	2.050	.200	.502	.596	.726	-.340	-.135	-.293
.950	2.050	.200	.550	.630	.730	-.343	-.144	-.313
1.050	2.050	.200	.575	.670	.820	-.345	-.153	-.331
1.150	2.050	.200	.607	.719	.972	-.348	-.160	-.347
1.250	2.050	.200	.635	.738	.910	-.350	-.165	-.361
1.350	2.050	.200	.660	.757	.945	-.351	-.172	-.373
1.450	2.050	.200	.683	.773	.978	-.352	-.177	-.383
1.550	2.050	.200	.704	.816	1.003	-.353	-.181	-.392
1.650	2.050	.200	.722	.816	1.027	-.354	-.184	-.400
1.750	2.050	.200	.731	.825	1.049	-.355	-.187	-.407
1.850	2.050	.200	.753	.871	1.068	-.355	-.189	-.413
1.950	2.050	.200	.764	.880	1.086	-.355	-.191	-.418
2.050	2.050	.200	.773	.899	1.101	-.356	-.193	-.422
2.150	2.050	.200	.779	.911	1.115	-.356	-.194	-.426
2.250	2.050	.200	.799	.922	1.127	-.355	-.195	-.429
2.350	2.050	.200	.807	.931	1.139	-.355	-.197	-.432
2.450	2.050	.200	.815	.940	1.148	-.355	-.197	-.434
2.550	2.050	.200	.822	.948	1.157	-.355	-.198	-.436
2.650	2.050	.200	.829	.955	1.166	-.355	-.199	-.438
2.750	2.050	.200	.835	.952	1.173	-.354	-.199	-.440
2.850	2.050	.200	.840	.958	1.180	-.354	-.199	-.441
2.950	2.050	.200	.845	.973	1.186	-.354	-.199	-.442
.050	2.150	.200	.000	.070	.088	-.008	-.019	-.039
.150	2.150	.200	.119	.130	.175	-.015	-.039	-.077
.250	2.150	.200	.177	.208	.259	-.023	-.057	-.115
.350	2.150	.200	.232	.273	.341	-.030	-.075	-.150
.450	2.150	.200	.285	.335	.418	-.037	-.092	-.184
.550	2.150	.200	.335	.393	.490	-.043	-.108	-.215
.650	2.150	.200	.382	.448	.557	-.049	-.122	-.244
.750	2.150	.200	.425	.498	.619	-.054	-.135	-.270
.850	2.150	.200	.468	.544	.675	-.059	-.147	-.294
.950	2.150	.200	.522	.586	.727	-.064	-.158	-.315
1.050	2.150	.200	.536	.625	.773	-.068	-.168	-.334
1.150	2.150	.200	.556	.659	.815	-.071	-.176	-.351
1.250	2.150	.200	.573	.691	.853	-.074	-.184	-.365
1.350	2.150	.200	.583	.719	.887	-.077	-.190	-.376
1.450	2.150	.200	.590	.744	.917	-.079	-.196	-.390
1.550	2.150	.200	.600	.766	.944	-.081	-.200	-.400
1.650	2.150	.200	.603	.787	.968	-.082	-.205	-.408
1.750	2.150	.200	.605	.805	.989	-.084	-.208	-.416
1.850	2.150	.200	.609	.821	1.009	-.085	-.211	-.422
1.950	2.150	.200	.622	.836	1.026	-.086	-.214	-.428
2.050	2.150	.200	.634	.849	1.042	-.086	-.216	-.433
2.150	2.150	.200	.645	.861	1.055	-.087	-.218	-.437
2.250	2.150	.200	.654	.872	1.064	-.087	-.220	-.441
2.350	2.150	.200	.662	.882	1.079	-.087	-.221	-.444
2.450	2.150	.200	.671	.890	1.089	-.087	-.222	-.447
2.550	2.150	.200	.673	.894	1.099	-.088	-.223	-.450
2.650	2.150	.200	.674	.896	1.107	-.088	-.224	-.452
2.750	2.150	.200	.674	.897	1.115	-.087	-.225	-.454
2.850	2.150	.200	.676	.897	1.121	-.087	-.225	-.454

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1.75	2.00	2.25	2.50	2.75	3.00	3.25	3.50	3.75	4.00	4.25	4.50	4.75	5.00	5.25	5.50	5.75	6.00	6.25	6.50	6.75	7.00	7.25	7.50	7.75	8.00	8.25	8.50	8.75	9.00	9.25	9.50	9.75	10.00	10.25	10.50	10.75	11.00	11.25	11.50	11.75	12.00	12.25	12.50	12.75	13.00	13.25	13.50	13.75	14.00	14.25	14.50	14.75	15.00	15.25	15.50	15.75	16.00	16.25	16.50	16.75	17.00	17.25	17.50	17.75	18.00	18.25	18.50	18.75	19.00	19.25	19.50	19.75	20.00	20.25	20.50	20.75	21.00	21.25	21.50	21.75	22.00	22.25	22.50	22.75	23.00	23.25	23.50	23.75	24.00	24.25	24.50	24.75	25.00	25.25	25.50	25.75	26.00	26.25	26.50	26.75	27.00	27.25	27.50	27.75	28.00	28.25	28.50	28.75	29.00	29.25	29.50	29.75	30.00	30.25	30.50	30.75	31.00	31.25	31.50	31.75	32.00	32.25	32.50	32.75	33.00	33.25	33.50	33.75	34.00	34.25	34.50	34.75	35.00	35.25	35.50	35.75	36.00	36.25	36.50	36.75	37.00	37.25	37.50	37.75	38.00	38.25	38.50	38.75	39.00	39.25	39.50	39.75	40.00	40.25	40.50	40.75	41.00	41.25	41.50	41.75	42.00	42.25	42.50	42.75	43.00	43.25	43.50	43.75	44.00	44.25	44.50	44.75	45.00	45.25	45.50	45.75	46.00	46.25	46.50	46.75	47.00	47.25	47.50	47.75	48.00	48.25	48.50	48.75	49.00	49.25	49.50	49.75	50.00	50.25	50.50	50.75	51.00	51.25	51.50	51.75	52.00	52.25	52.50	52.75	53.00	53.25	53.50	53.75	54.00	54.25	54.50	54.75	55.00	55.25	55.50	55.75	56.00	56.25	56.50	56.75	57.00	57.25	57.50	57.75	58.00	58.25	58.50	58.75	59.00	59.25	59.50	59.75	60.00	60.25	60.50	60.75	61.00	61.25	61.50	61.75	62.00	62.25	62.50	62.75	63.00	63.25	63.50	63.75	64.00	64.25	64.50	64.75	65.00	65.25	65.50	65.75	66.00	66.25	66.50	66.75	67.00	67.25	67.50	67.75	68.00	68.25	68.50	68.75	69.00	69.25	69.50	69.75	70.00	70.25	70.50	70.75	71.00	71.25	71.50	71.75	72.00	72.25	72.50	72.75	73.00	73.25	73.50	73.75	74.00	74.25	74.50	74.75	75.00	75.25	75.50	75.75	76.00	76.25	76.50	76.75	77.00	77.25	77.50	77.75	78.00	78.25	78.50	78.75	79.00	79.25	79.50	79.75	80.00	80.25	80.50	80.75	81.00	81.25	81.50	81.75	82.00	82.25	82.50	82.75	83.00	83.25	83.50	83.75	84.00	84.25	84.50	84.75	85.00	85.25	85.50	85.75	86.00	86.25	86.50	86.75	87.00	87.25	87.50	87.75	88.00	88.25	88.50	88.75	89.00	89.25	89.50	89.75	90.00	90.25	90.50	90.75	91.00	91.25	91.50	91.75	92.00	92.25	92.50	92.75	93.00	93.25	93.50	93.75	94.00	94.25	94.50	94.75	95.00	95.25	95.50	95.75	96.00	96.25	96.50	96.75	97.00	97.25	97.50	97.75	98.00	98.25	98.50	98.75	99.00	99.25	99.50	99.75	100.00	100.25	100.50	100.75	101.00	101.25	101.50	101.75	102.00	102.25	102.50	102.75	103.00	103.25	103.50	103.75	104.00	104.25	104.50	104.75	105.00	105.25	105.50	105.75	106.00	106.25	106.50	106.75	107.00	107.25	107.50	107.75	108.00	108.25	108.50	108.75	109.00	109.25	109.50	109.75	110.00	110.25	110.50	110.75	111.00	111.25	111.50	111.75	112.00	112.25	112.50	112.75	113.00	113.25	113.50	113.75	114.00	114.25	114.50	114.75	115.00	115.25	115.50	115.75	116.00	116.25	116.50	116.75	117.00	117.25	117.50	117.75	118.00	118.25	118.50	118.75	119.00	119.25	119.50	119.75	120.00	120.25	120.50	120.75	121.00	121.25	121.50	121.75	122.00	122.25	122.50	122.75	123.00	123.25	123.50	123.75	124.00	124.25	124.50	124.75	125.00	125.25	125.50	125.75	126.00	126.25	126.50	126.75	127.00	127.25	127.50	127.75	128.00	128.25	128.50	128.75	129.00	129.25	129.50	129.75	130.00	130.25	130.50	130.75	131.00	131.25	131.50	131.75	132.00	132.25	132.50	132.75	133.00	133.25	133.50	133.75	134.00	134.25	134.50	134.75	135.00	135.25	135.50	135.75	136.00	136.25	136.50	136.75	137.00	137.25	137.50	137.75	138.00	138.25	138.50	138.75	139.00	139.25	139.50	139.75	140.00	140.25	140.50	140.75	141.00	141.25	141.50	141.75	142.00	142.25	142.50	142.75	143.00	143.25	143.50	143.75	144.00	144.25	144.50	144.75	145.00	145.25	145.50	145.75	146.00	146.25	146.50	146.75	147.00	147.25	147.50	147.75	148.00	148.25	148.50	148.75	149.00	149.25	149.50	149.75	150.00	150.25	150.50	150.75	151.00	151.25	151.50	151.75	152.00	152.25	152.50	152.75	153.00	153.25	153.50	153.75	154.00	154.25	154.50	154.75	155.00	155.25	155.50	155.75	156.00	156.25	156.50	156.75	157.00	157.25	157.50	157.75	158.00	158.25	158.50	158.75	159.00	159.25	159.50	159.75	160.00	160.25	160.50	160.75	161.00	161.25	161.50	161.75	162.00	162.25	162.50	162.75	163.00	163.25	163.50	163.75	164.00	164.25	164.50	164.75	165.00	165.25	165.50	165.75	166.00	166.25	166.50	166.75	167.00	167.25	167.50	167.75	168.00	168.25	168.50	168.75	169.00	169.25	169.50	169.75	170.00	170.25	170.50	170.75	171.00	171.25	171.50	171.75	172.00	172.25	172.50	172.75	173.00	173.25	173.50	173.75	174.00	174.25	174.50	174.75	175.00	175.25	175.50	175.75	176.00	176.25	176.50	176.75	177.00	177.25	177.50	177.75	178.00	178.25	178.50	178.75	179.00	179.25	179.50	179.75	180.00	180.25	180.50	180.75	181.00	181.25	181.50	181.75	182.00	182.25	182.50	182.75	183.00	183.25	183.50	183.75	184.00	184.25	184.50	184.75	185.00	185.25	185.50	185.75	186.00	186.25	186.50	186.75	187.00	187.25	187.50	187.75	188.00	188.25	188.50	188.75	189.00	189.25	189.50	189.75	190.00	190.25	190.50	190.75	191.00	191.25	191.50	191.75	192.00	192.25	192.50	192.75	193.00	193.25	193.50	193.75	194.00	194.25	194.50	194.75	195.00	195.25	195.50	195.75	196.00	196.25	196.50	196.75	197.00	197.25	197.50	197.75	198.00	198.25	198.50	198.75	199.00	199.25	199.50	199.75	200.00	200.25	200.50	200.75	201.00	201.25	201.50	201.75	202.00	202.25	202.50	202.75	203.00	203.25	203.50	203.75	204.00	204.25	204.50	204.75	205.00	205.25	205.50	205.75	206.00	206.25	206.50	206.75	207.00	207.25	207.50	207.75	208.00	208.25	208.50	208.75	209.00	209.25	209.50	209.75	210.00	210.25	210.50	210.75	211.00	211.25	211.50	211.75	212.00	212.25	212.50	212.75	213.00	213.25	213.50	213.75	214.00	214.25	214.50	214.75	215.00	215.25	215.50	215.75	216.00	216.25	216.50	216.75	217.00	217.25	217.50	217.75	218.00	218.25	218.50	218.75	219.00	219.25	219.50	219.75	220.00	220.25	220.50	220.75	221.00	221.25	221.50	221.75	222.00	222.25	222.50	222.75	223.00	223.25	223.50	223.75	224.00	224.25	224.50	224.75	225.00	225.25	225.50	225.75	226.00	226.25	226.50	226.75	227.00	227.25	227.50	227.75	228.00	228.25	228.50	228.75	229.00	229.25	229.50	229.75	230.00	230.25	230.50	230.75	231.00	231.25	231.50	231.75	232.00	232.25	232.50	232.75	233.00	233.25	233.50	233.75	234.00	234.25	234.50	234.75	235.00	235.25	235.50	235.75	236.00	236.25	236.50	236.75	237.00	237.25	237.50	237.75	238.00	238.25	238.50	238.75	239.00	239.25	239.50	239.75	240.00	240.25	240.50	240.75	241.00	241.25	241.50	241.75	242.00	242.25	242.50	242.75	243.00	243.25	243.50	243.75	244.00	244.25	244.50	244.75	245.00	245.25	245.50	245.75	246.00	246.25	246.50	246.75	247.00	247.25	247.50	247.75	248.00	248.25	248.50	248.75	249.00	249.25	249.50	249.75	250.00	250.25	250.50	250.75	251.00	251.25	251.50	251.75	252.00	252.25	252.50	252.75	253.00	253.25	253.50	253.75	254.00	254.25	254.50	254.75	255.00	255.25	255.50	255.75	256.00	256.25	256.50	256.75	257.00	257.25	257.50	257.75	258.00	258.25	258.50	258.75	259.00	259.25	259.50	259.75	260.00	260.25	260.50	260.75	261.00	261.25	261.50	261.75	262.00	262.25	262.50	262.75	263.00	263.25	263.50	263.75	264.00	264.25	264.50	264.75	265.00	265.25	265.50	265.75	266.00	266.25	266.50	266.75	267.00	267.25	267.50	267.75	268.00	268.25	268.50	268.75	269.00	269.25	269.50	269.75	270.00	270.25	270.50	270.75	271.00	271.25	271.50	271.75	272.00	272.25	272.50	272.75	273.00	273.25	273.50	273.75	274.00	274.25	274.50	274.75	275.00	275.25	275.50	275.75	276.00	276.25	276.50	276.75	277.00	277.25	277.50	277.75	278.00	278.25	278.50	278.75	279.00	279.25	279.50	279.75	280.00	280.25	280.50	280.75	281.00	281.25	281.50	281.75	282.00	282.25	282.50	282.75	283.00	283.25	283.50	283.75	284.00	284.25	284.50	284.75	285.00	285.25	285.50	285.75	286.00	286.25	286.50	286.75	287.00	287.25	287.50	287.75	288.00	288.25	288.50	288.75	289.00	289.25	289.50	289.75
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1	2.150	2.450	.200	.724	.537	1.325	-.136	-.263	-.473
2	2.250	2.450	.200	.747	.556	1.370	-.112	-.021	-.336
3	2.350	2.450	.200	.769	.574	1.414	-.024	-.042	-.072
4	2.450	2.450	.200	.790	.595	1.456	-.035	-.062	-.157
5	2.550	2.450	.200	.815	.617	1.497	-.046	-.082	-.141
6	2.650	2.450	.200	.839	.639	1.537	-.057	-.101	-.173
7	2.750	2.450	.200	.864	.661	1.577	-.067	-.118	-.204
8	2.850	2.450	.200	.887	.681	1.617	-.077	-.135	-.232
9	2.950	2.450	.200	.910	.703	1.657	-.085	-.150	-.259
10	3.050	2.450	.200	.933	.724	1.697	-.093	-.165	-.283
11	3.150	2.450	.200	.956	.745	1.737	-.101	-.178	-.305
12	3.250	2.450	.200	.978	.766	1.777	-.109	-.189	-.326
13	3.350	2.450	.200	.999	.787	1.817	-.114	-.200	-.344
14	3.450	2.450	.200	1.020	.808	1.857	-.117	-.210	-.360
15	3.550	2.450	.200	1.041	.829	1.897	-.124	-.218	-.375
16	3.650	2.450	.200	1.061	.850	1.937	-.128	-.226	-.388
17	3.750	2.450	.200	1.081	.871	1.977	-.132	-.233	-.400
18	3.850	2.450	.200	1.101	.892	2.017	-.136	-.239	-.410
19	3.950	2.450	.200	1.121	.913	2.057	-.139	-.244	-.420
20	4.050	2.450	.200	1.141	.934	2.097	-.141	-.249	-.428
21	4.150	2.450	.200	1.161	.955	2.137	-.143	-.255	-.435
22	4.250	2.450	.200	1.181	.976	2.177	-.145	-.256	-.442
23	4.350	2.450	.200	1.201	.997	2.217	-.147	-.260	-.447
24	4.450	2.450	.200	1.221	1.018	2.257	-.148	-.263	-.453
25	4.550	2.450	.200	1.241	1.039	2.297	-.150	-.265	-.457
26	4.650	2.450	.200	1.261	1.060	2.337	-.151	-.267	-.461
27	4.750	2.450	.200	1.281	1.081	2.377	-.152	-.269	-.465
28	4.850	2.450	.200	1.301	1.102	2.417	-.153	-.271	-.468
29	4.950	2.450	.200	1.321	1.123	2.457	-.153	-.272	-.471
30	5.050	2.450	.200	1.341	1.144	2.497	-.154	-.274	-.473
31	5.150	2.450	.200	1.361	1.165	2.537	-.154	-.275	-.476
32	5.250	2.450	.200	1.381	1.186	2.577	-.154	-.275	-.476
33	5.350	2.450	.200	1.401	1.207	2.617	-.154	-.275	-.476
34	5.450	2.450	.200	1.421	1.228	2.657	-.154	-.275	-.476
35	5.550	2.450	.200	1.441	1.249	2.697	-.154	-.275	-.476
36	5.650	2.450	.200	1.461	1.270	2.737	-.154	-.275	-.476
37	5.750	2.450	.200	1.481	1.291	2.777	-.154	-.275	-.476
38	5.850	2.450	.200	1.501	1.312	2.817	-.154	-.275	-.476
39	5.950	2.450	.200	1.521	1.333	2.857	-.154	-.275	-.476
40	6.050	2.450	.200	1.541	1.354	2.897	-.154	-.275	-.476
41	6.150	2.450	.200	1.561	1.375	2.937	-.154	-.275	-.476
42	6.250	2.450	.200	1.581	1.396	2.977	-.154	-.275	-.476
43	6.350	2.450	.200	1.601	1.417	3.017	-.154	-.275	-.476
44	6.450	2.450	.200	1.621	1.438	3.057	-.154	-.275	-.476
45	6.550	2.450	.200	1.641	1.459	3.097	-.154	-.275	-.476
46	6.650	2.450	.200	1.661	1.480	3.137	-.154	-.275	-.476
47	6.750	2.450	.200	1.681	1.501	3.177	-.154	-.275	-.476
48	6.850	2.450	.200	1.701	1.522	3.217	-.154	-.275	-.476
49	6.950	2.450	.200	1.721	1.543	3.257	-.154	-.275	-.476
50	7.050	2.450	.200	1.741	1.564	3.297	-.154	-.275	-.476
51	7.150	2.450	.200	1.761	1.585	3.337	-.154	-.275	-.476
52	7.250	2.450	.200	1.781	1.606	3.377	-.154	-.275	-.476
53	7.350	2.450	.200	1.801	1.627	3.417	-.154	-.275	-.476
54	7.450	2.450	.200	1.821	1.648	3.457	-.154	-.275	-.476
55	7.550	2.450	.200	1.841	1.669	3.497	-.154	-.275	-.476
56	7.650	2.450	.200	1.861	1.690	3.537	-.154	-.275	-.476
57	7.750	2.450	.200	1.881	1.711	3.577	-.154	-.275	-.476
58	7.850	2.450	.200	1.901	1.732	3.617	-.154	-.275	-.476
59	7.950	2.450	.200	1.921	1.753	3.657	-.154	-.275	-.476
60	8.050	2.450	.200	1.941	1.774	3.697	-.154	-.275	-.476
61	8.150	2.450	.200	1.961	1.795	3.737	-.154	-.275	-.476
62	8.250	2.450	.200	1.981	1.816	3.777	-.154	-.275	-.476
63	8.350	2.450	.200	2.001	1.837	3.817	-.154	-.275	-.476
64	8.450	2.450	.200	2.021	1.858	3.857	-.154	-.275	-.476
65	8.550	2.450	.200	2.041	1.879	3.897	-.154	-.275	-.476
66	8.650	2.450	.200	2.061	1.900	3.937	-.154	-.275	-.476
67	8.750	2.450	.200	2.081	1.921	3.977	-.154	-.275	-.476
68	8.850	2.450	.200	2.101	1.942	4.017	-.154	-.275	-.476
69	8.950	2.450	.200	2.121	1.963	4.057	-.154	-.275	-.476
70	9.050	2.450	.200	2.141	1.984	4.097	-.154	-.275	-.476
71	9.150	2.450	.200	2.161	2.005	4.137	-.154	-.275	-.476
72	9.250	2.450	.200	2.181	2.026	4.177	-.154	-.275	-.476
73	9.350	2.450	.200	2.201	2.047	4.217	-.154	-.275	-.476
74	9.450	2.450	.200	2.221	2.068	4.257	-.154	-.275	-.476
75	9.550	2.450	.200	2.241	2.089	4.297	-.154	-.275	-.476
76	9.650	2.450	.200	2.261	2.110	4.337	-.154	-.275	-.476
77	9.750	2.450	.200	2.281	2.131	4.377	-.154	-.275	-.476
78	9.850	2.450	.200	2.301	2.152	4.417	-.154	-.275	-.476
79	9.950	2.450	.200	2.321	2.173	4.457	-.154	-.275	-.476
80	10.050	2.450	.200	2.341	2.194	4.497	-.154	-.275	-.476
81	10.150	2.450	.200	2.361	2.215	4.537	-.154	-.275	-.476
82	10.250	2.450	.200	2.381	2.236	4.577	-.154	-.275	-.476
83	10.350	2.450	.200	2.401	2.257	4.617	-.154	-.275	-.476
84	10.450	2.450	.200	2.421	2.278	4.657	-.154	-.275	-.476
85	10.550	2.450	.200	2.441	2.299	4.697	-.154	-.275	-.476
86	10.650	2.450	.200	2.461	2.320	4.737	-.154	-.275	-.476
87	10.750	2.450	.200	2.481	2.341	4.777	-.154	-.275	-.476
88	10.850	2.450	.200	2.501	2.362	4.817	-.154	-.275	-.476
89	10.950	2.450	.200	2.521	2.383	4.857	-.154	-.275	-.476
90	11.050	2.450	.200	2.541	2.404	4.897	-.154	-.275	-.476
91	11.150	2.450	.200	2.561	2.425	4.937	-.154	-.275	-.476
92	11.250	2.450	.200	2.581	2.446	4.977	-.154	-.275	-.476
93	11.350	2.450	.200	2.601	2.467	5.017	-.154	-.275	-.476
94	11.450	2.450	.200	2.621	2.488	5.057	-.154	-.275	-.476
95	11.550	2.450	.200	2.641	2.509	5.097	-.154	-.275	-.476
96	11.650	2.450	.200	2.661	2.530	5.137	-.154	-.275	-.476
97	11.750	2.450	.200	2.681	2.551	5.177	-.154	-.275	-.476
98	11.850	2.450	.200	2.701	2.572	5.217	-.154	-.275	-.476
99	11.950	2.450	.200	2.721	2.593	5.257	-.154	-.275	-.476
100	12.050	2.450	.200	2.741	2.614	5.297	-.154	-.275	-.476

UCT

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[illegible]

1.750	.150	.300	6.555	5.131	5.291	12.178	12.524	11.434
.350	.250	.300	5.245	4.281	4.406	9.744	9.532	9.174
.150	.250	.300	5.372	5.349	5.287	9.315	7.756	7.356
.250	.250	.300	1.324	1.355	1.372	10.596	10.149	9.405
.350	.250	.300	2.341	2.412	2.292	11.748	11.492	10.664
.450	.250	.300	3.508	3.312	2.959	12.851	12.326	11.450
.550	.250	.300	4.300	3.785	3.426	13.409	12.864	11.954
.650	.250	.300	4.346	4.124	3.754	13.781	13.226	12.302
.750	.250	.300	4.574	4.368	3.990	14.042	13.479	12.541
.850	.250	.300	4.777	4.547	4.164	14.229	13.661	12.714
.950	.250	.300	4.914	4.601	4.294	14.368	13.796	12.843
1.050	.250	.300	5.019	4.715	4.394	14.474	13.879	12.940
1.150	.250	.300	5.101	4.835	4.472	14.557	13.979	13.017
1.250	.250	.300	5.165	4.927	4.534	14.622	14.042	13.077
1.350	.250	.300	5.219	4.931	4.584	14.674	14.093	13.125
1.450	.250	.300	5.262	5.023	4.625	14.716	14.135	13.165
1.550	.250	.300	5.294	5.038	4.657	14.752	14.169	13.196
1.650	.250	.300	5.317	5.047	4.687	14.781	14.197	13.225
1.750	.250	.300	5.333	5.112	4.711	14.806	14.222	13.248
1.850	.250	.300	5.374	5.134	4.731	14.827	14.242	13.268
1.950	.250	.300	5.372	5.151	4.748	14.845	14.260	13.284
2.050	.250	.300	5.403	5.196	4.763	14.861	14.275	13.299
2.150	.250	.300	5.422	5.180	4.776	14.879	14.288	13.312
2.250	.250	.300	5.434	5.192	4.788	14.886	14.300	13.323
2.350	.250	.300	5.445	5.202	4.798	14.897	14.310	13.332
2.450	.250	.300	5.454	5.211	4.807	14.906	14.319	13.341
2.550	.250	.300	5.463	5.220	4.815	14.914	14.327	13.349
2.650	.250	.300	5.470	5.227	4.822	14.921	14.334	13.356
2.750	.250	.300	5.477	5.233	4.828	14.928	14.341	13.362
2.850	.250	.300	5.483	5.239	4.834	14.934	14.346	13.367
2.950	.250	.300	5.483	5.235	4.834	14.939	14.352	13.372
.350	.350	.300	.033	.017	-.034	9.166	9.001	8.726
.150	.350	.300	.563	.539	.497	7.332	7.042	6.558
.250	.350	.300	1.353	1.316	1.259	9.388	9.017	8.347
.350	.350	.300	2.354	2.290	1.267	10.664	10.243	9.541
.450	.350	.300	2.555	2.505	2.520	11.467	11.015	10.262
.550	.350	.300	3.577	3.522	2.930	11.990	11.517	10.734
.650	.350	.300	3.387	3.326	3.229	12.394	11.860	11.054
.750	.350	.300	3.615	3.553	3.750	12.593	12.100	11.279
.850	.350	.300	3.785	3.722	3.615	12.773	12.274	11.442
.950	.350	.300	3.917	3.851	3.740	12.907	12.403	11.564
1.050	.350	.300	4.018	3.950	3.833	13.009	12.502	11.658
1.150	.350	.300	4.347	4.029	3.914	13.089	12.579	11.730
1.250	.350	.300	4.181	4.072	3.975	13.152	12.641	11.788
1.350	.350	.300	4.213	4.142	4.025	13.203	12.690	11.835
1.450	.350	.300	4.255	4.134	4.056	13.244	12.736	11.873
1.550	.350	.300	4.280	4.219	4.099	13.279	12.763	11.905
1.650	.350	.300	4.320	4.243	4.124	13.303	12.791	11.931
1.750	.350	.300	4.345	4.272	4.151	13.332	12.815	11.953
1.850	.350	.300	4.366	4.293	4.172	13.352	12.835	11.973
1.950	.350	.300	4.384	4.311	4.189	13.370	12.852	11.989
2.050	.350	.300	4.400	4.327	4.204	13.386	12.867	12.003
2.150	.350	.300	4.414	4.340	4.217	13.397	12.880	12.015
2.250	.350	.300	4.423	4.352	4.229	13.411	12.892	12.026
2.350	.350	.300	4.437	4.353	4.239	13.421	12.902	12.036
2.450	.350	.300	4.446	4.372	4.248	13.430	12.910	12.044
2.550	.350	.300	4.454	4.380	4.256	13.436	12.910	12.052
2.650	.350	.300	4.462	4.387	4.263	13.445	12.925	12.058
2.750	.350	.300	4.469	4.374	4.270	13.452	12.932	12.064
2.850	.350	.300	4.477	4.400	4.275	13.458	12.937	12.070

U.C.T.

3	2.950	.350	.300	9.910	1.145	9.280	13.193	2.942	12.075
5	.750	.450	.300	.145	.103	.172	3.195	2.936	2.753
7	.150	.450	.300	.522	.532	.601	6.664	5.331	4.999
9	.250	.450	.300	1.309	1.098	1.157	7.266	6.960	6.450
11	.350	.450	.300	1.575	1.639	1.677	8.373	8.616	7.429
13	.450	.450	.300	2.316	2.006	2.152	9.072	8.706	9.063
15	.550	.450	.300	2.430	2.439	2.505	9.570	9.164	8.487
17	.650	.450	.300	2.671	2.704	2.773	9.899	9.479	8.778
19	.750	.450	.300	2.877	2.914	2.976	10.132	9.702	8.989
21	.850	.450	.300	3.035	3.071	3.132	10.302	9.865	9.137
23	.950	.450	.300	2.157	3.193	3.252	10.429	9.987	9.251
25	1.050	.450	.300	3.253	3.298	3.346	10.527	10.081	9.338
27	1.150	.450	.300	3.357	3.364	3.421	10.603	10.155	9.407
29	1.250	.450	.300	3.392	3.425	3.481	10.664	10.213	9.462
31	1.350	.450	.300	3.442	3.475	3.530	10.713	10.261	9.506
33	1.450	.450	.300	3.464	3.516	3.570	10.754	10.299	9.542
35	1.550	.450	.300	3.518	3.550	3.604	10.787	10.332	9.573
37	1.650	.450	.300	3.547	3.574	3.632	10.815	10.354	9.598
39	1.750	.450	.300	3.572	3.604	3.655	10.839	10.381	9.620
41	1.850	.450	.300	3.573	3.624	3.676	10.859	10.401	9.638
43	1.950	.450	.300	3.511	3.612	3.674	10.876	10.415	9.654
45	2.050	.450	.300	3.627	3.658	3.739	10.891	10.432	9.667
47	2.150	.450	.300	3.641	3.671	3.722	10.904	10.445	9.679
49	2.250	.450	.300	3.653	3.633	3.734	10.915	10.456	9.690
51	2.350	.450	.300	3.664	3.674	3.744	10.926	10.466	9.699
53	2.450	.450	.300	3.673	3.733	3.753	10.934	10.474	9.707
55	2.550	.450	.300	3.681	3.711	3.761	10.942	10.482	9.715
57	2.650	.450	.300	3.689	3.719	3.766	10.950	10.487	9.721
59	2.750	.450	.300	3.696	3.725	3.775	10.956	10.495	9.727
61	2.850	.450	.300	3.702	3.711	3.781	10.962	10.501	9.732
63	2.950	.450	.300	3.707	3.737	3.786	10.967	10.506	9.737
65	.050	.550	.300	.189	.218	.267	2.102	2.081	1.912
67	.150	.550	.300	.465	.538	.627	4.004	3.417	3.505
69	.250	.550	.300	.871	.941	1.057	5.341	5.089	4.668
71	.350	.550	.300	1.269	1.350	1.403	6.261	5.963	5.466
73	.450	.550	.300	1.625	1.711	1.855	6.504	6.554	6.005
75	.550	.550	.300	1.917	2.037	2.157	7.310	6.959	6.375
77	.650	.550	.300	2.151	2.242	2.375	7.609	7.243	6.634
79	.750	.550	.300	2.334	2.427	2.531	7.824	7.447	6.820
81	.850	.550	.300	2.474	2.572	2.726	7.962	7.598	6.958
83	.950	.550	.300	2.593	2.636	2.841	8.102	7.712	7.063
85	1.050	.550	.300	2.384	2.777	2.931	8.194	7.800	7.144
87	1.150	.550	.300	2.757	2.859	3.004	8.265	7.869	7.206
89	1.250	.550	.300	2.318	2.909	3.063	8.324	7.925	7.259
91	1.350	.550	.300	2.365	2.958	3.112	8.371	7.970	7.301
93	1.450	.550	.300	2.755	2.978	3.152	8.410	8.007	7.335
95	1.550	.550	.300	2.940	3.032	3.195	8.442	8.037	7.363
97	1.650	.550	.300	2.969	3.050	3.213	8.469	8.063	7.387
99	1.750	.550	.300	2.993	3.035	3.237	8.492	8.085	7.408
101	1.850	.550	.300	3.014	3.105	3.258	8.511	8.104	7.425
103	1.950	.550	.300	3.032	3.123	3.275	8.523	8.120	7.440
105	2.050	.550	.300	3.044	3.139	3.290	8.542	8.134	7.453
107	2.150	.550	.300	3.061	3.152	3.304	8.555	8.146	7.465
109	2.250	.550	.300	3.073	3.154	3.316	8.566	8.157	7.475
111	2.350	.550	.300	3.084	3.175	3.326	8.576	8.167	7.484
113	2.450	.550	.300	3.093	3.134	3.335	8.585	8.175	7.492
115	2.550	.550	.300	3.102	3.172	3.343	8.593	8.182	7.499
117	2.650	.550	.300	3.107	3.203	3.350	8.600	8.189	7.505
119	2.750	.550	.300	3.116	3.226	3.357	8.606	8.195	7.511
121	2.850	.550	.300	3.122	3.241	3.361	8.611		

UIC 2

3	2.950	.750	.300	2.340	2.190	2.728	2.451	2.917	2.360
5	.950	.850	.300	.178	.249	.253	.769	.711	.623
6	.157	.050	.300	.363	.422	.519	1.460	1.363	1.180
7	.250	.850	.300	.561	.613	.779	2.054	1.906	1.659
8	.350	.450	.300	.761	.851	1.027	2.513	2.334	2.029
9	.450	.350	.300	.951	1.055	1.254	2.872	2.662	2.311
10	.550	.250	.300	1.122	1.246	1.453	3.140	2.909	2.523
11	.650	.150	.300	1.272	1.403	1.622	3.342	3.095	2.683
12	.750	.050	.300	1.399	1.535	1.763	3.495	3.236	2.804
13	.850	.050	.300	1.505	1.646	1.840	3.613	3.345	2.898
14	.950	.050	.300	1.595	1.738	1.976	3.705	3.430	2.971
15	1.050	.050	.300	1.659	1.814	2.056	3.770	3.497	3.029
16	1.150	.050	.300	1.731	1.876	2.122	3.836	3.551	3.076
17	1.250	.050	.300	1.773	1.931	2.177	3.894	3.595	3.114
18	1.350	.050	.300	1.827	1.976	2.223	3.923	3.631	3.146
19	1.450	.050	.300	1.884	2.013	2.262	3.955	3.662	3.173
20	1.550	.050	.300	1.895	2.015	2.295	3.992	3.687	3.195
21	1.650	.050	.300	1.923	2.073	2.323	4.006	3.709	3.214
22	1.750	.050	.300	1.975	2.095	2.347	4.025	3.727	3.230
23	1.850	.050	.300	1.965	2.117	2.358	4.042	3.743	3.245
24	1.950	.050	.300	1.999	2.134	2.366	4.057	3.757	3.257
25	2.050	.050	.300	1.999	2.150	2.401	4.070	3.769	3.268
26	2.150	.050	.300	2.012	2.153	2.415	4.081	3.780	3.277
27	2.250	.050	.300	2.024	2.175	2.427	4.091	3.789	3.286
28	2.350	.050	.300	2.035	2.136	2.438	4.100	3.797	3.293
29	2.450	.050	.300	2.044	2.176	2.447	4.104	3.805	3.300
30	2.550	.050	.300	2.053	2.204	2.456	4.115	3.811	3.306
31	2.650	.050	.300	2.060	2.212	2.464	4.121	3.817	3.311
32	2.750	.050	.300	2.067	2.218	2.470	4.127	3.823	3.316
33	2.850	.050	.300	2.073	2.224	2.476	4.132	3.828	3.321
34	2.950	.050	.300	2.079	2.230	2.482	4.137	3.832	3.325
35	.050	.950	.300	.161	.109	.235	.559	.513	.436
36	.150	.850	.300	.326	.300	.470	1.075	.986	.837
37	.250	.750	.300	.495	.472	.699	1.519	1.392	1.181
38	.350	.650	.300	.665	.659	.917	1.882	1.724	1.481
39	.450	.550	.300	.825	.834	1.116	2.170	1.986	1.681
40	.550	.450	.300	.972	1.072	1.293	2.393	2.189	1.850
41	.650	.350	.300	1.103	1.231	1.445	2.565	2.346	1.981
42	.750	.250	.300	1.216	1.350	1.575	2.699	2.458	2.083
43	.850	.150	.300	1.312	1.451	1.684	2.803	2.553	2.162
44	.950	.050	.300	1.394	1.537	1.775	2.886	2.638	2.225
45	1.050	.050	.300	1.463	1.609	1.851	2.952	2.698	2.276
46	1.150	.050	.300	1.522	1.669	1.915	3.005	2.747	2.317
47	1.250	.050	.300	1.571	1.720	1.969	3.049	2.787	2.350
48	1.350	.050	.300	1.613	1.753	2.014	3.086	2.820	2.379
49	1.450	.050	.300	1.649	1.780	2.052	3.115	2.843	2.402
50	1.550	.050	.300	1.680	1.832	2.105	3.140	2.871	2.422
51	1.650	.050	.300	1.705	1.859	2.113	3.162	2.891	2.440
52	1.750	.050	.300	1.727	1.882	2.137	3.180	2.908	2.454
53	1.850	.050	.300	1.749	1.902	2.158	3.197	2.923	2.467
54	1.950	.050	.300	1.766	1.920	2.176	3.210	2.936	2.479
55	2.050	.050	.300	1.782	1.935	2.191	3.223	2.947	2.489
56	2.150	.050	.300	1.795	1.949	2.205	3.233	2.957	2.497
57	2.250	.050	.300	1.807	1.951	2.218	3.243	2.966	2.505
58	2.350	.050	.300	1.817	1.972	2.228	3.251	2.974	2.512
59	2.450	.050	.300	1.827	1.981	2.233	3.259	2.981	2.518
60	2.550	.050	.300	1.835	1.989	2.247	3.265	2.987	2.524
61	2.650	.050	.300	1.843	1.997	2.254	3.271	2.993	2.529
62	2.750	.050	.300	1.850	1.999	2.261	3.277	2.998	2.534
63	2.850	.050	.300	1.855	2.000	2.266	3.282	2.999	2.538

WEST

פסוק

1	2.950	1.150	.300	1.533	1.625	1.939	2.123	1.834	1.484
2	.950	1.250	.300	.119	.140	.174	.232	.203	.154
3	.150	1.250	.300	.237	.273	.346	.453	.390	.301
4	.750	1.250	.300	.353	.412	.511	.654	.571	.433
5	.350	1.250	.300	.466	.541	.666	.830	.724	.546
6	.950	1.250	.300	.574	.663	.810	.980	.854	.644
7	.550	1.250	.300	.671	.774	.941	1.104	.962	.724
8	.650	1.250	.300	.766	.875	1.057	1.207	1.050	.790
9	.750	1.250	.300	.848	.965	1.150	1.291	1.123	.843
10	.850	1.250	.300	.921	1.044	1.249	1.399	1.182	.886
11	.950	1.250	.300	.985	1.113	1.326	1.415	1.230	.922
12	1.350	1.250	.300	1.541	1.173	1.373	1.462	1.271	.952
13	1.150	1.250	.300	1.390	1.225	1.450	1.500	1.304	.977
14	1.250	1.250	.300	1.133	1.270	1.500	1.533	1.332	.998
15	1.350	1.250	.300	1.170	1.319	1.542	1.560	1.356	1.015
16	1.450	1.250	.300	1.202	1.343	1.579	1.583	1.376	1.031
17	1.550	1.250	.300	1.230	1.373	1.610	1.603	1.393	1.044
18	1.650	1.250	.300	1.255	1.396	1.636	1.620	1.408	1.055
19	1.750	1.250	.300	1.276	1.421	1.652	1.635	1.421	1.066
20	1.850	1.250	.300	1.295	1.440	1.663	1.647	1.433	1.074
21	1.950	1.250	.300	1.312	1.458	1.671	1.659	1.443	1.082
22	2.050	1.250	.300	1.327	1.473	1.677	1.669	1.452	1.089
23	2.150	1.250	.300	1.340	1.487	1.673	1.678	1.459	1.096
24	2.250	1.250	.300	1.351	1.497	1.674	1.686	1.467	1.102
25	2.350	1.250	.300	1.362	1.510	1.676	1.693	1.473	1.107
26	2.450	1.250	.300	1.371	1.519	1.676	1.699	1.479	1.111
27	2.550	1.250	.300	1.380	1.528	1.675	1.705	1.484	1.116
28	2.650	1.250	.300	1.387	1.536	1.673	1.710	1.488	1.119
29	2.750	1.250	.300	1.394	1.543	1.670	1.714	1.493	1.123
30	2.850	1.250	.300	1.400	1.549	1.677	1.719	1.497	1.126
31	2.950	1.250	.300	1.406	1.555	1.683	1.723	1.500	1.129
32	.350	1.350	.300	.107	.126	.158	.177	.152	.109
33	.150	1.350	.300	.214	.251	.313	.347	.297	.213
34	.750	1.350	.300	.319	.372	.462	.503	.430	.307
35	.350	1.350	.300	.420	.449	.603	.642	.548	.391
36	.950	1.350	.300	.516	.594	.734	.782	.650	.463
37	.550	1.350	.300	.606	.699	.854	.864	.736	.523
38	.650	1.350	.300	.689	.771	.961	.949	.808	.573
39	.750	1.350	.300	.764	.874	1.057	1.019	.867	.614
40	.850	1.350	.300	.831	.947	1.141	1.078	.917	.646
41	.950	1.350	.300	.890	1.012	1.214	1.127	.958	.676
42	1.050	1.350	.300	.943	1.053	1.278	1.167	.992	.700
43	1.150	1.350	.300	.987	1.118	1.333	1.202	1.021	.720
44	1.250	1.350	.300	1.029	1.151	1.381	1.230	1.045	.737
45	1.350	1.350	.300	1.165	1.179	1.422	1.255	1.066	.752
46	1.450	1.350	.300	1.096	1.232	1.458	1.275	1.084	.764
47	1.550	1.350	.300	1.123	1.261	1.440	1.293	1.099	.776
48	1.650	1.350	.300	1.147	1.236	1.517	1.309	1.112	.785
49	1.750	1.350	.300	1.168	1.310	1.541	1.322	1.124	.794
50	1.850	1.350	.300	1.187	1.327	1.552	1.334	1.134	.801
51	1.950	1.350	.300	1.203	1.345	1.540	1.345	1.143	.808
52	2.050	1.350	.300	1.218	1.360	1.597	1.354	1.152	.814
53	2.150	1.350	.300	1.231	1.373	1.611	1.362	1.159	.820
54	2.250	1.350	.300	1.245	1.385	1.624	1.369	1.165	.825
55	2.350	1.350	.300	1.253	1.376	1.635	1.376	1.171	.829
56	2.450	1.350	.300	1.262	1.406	1.645	1.382	1.176	.833
57	2.550	1.350	.300	1.271	1.415	1.655	1.387	1.181	.837
58	2.650	1.350	.300	1.277	1.422	1.663	1.392	1.185	.841
59	2.750	1.350	.300	1.285	1.430	1.670	1.396	1.189	.844
60	2.850	1.350	.300	1.291	1.434	1.674	1.398	1.191	.845
61	2.950	1.350	.300	1.294	1.437	1.677	1.399	1.192	.846

1125

1.750	1.450	.300	1.227	1.132	1.113	1.159	1.176	.899
1.750	1.450	.300	1.157	1.115	1.102	1.136	1.119	.876
1.750	1.450	.300	1.175	1.225	1.219	1.267	1.223	.193
1.250	1.450	.300	1.208	1.117	1.119	1.109	1.329	.215
1.750	1.450	.300	1.180	1.113	1.110	1.192	1.115	.275
1.150	1.450	.300	1.167	1.112	1.110	1.195	1.195	.327
1.550	1.450	.300	1.148	1.119	1.118	1.178	1.163	.371
1.650	1.450	.300	1.123	1.119	1.117	1.149	1.121	.408
1.750	1.450	.300	1.122	1.125	1.117	1.108	1.170	.439
1.450	1.450	.300	1.159	1.133	1.115	1.158	1.111	.465
1.550	1.450	.300	1.167	1.139	1.115	1.100	1.145	.487
1.250	1.450	.300	1.153	1.177	1.176	1.135	1.174	.505
1.150	1.450	.300	1.102	1.125	1.125	1.165	1.190	.521
1.250	1.450	.300	1.141	1.166	1.176	1.190	1.119	.535
1.350	1.450	.300	1.174	1.133	1.116	1.112	1.137	.546
1.150	1.450	.300	1.104	1.135	1.131	1.100	1.153	.556
1.550	1.450	.300	1.131	1.153	1.132	1.147	1.166	.565
1.650	1.450	.300	1.159	1.197	1.110	1.161	1.178	.573
1.750	1.450	.300	1.175	1.219	1.133	1.173	1.188	.580
1.150	1.450	.300	1.103	1.123	1.135	1.134	1.197	.597
1.750	1.450	.300	1.167	1.216	1.175	1.193	1.195	.592
1.350	1.450	.300	1.141	1.211	1.149	1.102	1.113	.597
1.150	1.450	.300	1.137	1.279	1.109	1.107	1.119	.602
1.250	1.450	.300	1.148	1.216	1.117	1.116	1.125	.608
1.350	1.450	.300	1.153	1.277	1.128	1.122	1.130	.610
1.450	1.450	.300	1.169	1.337	1.139	1.127	1.135	.614
1.550	1.450	.300	1.175	1.315	1.143	1.132	1.137	.617
1.650	1.450	.300	1.169	1.323	1.158	1.137	1.143	.620
1.750	1.450	.300	1.191	1.331	1.159	1.141	1.147	.623
1.150	1.450	.300	1.197	1.337	1.171	1.145	1.150	.625
1.250	1.450	.300	1.203	1.343	1.177	1.148	1.153	.628
1.150	1.550	.300	1.109	1.131	1.130	1.105	1.105	.652
1.150	1.550	.300	1.175	1.207	1.250	1.207	1.168	.101
1.250	1.550	.300	1.202	1.337	1.342	1.303	1.244	.147
1.350	1.550	.300	1.145	1.403	1.499	1.409	1.314	.189
1.450	1.550	.300	1.129	1.493	1.610	1.457	1.376	.225
1.550	1.550	.300	1.193	1.578	1.711	1.534	1.430	.256
1.650	1.550	.300	1.507	1.618	1.804	1.592	1.476	.283
1.750	1.550	.300	1.530	1.726	1.907	1.642	1.516	.305
1.050	1.550	.300	1.587	1.796	1.951	1.704	1.549	.324
1.150	1.550	.300	1.739	1.947	1.927	1.720	1.577	.340
1.150	1.550	.300	1.735	1.873	1.936	1.750	1.601	.354
1.150	1.550	.300	1.927	1.943	1.137	1.776	1.622	.366
1.150	1.550	.300	1.953	1.943	1.162	1.795	1.640	.376
1.150	1.550	.300	1.996	1.016	1.222	1.117	1.655	.385
1.120	1.550	.300	1.925	1.049	1.256	1.139	1.668	.393
1.150	1.550	.300	1.953	1.176	1.237	1.143	1.680	.400
1.150	1.550	.300	1.973	1.131	1.319	1.161	1.690	.406
1.750	1.550	.300	1.973	1.122	1.337	1.172	1.699	.412
1.150	1.550	.300	1.311	1.141	1.353	1.181	1.707	.417
1.750	1.550	.300	1.227	1.158	1.377	1.190	1.719	.421
1.150	1.550	.300	1.341	1.173	1.393	1.193	1.721	.425
1.150	1.550	.300	1.559	1.137	1.435	1.195	1.726	.429
1.250	1.550	.300	1.355	1.179	1.421	1.211	1.732	.433
1.350	1.550	.300	1.375	1.213	1.433	1.215	1.736	.436
1.450	1.550	.300	1.395	1.219	1.443	1.221	1.740	.439
1.550	1.550	.300	1.375	1.224	1.453	1.226	1.744	.442
1.650	1.550	.300	1.411	1.236	1.461	1.233	1.748	.444
1.750	1.550	.300	1.411	1.243	1.469	1.234	1.751	.447
1.850	1.550	.300	1.411	1.253	1.476	1.233	1.754	.449

UIC-T

1	2.250	1.500	.300	1.120	1.256	1.432	.941	.757	.451
2	.050	1.650	.300	.901	.095	.112	.382	.064	.034
3	.150	1.650	.300	.161	.139	.236	.161	.126	.066
4	.250	1.650	.300	.239	.210	.349	.236	.184	.097
5	.350	1.650	.300	.319	.300	.457	.305	.237	.124
6	.450	1.650	.300	.307	.451	.558	.367	.285	.148
7	.550	1.650	.300	.435	.529	.652	.421	.327	.169
8	.650	1.650	.300	.519	.600	.730	.469	.363	.187
9	.750	1.650	.300	.576	.656	.816	.510	.395	.202
10	.850	1.650	.300	.630	.726	.897	.545	.422	.215
11	.950	1.650	.300	.673	.790	.949	.576	.445	.226
12	1.050	1.650	.300	.721	.828	1.005	.602	.464	.236
13	1.150	1.650	.300	.761	.871	1.055	.624	.482	.244
14	1.250	1.650	.300	.795	.909	1.098	.643	.496	.251
15	1.350	1.650	.300	.827	.943	1.137	.660	.509	.258
16	1.450	1.650	.300	.859	.973	1.171	.674	.520	.263
17	1.550	1.650	.300	.879	1.000	1.201	.687	.530	.268
18	1.650	1.650	.300	.901	1.029	1.227	.698	.539	.273
19	1.750	1.650	.300	.921	1.055	1.251	.708	.547	.277
20	1.850	1.650	.300	.939	1.081	1.272	.717	.553	.281
21	1.950	1.650	.300	.959	1.099	1.290	.725	.560	.285
22	2.050	1.650	.300	.968	1.095	1.307	.732	.565	.288
23	2.150	1.650	.300	.961	1.119	1.322	.738	.570	.291
24	2.250	1.650	.300	.972	1.121	1.335	.743	.575	.294
25	2.350	1.650	.300	1.003	1.132	1.347	.749	.579	.296
26	2.450	1.650	.300	1.012	1.131	1.357	.753	.583	.299
27	2.550	1.650	.300	1.020	1.150	1.367	.757	.586	.301
28	2.650	1.650	.300	1.028	1.158	1.375	.761	.590	.303
29	2.750	1.650	.300	1.035	1.166	1.383	.765	.592	.305
30	2.850	1.650	.300	1.041	1.172	1.390	.768	.595	.307
31	2.950	1.650	.300	1.047	1.176	1.397	.771	.598	.309
32	.050	1.750	.300	.079	.037	.109	.064	.047	.026
33	.150	1.750	.300	.147	.173	.216	.126	.094	.040
34	.250	1.750	.300	.219	.256	.320	.185	.137	.055
35	.350	1.750	.300	.269	.337	.419	.239	.178	.075
36	.450	1.750	.300	.324	.413	.513	.280	.214	.090
37	.550	1.750	.300	.376	.485	.600	.322	.246	.103
38	.650	1.750	.300	.425	.552	.680	.371	.275	.114
39	.750	1.750	.300	.479	.613	.754	.405	.299	.123
40	.850	1.750	.300	.519	.669	.820	.435	.321	.131
41	.950	1.750	.300	.564	.720	.840	.460	.339	.137
42	1.050	1.750	.300	.605	.766	.933	.482	.355	.143
43	1.150	1.750	.300	.702	.837	.981	.501	.369	.148
44	1.250	1.750	.300	.736	.893	1.023	.518	.381	.153
45	1.350	1.750	.300	.766	.976	1.061	.532	.392	.157
46	1.450	1.750	.300	.792	.935	1.094	.545	.401	.161
47	1.550	1.750	.300	.816	.932	1.123	.556	.409	.164
48	1.650	1.750	.300	.839	.955	1.150	.566	.416	.167
49	1.750	1.750	.300	.857	.976	1.173	.574	.423	.170
50	1.850	1.750	.300	.874	.994	1.194	.582	.429	.173
51	1.950	1.750	.300	.893	1.011	1.212	.589	.434	.175
52	2.050	1.750	.300	.914	1.026	1.229	.595	.439	.178
53	2.150	1.750	.300	.915	1.039	1.244	.601	.443	.180
54	2.250	1.750	.300	.927	1.051	1.257	.606	.447	.182
55	2.350	1.750	.300	.930	1.062	1.269	.611	.451	.184
56	2.450	1.750	.300	.947	1.072	1.280	.615	.454	.186
57	2.550	1.750	.300	.955	1.081	1.289	.619	.457	.188
58	2.650	1.750	.300	.963	1.089	1.298	.622	.460	.190
59	2.750	1.750	.300	.970	1.096	1.306	.625	.463	.191
60	2.850	1.750	.300	.975	1.103	1.313	.626	.465	.193

UET

1	1.250	1.750	.300	.750	1.134	1.320	.831	.467	.194
2	1.250	1.750	.300	.800	1.139	1.330	.838	.469	.196
3	1.250	1.750	.300	.850	1.144	1.340	.845	.471	.198
4	1.250	1.750	.300	.900	1.149	1.350	.852	.473	.200
5	1.250	1.750	.300	.950	1.154	1.360	.859	.475	.202
6	1.250	1.750	.300	1.000	1.159	1.370	.866	.477	.204
7	1.250	1.750	.300	1.050	1.164	1.380	.873	.479	.206
8	1.250	1.750	.300	1.100	1.169	1.390	.880	.481	.208
9	1.250	1.750	.300	1.150	1.174	1.400	.887	.483	.210
10	1.250	1.750	.300	1.200	1.179	1.410	.894	.485	.212
11	1.250	1.750	.300	1.250	1.184	1.420	.901	.487	.214
12	1.250	1.750	.300	1.300	1.189	1.430	.908	.489	.216
13	1.250	1.750	.300	1.350	1.194	1.440	.915	.491	.218
14	1.250	1.750	.300	1.400	1.199	1.450	.922	.493	.220
15	1.250	1.750	.300	1.450	1.204	1.460	.929	.495	.222
16	1.250	1.750	.300	1.500	1.209	1.470	.936	.497	.224
17	1.250	1.750	.300	1.550	1.214	1.480	.943	.499	.226
18	1.250	1.750	.300	1.600	1.219	1.490	.950	.501	.228
19	1.250	1.750	.300	1.650	1.224	1.500	.957	.503	.230
20	1.250	1.750	.300	1.700	1.229	1.510	.964	.505	.232
21	1.250	1.750	.300	1.750	1.234	1.520	.971	.507	.234
22	1.250	1.750	.300	1.800	1.239	1.530	.978	.509	.236
23	1.250	1.750	.300	1.850	1.244	1.540	.985	.511	.238
24	1.250	1.750	.300	1.900	1.249	1.550	.992	.513	.240
25	1.250	1.750	.300	1.950	1.254	1.560	.999	.515	.242
26	1.250	1.750	.300	2.000	1.259	1.570	1.006	.517	.244
27	1.250	1.750	.300	2.050	1.264	1.580	1.013	.519	.246
28	1.250	1.750	.300	2.100	1.269	1.590	1.020	.521	.248
29	1.250	1.750	.300	2.150	1.274	1.600	1.027	.523	.250
30	1.250	1.750	.300	2.200	1.279	1.610	1.034	.525	.252
31	1.250	1.750	.300	2.250	1.284	1.620	1.041	.527	.254
32	1.250	1.750	.300	2.300	1.289	1.630	1.048	.529	.256
33	1.250	1.750	.300	2.350	1.294	1.640	1.055	.531	.258
34	1.250	1.750	.300	2.400	1.299	1.650	1.062	.533	.260
35	1.250	1.750	.300	2.450	1.304	1.660	1.069	.535	.262
36	1.250	1.750	.300	2.500	1.309	1.670	1.076	.537	.264
37	1.250	1.750	.300	2.550	1.314	1.680	1.083	.539	.266
38	1.250	1.750	.300	2.600	1.319	1.690	1.090	.541	.268
39	1.250	1.750	.300	2.650	1.324	1.700	1.097	.543	.270
40	1.250	1.750	.300	2.700	1.329	1.710	1.104	.545	.272
41	1.250	1.750	.300	2.750	1.334	1.720	1.111	.547	.274
42	1.250	1.750	.300	2.800	1.339	1.730	1.118	.549	.276
43	1.250	1.750	.300	2.850	1.344	1.740	1.125	.551	.278
44	1.250	1.750	.300	2.900	1.349	1.750	1.132	.553	.280
45	1.250	1.750	.300	2.950	1.354	1.760	1.139	.555	.282
46	1.250	1.750	.300	3.000	1.359	1.770	1.146	.557	.284
47	1.250	1.750	.300	3.050	1.364	1.780	1.153	.559	.286
48	1.250	1.750	.300	3.100	1.369	1.790	1.160	.561	.288
49	1.250	1.750	.300	3.150	1.374	1.800	1.167	.563	.290
50	1.250	1.750	.300	3.200	1.379	1.810	1.174	.565	.292
51	1.250	1.750	.300	3.250	1.384	1.820	1.181	.567	.294
52	1.250	1.750	.300	3.300	1.389	1.830	1.188	.569	.296
53	1.250	1.750	.300	3.350	1.394	1.840	1.195	.571	.298
54	1.250	1.750	.300	3.400	1.399	1.850	1.202	.573	.300
55	1.250	1.750	.300	3.450	1.404	1.860	1.209	.575	.302
56	1.250	1.750	.300	3.500	1.409	1.870	1.216	.577	.304
57	1.250	1.750	.300	3.550	1.414	1.880	1.223	.579	.306
58	1.250	1.750	.300	3.600	1.419	1.890	1.230	.581	.308
59	1.250	1.750	.300	3.650	1.424	1.900	1.237	.583	.310
60	1.250	1.750	.300	3.700	1.429	1.910	1.244	.585	.312
61	1.250	1.750	.300	3.750	1.434	1.920	1.251	.587	.314
62	1.250	1.750	.300	3.800	1.439	1.930	1.258	.589	.316
63	1.250	1.750	.300	3.850	1.444	1.940	1.265	.591	.318

UCT

2.950	1.950	.300	.371	.939	1.136	.410	.271	.125
.950	2.350	.300	.059	.050	.085	.039	.019	-.003
.150	2.050	.300	.115	.135	.100	.059	.035	-.005
.250	2.050	.300	.171	.200	.230	.087	.051	-.008
.350	2.050	.300	.225	.259	.329	.113	.067	-.011
.450	2.050	.300	.277	.325	.409	.138	.081	-.014
.550	2.050	.300	.327	.382	.475	.160	.099	-.017
.650	2.050	.300	.374	.436	.541	.180	.105	-.020
.750	2.050	.300	.418	.487	.602	.198	.115	-.023
.850	2.050	.300	.459	.534	.658	.215	.124	-.026
.950	2.050	.300	.497	.577	.710	.229	.132	-.029
1.050	2.050	.300	.532	.616	.757	.241	.139	-.031
1.150	2.050	.300	.564	.652	.795	.253	.145	-.033
1.250	2.050	.300	.593	.684	.836	.262	.151	-.035
1.350	2.050	.300	.619	.714	.872	.271	.156	-.036
1.450	2.050	.300	.643	.741	.903	.279	.160	-.030
1.550	2.050	.300	.665	.765	.931	.286	.164	-.039
1.650	2.050	.300	.685	.787	.956	.292	.168	-.039
1.750	2.050	.300	.703	.806	.979	.298	.171	-.040
1.850	2.050	.300	.717	.824	.999	.303	.174	-.040
1.950	2.050	.300	.733	.840	1.018	.307	.177	-.040
2.050	2.050	.300	.747	.854	1.034	.312	.180	-.040
2.150	2.050	.300	.757	.868	1.049	.315	.182	-.040
2.250	2.050	.300	.770	.880	1.062	.319	.184	-.040
2.350	2.050	.300	.779	.890	1.074	.322	.186	-.040
2.450	2.050	.300	.789	.900	1.085	.325	.188	-.040
2.550	2.050	.300	.797	.909	1.095	.328	.190	-.039
2.650	2.050	.300	.805	.917	1.105	.330	.192	-.039
2.750	2.050	.300	.812	.925	1.113	.333	.194	-.038
2.850	2.050	.300	.818	.931	1.120	.335	.195	-.038
2.950	2.050	.300	.824	.938	1.127	.337	.197	-.037
.050	2.150	.300	.053	.053	.076	.023	.012	-.007
.150	2.150	.300	.106	.125	.156	.045	.023	-.014
.250	2.150	.300	.153	.185	.232	.067	.034	-.021
.350	2.150	.300	.200	.245	.305	.087	.044	-.027
.450	2.150	.300	.247	.301	.375	.106	.054	-.034
.550	2.150	.300	.293	.355	.441	.124	.062	-.040
.650	2.150	.300	.347	.408	.503	.140	.070	-.046
.750	2.150	.300	.389	.453	.561	.154	.077	-.052
.850	2.150	.300	.427	.497	.614	.167	.083	-.057
.950	2.150	.300	.463	.538	.664	.179	.088	-.062
1.050	2.150	.300	.495	.576	.708	.188	.093	-.066
1.150	2.150	.300	.525	.610	.749	.197	.097	-.070
1.250	2.150	.300	.554	.641	.786	.205	.101	-.073
1.350	2.150	.300	.580	.670	.820	.213	.104	-.076
1.450	2.150	.300	.603	.695	.850	.219	.107	-.079
1.550	2.150	.300	.624	.719	.878	.225	.110	-.081
1.650	2.150	.300	.643	.740	.903	.230	.113	-.083
1.750	2.150	.300	.661	.759	.925	.235	.115	-.084
1.850	2.150	.300	.675	.777	.945	.239	.117	-.086
1.950	2.150	.300	.691	.793	.963	.243	.119	-.087
2.050	2.150	.300	.704	.807	.980	.246	.121	-.087
2.150	2.150	.300	.716	.820	.994	.250	.123	-.088
2.250	2.150	.300	.727	.832	1.008	.253	.125	-.088
2.350	2.150	.300	.737	.843	1.020	.255	.126	-.089
2.450	2.150	.300	.745	.853	1.031	.258	.128	-.089
2.550	2.150	.300	.754	.862	1.041	.260	.129	-.089
2.650	2.150	.300	.762	.870	1.050	.263	.131	-.089
2.750	2.150	.300	.767	.877	1.057	.265	.132	-.089
2.850	2.150	.300	.773	.884	1.066	.267	.133	-.089

UIC 77

[illegible]

2.750	2.350	.300	.705	.117	.570	.151	.057	-.104
.350	2.450	.300	.703	.051	.603	.057	.000	-.014
.150	2.450	.300	.703	.111	.125	.111	.001	-.028
.250	2.450	.300	.127	.150	.137	.027	.001	-.042
.350	2.450	.310	.134	.178	.247	.035	.001	-.055
.450	2.450	.300	.219	.244	.304	.043	.001	-.068
.550	2.450	.300	.215	.238	.359	.050	.001	-.081
.650	2.450	.300	.252	.330	.411	.057	.001	-.092
.750	2.450	.300	.317	.373	.460	.063	.001	-.103
.850	2.450	.300	.349	.408	.506	.069	.001	-.113
.950	2.450	.320	.300	.413	.548	.074	.000	-.122
1.050	2.450	.300	.410	.475	.588	.078	-.000	-.131
1.150	2.450	.300	.435	.516	.624	.082	-.001	-.139
1.250	2.450	.300	.459	.534	.658	.086	-.001	-.146
1.350	2.450	.300	.482	.559	.688	.089	-.001	-.152
1.450	2.450	.300	.503	.583	.716	.093	-.001	-.158
1.550	2.450	.300	.522	.604	.742	.095	-.001	-.163
1.650	2.450	.300	.539	.624	.765	.098	-.001	-.167
1.750	2.450	.300	.555	.642	.787	.100	-.001	-.171
1.850	2.450	.300	.571	.659	.806	.102	-.001	-.174
1.950	2.450	.300	.589	.674	.824	.104	-.001	-.177
2.050	2.450	.300	.597	.688	.840	.106	-.001	-.180
2.150	2.450	.300	.604	.700	.855	.108	-.001	-.182
2.250	2.450	.300	.613	.712	.868	.110	-.001	-.184
2.350	2.450	.300	.620	.723	.880	.111	-.000	-.186
2.450	2.450	.300	.637	.732	.891	.113	.000	-.188
2.550	2.450	.300	.645	.741	.902	.114	.000	-.189
2.650	2.450	.300	.653	.749	.911	.115	.001	-.190
2.750	2.450	.300	.659	.757	.920	.117	.001	-.191
2.850	2.450	.300	.655	.764	.926	.118	.002	-.192
2.950	2.450	.300	.672	.770	.935	.119	.002	-.192
.350	2.550	.300	.045	.047	.059	.016	-.002	-.015
.150	2.550	.300	.080	.074	.117	.012	-.004	-.031
.250	2.550	.300	.119	.110	.175	.010	-.006	-.046
.350	2.550	.300	.157	.135	.231	.024	-.008	-.060
.450	2.550	.300	.195	.220	.235	.029	-.010	-.074
.550	2.550	.300	.230	.270	.336	.034	-.011	-.088
.650	2.550	.300	.265	.310	.385	.039	-.013	-.101
.750	2.550	.300	.297	.348	.432	.043	-.015	-.112
.850	2.550	.300	.324	.383	.476	.047	-.017	-.124
.950	2.550	.300	.357	.417	.516	.050	-.019	-.134
1.050	2.550	.300	.394	.448	.554	.053	-.020	-.143
1.150	2.550	.300	.429	.477	.589	.056	-.022	-.152
1.250	2.550	.300	.453	.504	.621	.059	-.023	-.160
1.350	2.550	.300	.455	.528	.651	.061	-.024	-.167
1.450	2.550	.300	.475	.551	.679	.063	-.024	-.173
1.550	2.550	.300	.493	.572	.704	.065	-.026	-.179
1.650	2.550	.300	.510	.591	.726	.067	-.027	-.184
1.750	2.550	.300	.526	.607	.747	.069	-.028	-.189
1.850	2.550	.300	.541	.625	.767	.070	-.028	-.193
1.950	2.550	.300	.554	.640	.784	.072	-.029	-.196
2.050	2.550	.300	.565	.654	.800	.073	-.029	-.199
2.150	2.550	.300	.574	.666	.815	.074	-.029	-.202
2.250	2.550	.300	.584	.678	.828	.076	-.029	-.205
2.350	2.550	.300	.597	.688	.840	.077	-.030	-.207
2.450	2.550	.300	.608	.698	.851	.078	-.030	-.209
2.550	2.550	.300	.613	.707	.867	.079	-.027	-.210
2.650	2.550	.300	.622	.715	.871	.080	-.027	-.212
2.750	2.550	.300	.627	.723	.876	.081	-.027	-.213
2.850	2.550	.300	.635	.733	.880	.082	-.027	-.214

UICET

1	2.250	2.950	4.300	5.337	6.621	7.738	8.816	9.811	10.770
2	2.500	3.200	4.550	5.587	6.871	7.988	9.066	10.061	11.020
3	2.750	3.450	4.800	5.837	7.121	8.238	9.316	10.311	11.270
4	3.000	3.700	5.050	6.087	7.371	8.488	9.566	10.561	11.520
5	3.250	3.950	5.300	6.337	7.621	8.738	9.816	10.811	11.770
6	3.500	4.200	5.550	6.587	7.871	8.988	10.066	11.061	12.020
7	3.750	4.450	5.800	6.837	8.121	9.238	10.316	11.311	12.270
8	4.000	4.700	6.050	7.087	8.371	9.488	10.566	11.561	12.520
9	4.250	4.950	6.300	7.337	8.621	9.738	10.816	11.811	12.770
10	4.500	5.200	6.550	7.587	8.871	9.988	11.066	12.061	13.020
11	4.750	5.450	6.800	7.837	9.121	10.238	11.316	12.311	13.270
12	5.000	5.700	7.050	8.087	9.371	10.488	11.566	12.561	13.520
13	5.250	5.950	7.300	8.337	9.621	10.738	11.816	12.811	13.770
14	5.500	6.200	7.550	8.587	9.871	10.988	12.066	13.061	14.020
15	5.750	6.450	7.800	8.837	10.121	11.238	12.316	13.311	14.270
16	6.000	6.700	8.050	9.087	10.371	11.488	12.566	13.561	14.520
17	6.250	6.950	8.300	9.337	10.621	11.738	12.816	13.811	14.770
18	6.500	7.200	8.550	9.587	10.871	11.988	13.066	14.061	15.020
19	6.750	7.450	8.800	9.837	11.121	12.238	13.316	14.311	15.270
20	7.000	7.700	9.050	10.087	11.371	12.488	13.566	14.561	15.520
21	7.250	7.950	9.300	10.337	11.621	12.738	13.816	14.811	15.770
22	7.500	8.200	9.550	10.587	11.871	12.988	14.066	15.061	16.020
23	7.750	8.450	9.800	10.837	12.121	13.238	14.316	15.311	16.270
24	8.000	8.700	10.050	11.087	12.371	13.488	14.566	15.561	16.520
25	8.250	8.950	10.300	11.337	12.621	13.738	14.816	15.811	16.770
26	8.500	9.200	10.550	11.587	12.871	13.988	15.066	16.061	17.020
27	8.750	9.450	10.800	11.837	13.121	14.238	15.316	16.311	17.270
28	9.000	9.700	11.050	12.087	13.371	14.488	15.566	16.561	17.520
29	9.250	9.950	11.300	12.337	13.621	14.738	15.816	16.811	17.770
30	9.500	10.200	11.550	12.587	13.871	14.988	16.066	17.061	18.020
31	9.750	10.450	11.800	12.837	14.121	15.238	16.316	17.311	18.270
32	10.000	10.700	12.050	13.087	14.371	15.488	16.566	17.561	18.520
33	10.250	10.950	12.300	13.337	14.621	15.738	16.816	17.811	18.770
34	10.500	11.200	12.550	13.587	14.871	15.988	17.066	18.061	19.020
35	10.750	11.450	12.800	13.837	15.121	16.238	17.316	18.311	19.270
36	11.000	11.700	13.050	14.087	15.371	16.488	17.566	18.561	19.520
37	11.250	11.950	13.300	14.337	15.621	16.738	17.816	18.811	19.770
38	11.500	12.200	13.550	14.587	15.871	16.988	18.066	19.061	20.020
39	11.750	12.450	13.800	14.837	16.121	17.238	18.316	19.311	20.270
40	12.000	12.700	14.050	15.087	16.371	17.488	18.566	19.561	20.520
41	12.250	12.950	14.300	15.337	16.621	17.738	18.816	19.811	20.770
42	12.500	13.200	14.550	15.587	16.871	17.988	19.066	20.061	21.020
43	12.750	13.450	14.800	15.837	17.121	18.238	19.316	20.311	21.270
44	13.000	13.700	15.050	16.087	17.371	18.488	19.566	20.561	21.520
45	13.250	13.950	15.300	16.337	17.621	18.738	19.816	20.811	21.770
46	13.500	14.200	15.550	16.587	17.871	18.988	20.066	21.061	22.020
47	13.750	14.450	15.800	16.837	18.121	19.238	20.316	21.311	22.270
48	14.000	14.700	16.050	17.087	18.371	19.488	20.566	21.561	22.520
49	14.250	14.950	16.300	17.337	18.621	19.738	20.816	21.811	22.770
50	14.500	15.200	16.550	17.587	18.871	19.988	21.066	22.061	23.020
51	14.750	15.450	16.800	17.837	19.121	20.238	21.316	22.311	23.270
52	15.000	15.700	17.050	18.087	19.371	20.488	21.566	22.561	23.520
53	15.250	15.950	17.300	18.337	19.621	20.738	21.816	22.811	23.770
54	15.500	16.200	17.550	18.587	19.871	20.988	22.066	23.061	24.020
55	15.750	16.450	17.800	18.837	20.121	21.238	22.316	23.311	24.270
56	16.000	16.700	18.050	19.087	20.371	21.488	22.566	23.561	24.520
57	16.250	16.950	18.300	19.337	20.621	21.738	22.816	23.811	24.770
58	16.500	17.200	18.550	19.587	20.871	21.988	23.066	24.061	25.020
59	16.750	17.450	18.800	19.837	21.121	22.238	23.316	24.311	25.270
60	17.000	17.700	19.050	20.087	21.371	22.488	23.566	24.561	25.520
61	17.250	17.950	19.300	20.337	21.621	22.738	23.816	24.811	25.770
62	17.500	18.200	19.550	20.587	21.871	22.988	24.066	25.061	26.020
63	17.750	18.450	19.800	20.837	22.121	23.238	24.316	25.311	26.270
64	18.000	18.700	20.050	21.087	22.371	23.488	24.566	25.561	26.520

UCT

1	2.750	.150	.400	5.252	4.831	4.151	8.592	5.157	7.296
2	.050	.250	.400	-3.313	-1.113	-5.947	3.151	2.220	1.985
3	.150	.250	.400	.036	-1.100	-3.447	4.474	5.213	5.325
4	.250	.250	.400	.892	.659	.391	5.176	5.862	5.321
5	.350	.250	.400	1.663	1.416	1.036	7.409	7.034	6.421
6	.450	.250	.400	2.335	2.099	1.707	8.262	7.862	7.195
7	.550	.250	.400	2.945	2.527	2.134	8.956	8.437	7.738
8	.650	.250	.400	3.224	2.959	2.541	9.277	8.845	8.125
9	.750	.250	.400	3.510	3.217	2.809	9.582	9.141	8.406
10	.850	.250	.400	3.725	3.457	3.011	9.808	9.360	8.614
11	.950	.250	.400	3.890	3.619	3.167	9.978	9.526	8.772
12	1.050	.250	.400	4.019	3.745	3.288	10.110	9.654	8.894
13	1.150	.250	.400	4.121	3.845	3.394	10.213	9.755	8.990
14	1.250	.250	.400	4.203	3.925	3.462	10.296	9.835	9.067
15	1.350	.250	.400	4.269	3.990	3.524	10.363	9.909	9.129
16	1.450	.250	.400	4.325	4.043	3.576	10.410	9.954	9.180
17	1.550	.250	.400	4.369	4.084	3.619	10.463	9.998	9.222
18	1.650	.250	.400	4.408	4.125	3.655	10.501	10.035	9.258
19	1.750	.250	.400	4.440	4.157	3.696	10.534	10.067	9.288
20	1.850	.250	.400	4.464	4.184	3.712	10.561	10.093	9.314
21	1.950	.250	.400	4.491	4.217	3.734	10.585	10.116	9.336
22	2.050	.250	.400	4.512	4.229	3.754	10.605	10.136	9.355
23	2.150	.250	.400	4.530	4.245	3.771	10.623	10.154	9.371
24	2.250	.250	.400	4.546	4.251	3.786	10.639	10.169	9.386
25	2.350	.250	.400	4.560	4.274	3.799	10.653	10.182	9.399
26	2.450	.250	.400	4.572	4.286	3.810	10.665	10.194	9.410
27	2.550	.250	.400	4.583	4.297	3.821	10.676	10.205	9.420
28	2.650	.250	.400	4.593	4.307	3.830	10.685	10.214	9.430
29	2.750	.250	.400	4.601	4.315	3.838	10.694	10.223	9.438
30	2.850	.250	.400	4.609	4.323	3.846	10.702	10.231	9.445
31	2.950	.250	.400	4.616	4.330	3.852	10.709	10.238	9.452
32	.350	.350	.400	-1.196	-1.139	-1.247	2.716	2.599	2.402
33	.450	.350	.400	.112	.042	-0.274	5.007	4.793	4.436
34	.550	.350	.400	.883	.539	.432	6.715	6.433	5.963
35	.650	.350	.400	1.312	1.211	1.015	7.913	7.566	7.040
36	.750	.350	.400	1.363	1.739	1.533	8.739	8.382	7.787
37	.850	.350	.400	2.362	2.170	1.949	9.314	8.936	8.308
38	.950	.350	.400	2.641	2.505	2.271	9.721	9.330	8.679
39	1.050	.350	.400	2.767	2.758	2.519	10.016	9.616	8.948
40	1.150	.350	.400	2.822	2.955	2.718	10.235	9.829	9.149
41	1.250	.350	.400	3.204	3.100	2.859	10.401	9.989	9.301
42	1.350	.350	.400	3.361	3.229	2.976	10.530	10.113	9.419
43	1.450	.350	.400	3.480	3.326	3.069	10.631	10.211	9.512
44	1.550	.350	.400	3.559	3.404	3.145	10.712	10.290	9.587
45	1.650	.350	.400	3.624	3.467	3.206	10.777	10.354	9.647
46	1.750	.350	.400	3.677	3.520	3.257	10.831	10.406	9.697
47	1.850	.350	.400	3.722	3.564	3.308	10.876	10.449	9.738
48	1.950	.350	.400	3.760	3.601	3.336	10.913	10.486	9.773
49	2.050	.350	.400	3.792	3.632	3.366	10.945	10.517	9.802
50	2.150	.350	.400	3.819	3.654	3.392	10.972	10.543	9.824
51	2.250	.350	.400	3.843	3.682	3.415	10.996	10.566	9.844
52	2.350	.350	.400	3.863	3.702	3.434	11.016	10.585	9.868
53	2.450	.350	.400	3.881	3.720	3.451	11.030	10.603	9.884
54	2.550	.350	.400	3.897	3.735	3.466	11.049	10.618	9.899
55	2.650	.350	.400	3.911	3.749	3.479	11.062	10.631	9.911
56	2.750	.350	.400	3.925	3.761	3.491	11.075	10.643	9.923
57	2.850	.350	.400	3.934	3.771	3.501	11.085	10.653	9.933
58	2.950	.350	.400	3.943	3.781	3.510	11.095	10.662	9.941
59	3.050	.350	.400	3.952	3.789	3.519	11.104	10.671	9.950
60	3.150	.350	.400	3.960	3.797	3.526	11.111	10.678	9.957

WEST

[illegible]

2	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	5.410	2
3	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	.779	3
4	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	1.453	4
5	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	2.100	5
6	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	2.590	6
7	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	2.971	7
8	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	3.264	8
9	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	3.469	9
10	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	3.661	10
11	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	3.796	11
12	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	3.901	12
13	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	3.986	13
14	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.054	14
15	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.109	15
16	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.155	16
17	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.194	17
18	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.226	18
19	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.254	19
20	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.277	20
21	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.297	21
22	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.315	22
23	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.331	23
24	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.344	24
25	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.356	25
26	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.367	26
27	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.376	27
28	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.385	28
29	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.393	29
30	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.399	30
31	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.406	31
32	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	32
33	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	33
34	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	34
35	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	35
36	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	36
37	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	37
38	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	38
39	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	39
40	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	40
41	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	41
42	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	42
43	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	43
44	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	44
45	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	45
46	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	46
47	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	47
48	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	48
49	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	49
50	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	50
51	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	51
52	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	52
53	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	53
54	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	54
55	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	55
56	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	56
57	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	57
58	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	58
59	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	59
60	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	60
61	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	61
62	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	62
63	2.750	.750	.400	2.250	2.322	2.547	2.221	2.221	4.411	63

2.250	.950	.400	1.000	1.900	2.077	1.276	1.010	3.500
.750	1.000	.400	1.000	1.122	.152	.536	.501	.443
.150	1.000	.400	.213	.210	.306	1.040	.972	.859
.250	1.000	.400	.332	.302	.465	1.188	1.390	1.227
.150	1.000	.400	.457	.520	.624	1.369	1.745	1.540
.450	1.000	.400	.504	.637	.779	2.102	2.037	1.796
.550	1.000	.400	.767	.708	.924	2.436	2.273	2.002
.650	1.000	.400	.022	.910	1.057	2.638	2.461	2.167
.750	1.000	.400	.727	1.020	1.175	2.800	2.611	2.297
.850	1.000	.400	1.041	1.110	1.279	2.929	2.731	2.402
.950	1.000	.400	1.164	1.203	1.370	3.133	2.828	2.486
1.050	1.000	.400	1.176	1.278	1.440	3.117	2.906	2.554
1.150	1.000	.400	1.200	1.342	1.515	3.136	2.970	2.610
1.250	1.000	.400	1.242	1.397	1.573	3.243	3.023	2.657
1.350	1.000	.400	1.309	1.445	1.622	3.290	3.067	2.695
1.450	1.000	.400	1.300	1.487	1.665	3.130	3.104	2.728
1.550	1.000	.400	1.415	1.523	1.702	3.354	3.136	2.756
1.650	1.000	.400	1.446	1.554	1.735	3.393	3.163	2.779
1.750	1.000	.400	1.473	1.562	1.763	3.417	3.186	2.800
1.850	1.000	.400	1.497	1.606	1.787	3.439	3.206	2.816
1.950	1.000	.400	1.514	1.627	1.809	3.457	3.223	2.833
2.050	1.000	.400	1.536	1.645	1.820	3.474	3.238	2.847
2.150	1.000	.400	1.562	1.662	1.844	3.488	3.252	2.859
2.250	1.000	.400	1.567	1.677	1.859	3.501	3.264	2.870
2.350	1.000	.400	1.560	1.676	1.872	3.512	3.275	2.879
2.450	1.000	.400	1.572	1.701	1.894	3.522	3.284	2.886
2.550	1.000	.400	1.562	1.712	1.895	3.531	3.293	2.895
2.650	1.000	.400	1.612	1.721	1.904	3.539	3.300	2.902
2.750	1.000	.400	1.620	1.730	1.913	3.546	3.307	2.908
2.850	1.000	.400	1.624	1.736	1.921	3.553	3.313	2.914
2.950	1.000	.400	1.635	1.745	1.928	3.559	3.319	2.919
.050	1.150	.400	.090	.115	.143	.410	.387	.337
.150	1.150	.400	.199	.232	.238	.813	.754	.656
.250	1.150	.400	.305	.353	.433	1.171	1.005	.943
.350	1.150	.400	.414	.475	.575	1.491	1.372	1.191
.450	1.150	.400	.525	.596	.715	1.742	1.613	1.398
.550	1.150	.400	.632	.712	.845	1.757	1.612	1.569
.650	1.150	.400	.733	.820	.965	2.132	1.973	1.706
.750	1.150	.400	.826	.919	1.073	2.275	2.104	1.820
.850	1.150	.400	.910	1.017	1.169	2.370	2.210	1.910
.950	1.150	.400	.965	1.095	1.253	2.404	2.246	1.984
1.050	1.150	.400	1.001	1.154	1.326	2.560	2.367	2.045
1.150	1.150	.400	1.109	1.214	1.370	2.524	2.425	2.095
1.250	1.150	.400	1.160	1.267	1.445	2.676	2.474	2.136
1.350	1.150	.400	1.214	1.312	1.473	2.721	2.515	2.172
1.450	1.150	.400	1.243	1.352	1.535	2.750	2.549	2.201
1.550	1.150	.400	1.277	1.387	1.571	2.769	2.578	2.226
1.650	1.150	.400	1.303	1.417	1.602	2.817	2.603	2.248
1.750	1.150	.400	1.332	1.449	1.630	2.840	2.625	2.267
1.850	1.150	.400	1.355	1.467	1.654	2.860	2.644	2.284
1.950	1.150	.400	1.376	1.488	1.675	2.870	2.650	2.298
2.050	1.150	.400	1.394	1.507	1.694	2.893	2.675	2.311
2.150	1.150	.400	1.410	1.523	1.711	2.907	2.688	2.322
2.250	1.150	.400	1.424	1.537	1.726	2.919	2.699	2.332
2.350	1.150	.400	1.437	1.550	1.739	2.930	2.709	2.341
2.450	1.150	.400	1.449	1.562	1.751	2.940	2.718	2.349
2.550	1.150	.400	1.469	1.573	1.762	2.948	2.726	2.356
2.650	1.150	.400	1.468	1.582	1.771	2.956	2.734	2.363
2.750	1.150	.400	1.477	1.591	1.780	2.963	2.740	2.368
2.850	1.150	.400	1.485	1.598	1.788	2.972	2.746	2.374

WEST

U E T

13A

1	2.250	1.550	.900	1.572	1.225	1.373	1.219	1.344	1.052
2	2.200	1.500	.900	1.565	1.200	1.372	1.216	1.341	1.051
3	2.150	1.450	.900	1.558	1.175	1.371	1.213	1.338	1.050
4	2.100	1.400	.900	1.551	1.150	1.370	1.210	1.335	1.049
5	2.050	1.350	.900	1.544	1.125	1.369	1.207	1.332	1.048
6	2.000	1.300	.900	1.537	1.100	1.368	1.204	1.329	1.047
7	1.950	1.250	.900	1.530	1.075	1.367	1.201	1.326	1.046
8	1.900	1.200	.900	1.523	1.050	1.366	1.198	1.323	1.045
9	1.850	1.150	.900	1.516	1.025	1.365	1.195	1.320	1.044
10	1.800	1.100	.900	1.509	1.000	1.364	1.192	1.317	1.043
11	1.750	1.050	.900	1.502	.975	1.363	1.189	1.314	1.042
12	1.700	1.000	.900	1.495	.950	1.362	1.186	1.311	1.041
13	1.650	.950	.900	1.488	.925	1.361	1.183	1.308	1.040
14	1.600	.900	.900	1.481	.900	1.360	1.180	1.305	1.039
15	1.550	.850	.900	1.474	.875	1.359	1.177	1.302	1.038
16	1.500	.800	.900	1.467	.850	1.358	1.174	1.299	1.037
17	1.450	.750	.900	1.460	.825	1.357	1.171	1.296	1.036
18	1.400	.700	.900	1.453	.800	1.356	1.168	1.293	1.035
19	1.350	.650	.900	1.446	.775	1.355	1.165	1.290	1.034
20	1.300	.600	.900	1.439	.750	1.354	1.162	1.287	1.033
21	1.250	.550	.900	1.432	.725	1.353	1.159	1.284	1.032
22	1.200	.500	.900	1.425	.700	1.352	1.156	1.281	1.031
23	1.150	.450	.900	1.418	.675	1.351	1.153	1.278	1.030
24	1.100	.400	.900	1.411	.650	1.350	1.150	1.275	1.029
25	1.050	.350	.900	1.404	.625	1.349	1.147	1.272	1.028
26	1.000	.300	.900	1.397	.600	1.348	1.144	1.269	1.027
27	.950	.250	.900	1.390	.575	1.347	1.141	1.266	1.026
28	.900	.200	.900	1.383	.550	1.346	1.138	1.263	1.025
29	.850	.150	.900	1.376	.525	1.345	1.135	1.260	1.024
30	.800	.100	.900	1.369	.500	1.344	1.132	1.257	1.023
31	.750	.050	.900	1.362	.475	1.343	1.129	1.254	1.022
32	.700	.000	.900	1.355	.450	1.342	1.126	1.251	1.021
33	.650	.000	.900	1.348	.425	1.341	1.123	1.248	1.020
34	.600	.000	.900	1.341	.400	1.340	1.120	1.245	1.019
35	.550	.000	.900	1.334	.375	1.339	1.117	1.242	1.018
36	.500	.000	.900	1.327	.350	1.338	1.114	1.239	1.017
37	.450	.000	.900	1.320	.325	1.337	1.111	1.236	1.016
38	.400	.000	.900	1.313	.300	1.336	1.108	1.233	1.015
39	.350	.000	.900	1.306	.275	1.335	1.105	1.230	1.014
40	.300	.000	.900	1.299	.250	1.334	1.102	1.227	1.013
41	.250	.000	.900	1.292	.225	1.333	1.099	1.224	1.012
42	.200	.000	.900	1.285	.200	1.332	1.096	1.221	1.011
43	.150	.000	.900	1.278	.175	1.331	1.093	1.218	1.010
44	.100	.000	.900	1.271	.150	1.330	1.090	1.215	1.009
45	.050	.000	.900	1.264	.125	1.329	1.087	1.212	1.008
46	.000	.000	.900	1.257	.100	1.328	1.084	1.209	1.007
47	.000	.000	.900	1.250	.075	1.327	1.081	1.206	1.006
48	.000	.000	.900	1.243	.050	1.326	1.078	1.203	1.005
49	.000	.000	.900	1.236	.025	1.325	1.075	1.200	1.004
50	.000	.000	.900	1.229	.000	1.324	1.072	1.197	1.003
51	.000	.000	.900	1.222	.000	1.323	1.069	1.194	1.002
52	.000	.000	.900	1.215	.000	1.322	1.066	1.191	1.001
53	.000	.000	.900	1.208	.000	1.321	1.063	1.188	1.000
54	.000	.000	.900	1.201	.000	1.320	1.060	1.185	.999
55	.000	.000	.900	1.194	.000	1.319	1.057	1.182	.998
56	.000	.000	.900	1.187	.000	1.318	1.054	1.179	.997
57	.000	.000	.900	1.180	.000	1.317	1.051	1.176	.996
58	.000	.000	.900	1.173	.000	1.316	1.048	1.173	.995
59	.000	.000	.900	1.166	.000	1.315	1.045	1.170	.994
60	.000	.000	.900	1.159	.000	1.314	1.042	1.167	.993
61	.000	.000	.900	1.152	.000	1.313	1.039	1.164	.992
62	.000	.000	.900	1.145	.000	1.312	1.036	1.161	.991
63	.000	.000	.900	1.138	.000	1.311	1.033	1.158	.990

UCT

1	1.250	1.750	.400	.507	1.265	1.246	1.127	.751	.689
2	1.300	1.700	.450	.524	1.287	1.236	1.120	.777	.704
3	1.350	1.650	.500	.541	1.307	1.170	1.127	.802	.729
4	1.400	1.600	.550	.558	1.327	1.203	1.203	.827	.754
5	1.450	1.550	.600	.575	1.347	1.234	1.242	.852	.779
6	1.500	1.500	.650	.592	1.367	1.264	1.270	.877	.804
7	1.550	1.450	.700	.609	1.387	1.295	1.300	.902	.829
8	1.600	1.400	.750	.626	1.407	1.325	1.331	.927	.854
9	1.650	1.350	.800	.643	1.427	1.356	1.362	.952	.879
10	1.700	1.300	.850	.660	1.447	1.386	1.392	.977	.904
11	1.750	1.250	.900	.677	1.467	1.417	1.423	1.002	.929
12	1.800	1.200	.950	.694	1.487	1.447	1.453	1.027	.954
13	1.850	1.150	1.000	.711	1.507	1.478	1.484	1.052	.979
14	1.900	1.100	1.050	.728	1.527	1.508	1.514	1.077	1.004
15	1.950	1.050	1.100	.745	1.547	1.539	1.545	1.102	1.029
16	2.000	1.000	1.150	.762	1.567	1.569	1.575	1.127	1.054
17	2.050	0.950	1.200	.779	1.587	1.600	1.606	1.152	1.079
18	2.100	0.900	1.250	.796	1.607	1.630	1.636	1.177	1.104
19	2.150	0.850	1.300	.813	1.627	1.661	1.667	1.202	1.129
20	2.200	0.800	1.350	.830	1.647	1.691	1.698	1.227	1.154
21	2.250	0.750	1.400	.847	1.667	1.722	1.728	1.252	1.179
22	2.300	0.700	1.450	.864	1.687	1.752	1.759	1.277	1.204
23	2.350	0.650	1.500	.881	1.707	1.783	1.789	1.302	1.229
24	2.400	0.600	1.550	.898	1.727	1.813	1.819	1.327	1.254
25	2.450	0.550	1.600	.915	1.747	1.844	1.850	1.352	1.279
26	2.500	0.500	1.650	.932	1.767	1.874	1.881	1.377	1.304
27	2.550	0.450	1.700	.949	1.787	1.905	1.911	1.402	1.329
28	2.600	0.400	1.750	.966	1.807	1.935	1.941	1.427	1.354
29	2.650	0.350	1.800	.983	1.827	1.965	1.971	1.452	1.379
30	2.700	0.300	1.850	1.000	1.847	1.996	2.002	1.477	1.404
31	2.750	0.250	1.900	1.017	1.867	2.026	2.032	1.502	1.429
32	2.800	0.200	1.950	1.034	1.887	2.057	2.063	1.527	1.454
33	2.850	0.150	2.000	1.051	1.907	2.087	2.094	1.552	1.479
34	2.900	0.100	2.050	1.068	1.927	2.118	2.124	1.577	1.504
35	2.950	0.050	2.100	1.085	1.947	2.148	2.154	1.602	1.529
36	3.000	0.000	2.150	1.102	1.967	2.179	2.185	1.627	1.554
37	3.050		2.200	1.119	1.987	2.209	2.215	1.652	1.579
38	3.100		2.250	1.136	2.007	2.240	2.246	1.677	1.604
39	3.150		2.300	1.153	2.027	2.270	2.276	1.702	1.629
40	3.200		2.350	1.170	2.047	2.301	2.307	1.727	1.654
41	3.250		2.400	1.187	2.067	2.331	2.337	1.752	1.679
42	3.300		2.450	1.204	2.087	2.362	2.368	1.777	1.704
43	3.350		2.500	1.221	2.107	2.392	2.398	1.802	1.729
44	3.400		2.550	1.238	2.127	2.423	2.429	1.827	1.754
45	3.450		2.600	1.255	2.147	2.453	2.459	1.852	1.779
46	3.500		2.650	1.272	2.167	2.484	2.490	1.877	1.804
47	3.550		2.700	1.289	2.187	2.514	2.520	1.902	1.829
48	3.600		2.750	1.306	2.207	2.545	2.551	1.927	1.854
49	3.650		2.800	1.323	2.227	2.575	2.581	1.952	1.879
50	3.700		2.850	1.340	2.247	2.606	2.612	1.977	1.904
51	3.750		2.900	1.357	2.267	2.636	2.642	2.002	1.929
52	3.800		2.950	1.374	2.287	2.667	2.673	2.027	1.954
53	3.850		3.000	1.391	2.307	2.697	2.703	2.052	1.979
54	3.900		3.050	1.408	2.327	2.728	2.734	2.077	2.004
55	3.950		3.100	1.425	2.347	2.758	2.764	2.102	2.029
56	4.000		3.150	1.442	2.367	2.789	2.795	2.127	2.054
57	4.050		3.200	1.459	2.387	2.819	2.825	2.152	2.079
58	4.100		3.250	1.476	2.407	2.850	2.856	2.177	2.104
59	4.150		3.300	1.493	2.427	2.880	2.886	2.202	2.129
60	4.200		3.350	1.510	2.447	2.911	2.917	2.227	2.154
61	4.250		3.400	1.527	2.467	2.941	2.947	2.252	2.179
62	4.300		3.450	1.544	2.487	2.972	2.978	2.277	2.204
63	4.350		3.500	1.561	2.507	3.002	3.008	2.302	2.229

WEST

3	2.150	1.750	.400	.750	.952	1.123	.113	.672	.435
5	2.150	1.750	.400	.750	.959	.974	.101	.651	.431
7	2.150	1.750	.400	.750	.966	.981	.101	.631	.401
9	2.150	1.750	.400	.750	.973	.988	.101	.611	.381
11	2.150	1.750	.400	.750	.980	.995	.101	.591	.361
13	2.150	1.750	.400	.750	.987	.998	.101	.571	.341
15	2.150	1.750	.400	.750	.994	.999	.101	.551	.321
17	2.150	1.750	.400	.750	.997	.999	.101	.531	.301
19	2.150	1.750	.400	.750	.999	.999	.101	.511	.281
21	2.150	1.750	.400	.750	.999	.999	.101	.491	.261
23	2.150	1.750	.400	.750	.999	.999	.101	.471	.241
25	2.150	1.750	.400	.750	.999	.999	.101	.451	.221
27	2.150	1.750	.400	.750	.999	.999	.101	.431	.201
29	2.150	1.750	.400	.750	.999	.999	.101	.411	.181
31	2.150	1.750	.400	.750	.999	.999	.101	.391	.161
33	2.150	1.750	.400	.750	.999	.999	.101	.371	.141
35	2.150	1.750	.400	.750	.999	.999	.101	.351	.121
37	2.150	1.750	.400	.750	.999	.999	.101	.331	.101
39	2.150	1.750	.400	.750	.999	.999	.101	.311	.081
41	2.150	1.750	.400	.750	.999	.999	.101	.291	.061
43	2.150	1.750	.400	.750	.999	.999	.101	.271	.041
45	2.150	1.750	.400	.750	.999	.999	.101	.251	.021
47	2.150	1.750	.400	.750	.999	.999	.101	.231	.001
49	2.150	1.750	.400	.750	.999	.999	.101	.211	.000
51	2.150	1.750	.400	.750	.999	.999	.101	.191	.000
53	2.150	1.750	.400	.750	.999	.999	.101	.171	.000
55	2.150	1.750	.400	.750	.999	.999	.101	.151	.000
57	2.150	1.750	.400	.750	.999	.999	.101	.131	.000
59	2.150	1.750	.400	.750	.999	.999	.101	.111	.000
61	2.150	1.750	.400	.750	.999	.999	.101	.091	.000
63	2.150	1.750	.400	.750	.999	.999	.101	.071	.000

UET

2.950	2.950	.950	.956	.775	.741	.491	.323	.127
.950	2.950	.950	.959	.845	.857	.629	.620	.397
.150	2.950	.950	.977	.935	.913	.57	.491	.313
.250	2.950	.950	.995	.995	.968	.565	.666	.319
.350	2.950	.950	.992	.973	.922	.511	.677	.325
.450	2.950	.950	.989	.921	.875	.437	.697	.330
.550	2.950	.950	.984	.822	.825	.360	.713	.335
.650	2.950	.950	.978	.701	.733	.282	.729	.339
.750	2.950	.950	.970	.518	.719	.202	.743	.343
.850	2.950	.950	.961	.321	.662	.221	.755	.346
.950	2.950	.950	.951	.126	.513	.233	.767	.349
1.050	2.950	.950	.939	.039	.390	.253	.777	.352
1.150	2.950	.950	.925	.069	.275	.267	.787	.354
1.250	2.950	.950	.909	.099	.163	.279	.795	.356
1.350	2.950	.950	.892	.022	.033	.290	.803	.358
1.450	2.950	.950	.873	.045	.066	.300	.810	.360
1.550	2.950	.950	.853	.067	.091	.312	.815	.361
1.650	2.950	.950	.831	.087	.115	.318	.822	.363
1.750	2.950	.950	.808	.106	.135	.325	.827	.364
1.850	2.950	.950	.783	.123	.156	.332	.832	.365
1.950	2.950	.950	.758	.139	.174	.338	.836	.366
2.050	2.950	.950	.731	.154	.191	.344	.840	.367
2.150	2.950	.950	.703	.167	.206	.349	.844	.368
2.250	2.950	.950	.675	.179	.220	.353	.847	.370
2.350	2.950	.950	.645	.191	.233	.358	.850	.371
2.450	2.950	.950	.615	.201	.245	.362	.853	.372
2.550	2.950	.950	.584	.209	.256	.365	.856	.373
2.650	2.950	.950	.552	.217	.266	.369	.859	.374
2.750	2.950	.950	.519	.225	.275	.372	.862	.375
2.850	2.950	.950	.487	.233	.283	.375	.865	.376
2.950	2.950	.950	.453	.242	.291	.377	.867	.376
.050	2.950	.950	.418	.250	.298	.379	.869	.377
.150	2.950	.950	.382	.258	.305	.381	.871	.378
.250	2.950	.950	.345	.266	.312	.383	.873	.379
.350	2.950	.950	.308	.273	.319	.385	.875	.380
.450	2.950	.950	.270	.280	.326	.387	.877	.381
.550	2.950	.950	.232	.287	.333	.389	.879	.382
.650	2.950	.950	.194	.294	.340	.391	.881	.383
.750	2.950	.950	.156	.301	.347	.393	.883	.384
.850	2.950	.950	.118	.308	.354	.395	.885	.385
.950	2.950	.950	.080	.315	.361	.397	.887	.386
1.050	2.950	.950	.042	.322	.368	.399	.889	.387
1.150	2.950	.950	.004	.329	.375	.401	.891	.388
1.250	2.950	.950	.000	.336	.382	.403	.893	.389
1.350	2.950	.950	.000	.343	.389	.405	.895	.390
1.450	2.950	.950	.000	.350	.396	.407	.897	.391
1.550	2.950	.950	.000	.357	.403	.409	.899	.392
1.650	2.950	.950	.000	.364	.410	.411	.901	.393
1.750	2.950	.950	.000	.371	.417	.413	.903	.394
1.850	2.950	.950	.000	.378	.424	.415	.905	.395
1.950	2.950	.950	.000	.385	.431	.417	.907	.396

0	2.750	2.750	2.750
1	2.750	2.750	2.750
2	2.750	2.750	2.750
3	2.750	2.750	2.750
4	2.750	2.750	2.750
5	2.750	2.750	2.750
6	2.750	2.750	2.750
7	2.750	2.750	2.750
8	2.750	2.750	2.750
9	2.750	2.750	2.750
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94	2.750	2.750	2.750
95	2.750	2.750	2.750
96	2.750	2.750	2.750
97	2.750	2.750	2.750

[illegible]

[illegible]

[illegible]

2	2.250	1.350	.500	1.228	1.317	1.405	2.350	2.471	2.154
4	.250	1.450	.500	.162	.073	.091	.251	.212	.216
6	.125	1.425	.500	.125	.107	.103	.319	.275	.213
8	.250	1.400	.500	.171	.222	.275	.751	.675	.603
10	.350	1.400	.500	.257	.277	.250	.750	.895	.775
12	.450	1.400	.500	.324	.377	.457	1.157	1.071	.928
14	.550	1.450	.500	.394	.453	.545	1.324	1.245	1.061
16	.650	1.450	.500	.467	.529	.630	1.468	1.358	1.174
18	.750	1.450	.500	.533	.599	.709	1.590	1.471	1.271
20	.850	1.450	.500	.595	.665	.783	1.594	1.566	1.353
22	.950	1.450	.500	.653	.727	.851	1.782	1.647	1.422
24	1.050	1.450	.500	.717	.784	.912	1.857	1.715	1.480
26	1.150	1.450	.500	.756	.835	.968	1.920	1.774	1.530
28	1.250	1.450	.500	.801	.882	1.010	1.974	1.823	1.572
30	1.350	1.450	.500	.841	.924	1.062	2.120	1.865	1.608
32	1.450	1.450	.500	.874	.962	1.102	2.359	1.932	1.639
34	1.550	1.450	.500	.913	.976	1.138	2.493	1.933	1.656
36	1.650	1.450	.500	.943	1.026	1.170	2.123	1.960	1.690
38	1.750	1.450	.500	.966	1.055	1.178	2.148	1.984	1.710
40	1.850	1.450	.500	.990	1.078	1.224	2.171	2.005	1.728
42	1.950	1.450	.500	1.011	1.099	1.247	2.191	2.023	1.744
44	2.050	1.450	.500	1.030	1.119	1.267	2.204	2.037	1.758
46	2.150	1.450	.500	1.048	1.137	1.285	2.224	2.054	1.770
48	2.250	1.450	.500	1.063	1.153	1.302	2.237	2.066	1.781
50	2.350	1.450	.500	1.077	1.157	1.317	2.250	2.078	1.791
52	2.450	1.450	.500	1.073	1.130	1.330	2.261	2.088	1.800
54	2.550	1.450	.500	1.102	1.172	1.343	2.271	2.095	1.806
56	2.650	1.450	.500	1.113	1.203	1.354	2.280	2.105	1.816
58	2.750	1.450	.500	1.122	1.213	1.364	2.288	2.114	1.823
60	2.850	1.450	.500	1.131	1.222	1.373	2.296	2.121	1.829
62	2.950	1.450	.500	1.137	1.230	1.381	2.303	2.127	1.834
64	.050	1.550	.500	.059	.039	.036	.216	.193	.170
66	.150	1.550	.500	.113	.113	.173	.425	.391	.334
68	.250	1.550	.500	.179	.209	.259	.622	.572	.484
70	.350	1.550	.500	.252	.280	.315	.803	.738	.630
72	.450	1.550	.500	.335	.351	.424	.966	.888	.757
74	.550	1.550	.500	.363	.421	.510	1.109	1.019	.869
76	.650	1.550	.500	.439	.447	.538	1.235	1.134	.965
78	.750	1.550	.500	.489	.553	.661	1.342	1.232	1.049
80	.850	1.550	.500	.546	.615	.740	1.435	1.317	1.120
82	.950	1.550	.500	.597	.672	.793	1.514	1.369	1.181
84	1.050	1.550	.500	.649	.725	.851	1.582	1.451	1.232
86	1.150	1.550	.500	.691	.773	.903	1.639	1.503	1.277
88	1.250	1.550	.500	.736	.817	.951	1.689	1.548	1.314
90	1.350	1.550	.500	.774	.856	.994	1.731	1.587	1.347
92	1.450	1.550	.500	.813	.892	1.032	1.769	1.621	1.375
94	1.550	1.550	.500	.857	.924	1.066	1.800	1.650	1.400
96	1.650	1.550	.500	.887	.953	1.077	1.828	1.675	1.421
98	1.750	1.550	.500	.912	.990	1.125	1.852	1.697	1.440
100	1.850	1.550	.500	.915	1.003	1.150	1.873	1.717	1.456
102	1.950	1.550	.500	.935	1.021	1.172	1.892	1.734	1.471
104	2.050	1.550	.500	.955	1.044	1.192	1.909	1.747	1.484
106	2.150	1.550	.500	.971	1.061	1.210	1.923	1.763	1.495
108	2.250	1.550	.500	.987	1.077	1.227	1.937	1.775	1.506
110	2.350	1.550	.500	1.000	1.091	1.241	1.945	1.786	1.515
112	2.450	1.550	.500	1.013	1.109	1.255	1.959	1.796	1.524
114	2.550	1.550	.500	1.025	1.115	1.267	1.969	1.805	1.531
116	2.650	1.550	.500	1.035	1.125	1.278	1.977	1.813	1.538
118	2.750	1.550	.500	1.045	1.136	1.288	1.985	1.820	1.545
120	2.850	1.550	.500	1.054	1.145	1.297	1.992	1.827	1.550

UIC 77

2	2.750	1.500	.500	1.271	1.153	1.396	1.299	1.253	1.356
4	.750	1.500	.500	.895	.835	.982	.879	.863	.837
6	.150	1.500	.500	.112	.131	.163	.153	.122	.271
8	.750	1.500	.500	.100	.177	.244	.218	.172	.397
10	.350	1.500	.500	.225	.253	.324	.271	.212	.513
12	.450	1.500	.500	.284	.320	.402	.340	.238	.619
14	.550	1.500	.500	.341	.392	.477	.403	.250	.712
16	.650	1.500	.500	.397	.454	.550	.462	.299	.794
18	.750	1.500	.500	.452	.514	.616	.513	.335	.866
20	.850	1.500	.500	.504	.571	.682	.571	.369	.927
22	.950	1.500	.500	.553	.623	.741	.620	.394	.980
24	1.050	1.500	.500	.598	.672	.796	.661	.419	1.026
26	1.150	1.500	.500	.640	.717	.845	.700	.444	1.065
28	1.250	1.500	.500	.679	.758	.890	.739	.469	1.099
30	1.350	1.500	.500	.715	.796	.931	.773	.494	1.128
32	1.450	1.500	.500	.747	.830	.966	.802	.519	1.154
34	1.550	1.500	.500	.777	.861	1.001	.832	.541	1.176
36	1.650	1.500	.500	.803	.889	1.031	.857	.564	1.195
38	1.750	1.500	.500	.828	.914	1.056	.881	.585	1.212
40	1.850	1.500	.500	.850	.937	1.082	.902	.604	1.227
42	1.950	1.500	.500	.869	.957	1.104	.923	.620	1.241
44	2.050	1.500	.500	.887	.976	1.124	.944	.634	1.253
46	2.150	1.500	.500	.904	.993	1.142	.966	.646	1.264
48	2.250	1.500	.500	.919	1.008	1.158	.981	.658	1.273
50	2.350	1.500	.500	.932	1.022	1.173	.992	.669	1.282
52	2.450	1.500	.500	.945	1.035	1.186	1.002	.679	1.290
54	2.550	1.500	.500	.956	1.047	1.198	1.011	.688	1.297
56	2.650	1.500	.500	.966	1.057	1.209	1.020	.696	1.303
58	2.750	1.500	.500	.975	1.067	1.219	1.027	.704	1.309
60	2.850	1.500	.500	.984	1.076	1.228	1.034	.712	1.315
62	2.950	1.500	.500	.992	1.084	1.237	1.040	.719	1.320
64	3.050	1.750	.500	.992	1.082	1.277	1.149	.715	1.111
66	.150	1.750	.500	.105	.123	.154	.129	.126	.220
68	.750	1.750	.500	.109	.135	.169	.133	.132	.323
70	.350	1.750	.500	.211	.216	.304	.262	.208	.419
72	.450	1.750	.500	.254	.257	.377	.301	.215	.506
74	.550	1.750	.500	.317	.316	.447	.377	.271	.585
76	.650	1.750	.500	.369	.365	.515	.422	.296	.654
78	.750	1.750	.500	.417	.409	.579	.465	.321	.715
80	.850	1.750	.500	.466	.453	.638	1.038	.437	.768
82	.950	1.750	.500	.511	.490	.694	1.101	.494	.814
84	1.050	1.750	.500	.554	.528	.745	1.157	.543	.854
86	1.150	1.750	.500	.593	.568	.792	1.204	.588	.888
88	1.250	1.750	.500	.627	.607	.835	1.246	.623	.918
90	1.350	1.750	.500	.653	.632	.874	1.282	.655	.945
92	1.450	1.750	.500	.673	.655	.910	1.313	.684	.967
94	1.550	1.750	.500	.721	.684	.942	1.341	.720	.987
96	1.650	1.750	.500	.747	.711	.971	1.365	.750	1.005
98	1.750	1.750	.500	.770	.735	.997	1.386	.774	1.020
100	1.850	1.750	.500	.771	.777	1.021	1.405	.766	1.034
102	1.950	1.750	.500	.810	.807	1.042	1.422	.811	1.046
104	2.050	1.750	.500	.828	.816	1.062	1.437	.825	1.057
106	2.150	1.750	.500	.844	.832	1.077	1.451	.837	1.067
108	2.250	1.750	.500	.855	.847	1.085	1.462	.847	1.076
110	2.350	1.750	.500	.872	.861	1.110	1.473	.867	1.084
112	2.450	1.750	.500	.884	.873	1.123	1.482	.876	1.091
114	2.550	1.750	.500	.895	.885	1.135	1.491	.884	1.098
116	2.650	1.750	.500	.905	.895	1.146	1.499	.891	1.104
118	2.750	1.750	.500	.914	.905	1.156	1.506	.898	1.109
120						1.165	1.513	.904	1.115

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131

2.750	2.450	.300	.364	.718	.835	.701	.530	.396
2.500	2.450	.050	.139	.090	.031	.037	.039	.025
2.250	2.450	.200	.167	.131	.101	.093	.077	.050
2.000	2.450	.450	.183	.121	.101	.138	.114	.075
1.750	2.450	.700	.135	.100	.109	.101	.150	.098
1.500	2.450	.950	.170	.179	.207	.222	.184	.120
1.250	2.450	1.200	.202	.236	.293	.260	.215	.141
1.000	2.450	1.450	.234	.272	.337	.296	.245	.160
.750	2.450	1.700	.269	.320	.330	.329	.272	.177
.500	2.450	1.950	.299	.341	.420	.360	.297	.193
.250	2.450	2.200	.322	.373	.455	.338	.320	.207
1.000	2.450	.050	.367	.409	.494	.413	.341	.220
1.150	2.450	.200	.370	.412	.525	.436	.359	.232
1.250	2.450	.300	.377	.459	.536	.456	.376	.242
1.350	2.450	.400	.422	.445	.589	.475	.391	.252
1.450	2.450	.500	.444	.519	.617	.492	.405	.260
1.550	2.450	.600	.463	.531	.642	.507	.417	.268
1.650	2.450	.700	.473	.551	.655	.520	.428	.275
1.750	2.450	.800	.505	.570	.637	.533	.438	.281
1.850	2.450	.900	.516	.590	.707	.544	.443	.287
1.950	2.450	1.000	.532	.605	.726	.554	.456	.292
2.050	2.450	1.100	.545	.620	.743	.563	.463	.297
2.150	2.450	1.200	.559	.634	.759	.572	.470	.301
2.250	2.450	1.300	.571	.647	.773	.579	.476	.305
2.350	2.450	1.400	.582	.657	.787	.586	.482	.309
2.450	2.450	1.500	.592	.670	.799	.593	.487	.312
2.550	2.450	1.600	.602	.680	.810	.599	.492	.315
2.650	2.450	1.700	.611	.690	.821	.604	.497	.318
2.750	2.450	1.800	.619	.697	.831	.607	.501	.321
2.850	2.450	1.900	.627	.707	.846	.613	.505	.324
2.950	2.450	2.000	.634	.715	.848	.617	.508	.326
3.050	2.450	2.100	.633	.718	.848	.610	.503	.320
3.150	2.450	2.200	.635	.726	.870	.600	.505	.340
3.250	2.450	2.300	.647	.734	.882	.610	.506	.359
3.350	2.450	2.400	.659	.743	.895	.615	.506	.378
3.450	2.450	2.500	.669	.752	.907	.624	.505	.396
3.550	2.450	2.600	.677	.761	.919	.633	.505	.412
3.650	2.450	2.700	.682	.769	.931	.641	.505	.427
3.750	2.450	2.800	.687	.777	.943	.649	.505	.441
3.850	2.450	2.900	.692	.785	.955	.657	.505	.454
3.950	2.450	3.000	.697	.793	.967	.665	.505	.466
4.050	2.450	3.100	.701	.801	.979	.673	.505	.478
4.150	2.450	3.200	.706	.809	.991	.681	.505	.489
4.250	2.450	3.300	.710	.817	1.003	.689	.505	.500
4.350	2.450	3.400	.715	.825	1.015	.697	.505	.511
4.450	2.450	3.500	.719	.833	1.027	.705	.505	.522
4.550	2.450	3.600	.724	.841	1.039	.713	.505	.533
4.650	2.450	3.700	.728	.849	1.051	.721	.505	.544
4.750	2.450	3.800	.733	.857	1.063	.729	.505	.554
4.850	2.450	3.900	.737	.86				

1	2.250	2.250	.500	.625	.633	.613	.565	.495	.295
2	2.250	2.250	.500	.631	.636	.645	.634	.627	.316
3	2.250	2.250	.500	.632	.637	.646	.635	.629	.331
4	2.250	2.250	.500	.633	.638	.647	.636	.631	.347
5	2.250	2.250	.500	.634	.639	.648	.637	.632	.361
6	2.250	2.250	.500	.635	.640	.649	.638	.633	.375
7	2.250	2.250	.500	.636	.641	.650	.639	.634	.388
8	2.250	2.250	.500	.637	.642	.651	.640	.635	.400
9	2.250	2.250	.500	.638	.643	.652	.641	.636	.411
10	2.250	2.250	.500	.639	.644	.653	.642	.637	.422
11	2.250	2.250	.500	.640	.645	.654	.643	.638	.431
12	2.250	2.250	.500	.641	.646	.655	.644	.639	.440
13	2.250	2.250	.500	.642	.647	.656	.645	.640	.449
14	2.250	2.250	.500	.643	.648	.657	.646	.641	.458
15	2.250	2.250	.500	.644	.649	.658	.647	.642	.467
16	2.250	2.250	.500	.645	.650	.659	.648	.643	.475
17	2.250	2.250	.500	.646	.651	.660	.649	.644	.484
18	2.250	2.250	.500	.647	.652	.661	.650	.645	.492
19	2.250	2.250	.500	.648	.653	.662	.651	.646	.500
20	2.250	2.250	.500	.649	.654	.663	.652	.647	.508
21	2.250	2.250	.500	.650	.655	.664	.653	.648	.516
22	2.250	2.250	.500	.651	.656	.665	.654	.649	.524
23	2.250	2.250	.500	.652	.657	.666	.655	.650	.532
24	2.250	2.250	.500	.653	.658	.667	.656	.651	.540
25	2.250	2.250	.500	.654	.659	.668	.657	.652	.548
26	2.250	2.250	.500	.655	.660	.669	.658	.653	.556
27	2.250	2.250	.500	.656	.661	.670	.659	.654	.564
28	2.250	2.250	.500	.657	.662	.671	.660	.655	.572
29	2.250	2.250	.500	.658	.663	.672	.661	.656	.580
30	2.250	2.250	.500	.659	.664	.673	.662	.657	.588
31	2.250	2.250	.500	.660	.665	.674	.663	.658	.596
32	2.250	2.250	.500	.661	.666	.675	.664	.659	.604
33	2.250	2.250	.500	.662	.667	.676	.665	.660	.612
34	2.250	2.250	.500	.663	.668	.677	.666	.661	.620
35	2.250	2.250	.500	.664	.669	.678	.667	.662	.628
36	2.250	2.250	.500	.665	.670	.679	.668	.663	.636
37	2.250	2.250	.500	.666	.671	.680	.669	.664	.644
38	2.250	2.250	.500	.667	.672	.681	.670	.665	.652
39	2.250	2.250	.500	.668	.673	.682	.671	.666	.660
40	2.250	2.250	.500	.669	.674	.683	.672	.667	.668
41	2.250	2.250	.500	.670	.675	.684	.673	.668	.676
42	2.250	2.250	.500	.671	.676	.685	.674	.669	.684
43	2.250	2.250	.500	.672	.677	.686	.675	.670	.692
44	2.250	2.250	.500	.673	.678	.687	.676	.671	.700
45	2.250	2.250	.500	.674	.679	.688	.677	.672	.708
46	2.250	2.250	.500	.675	.680	.689	.678	.673	.716
47	2.250	2.250	.500	.676	.681	.690	.679	.674	.724
48	2.250	2.250	.500	.677	.682	.691	.680	.675	.732
49	2.250	2.250	.500	.678	.683	.692	.681	.676	.740
50	2.250	2.250	.500	.679	.684	.693	.682	.677	.748
51	2.250	2.250	.500	.680	.685	.694	.683	.678	.756
52	2.250	2.250	.500	.681	.686	.695	.684	.679	.764
53	2.250	2.250	.500	.682	.687	.696	.685	.680	.772
54	2.250	2.250	.500	.683	.688	.697	.686	.681	.780
55	2.250	2.250	.500	.684	.689	.698	.687	.682	.788
56	2.250	2.250	.500	.685	.690	.699	.688	.683	.796
57	2.250	2.250	.500	.686	.691	.700	.689	.684	.804
58	2.250	2.250	.500	.687	.692	.701	.690	.685	.812
59	2.250	2.250	.500	.688	.693	.702	.691	.686	.820
60	2.250	2.250	.500	.689	.694	.703	.692	.687	.828
61	2.250	2.250	.500	.690	.695	.704	.693	.688	.836
62	2.250	2.250	.500	.691	.696	.705	.694	.689	.844
63	2.250	2.250	.500	.692	.697	.706	.695	.690	.852
64	2.250	2.250	.500	.693	.698	.707	.696	.691	.860

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2.950	.950	.950	2.359	2.351	2.521	6.596	6.500	6.053
2.950	.950	.950	2.127	2.133	2.177	1.190	1.131	1.034
2.950	.950	.950	2.122	2.127	2.251	2.301	2.137	2.004
2.950	.950	.950	2.055	2.047	2.127	3.271	3.117	2.660
2.950	.950	.950	2.042	2.057	2.113	5.071	3.090	3.577
2.950	.950	.950	2.007	2.070	2.400	4.726	4.512	4.156
2.950	.950	.950	2.003	2.075	2.076	5.235	5.033	4.615
2.950	.950	.950	1.265	1.130	.930	5.634	5.337	4.976
2.950	.950	.950	1.236	1.136	1.126	5.945	5.608	5.252
2.950	.950	.950	1.709	1.533	1.375	6.191	5.926	5.483
2.950	.950	.950	1.079	1.748	1.534	6.086	6.115	5.662
1.750	.950	.950	2.015	1.834	1.655	6.543	6.266	5.005
1.150	.950	.950	2.121	1.772	1.775	6.570	6.307	5.921
1.250	.950	.950	2.223	2.092	1.867	6.773	6.490	6.617
1.350	.950	.950	2.339	2.172	1.944	6.859	6.573	6.896
1.450	.950	.950	2.377	2.239	2.009	6.931	6.643	6.162
1.550	.950	.950	2.435	2.295	2.064	6.991	6.701	6.210
1.650	.950	.950	2.496	2.395	2.111	7.043	6.751	6.265
1.750	.950	.950	2.529	2.537	2.152	7.086	6.794	6.305
1.850	.950	.950	2.506	2.424	2.137	7.124	6.830	6.340
1.950	.950	.950	2.526	2.455	2.210	7.157	6.862	6.370
2.050	.950	.950	2.526	2.433	2.245	7.193	6.890	6.397
2.150	.950	.950	2.531	2.437	2.260	7.210	6.914	6.420
2.250	.950	.950	2.523	2.529	2.309	7.232	6.935	6.440
2.350	.950	.950	2.543	2.538	2.337	7.252	6.954	6.458
2.450	.950	.950	2.710	2.555	2.324	7.269	6.971	6.475
2.550	.950	.950	2.725	2.530	2.338	7.294	6.985	6.489
2.650	.950	.950	2.737	2.574	2.352	7.298	7.000	6.502
2.750	.950	.950	2.732	2.600	2.364	7.311	7.012	6.513
2.850	.950	.950	2.763	2.617	2.374	7.322	7.023	6.524
2.950	.950	.950	2.774	2.627	2.384	7.332	7.033	6.533
.950	.950	.950	2.075	2.085	2.100	1.210	1.169	1.079
.950	.950	.950	2.050	2.070	2.125	2.339	2.241	2.077
.950	.950	.950	2.047	2.046	2.017	3.308	3.170	2.940
.950	.950	.950	2.312	2.263	2.190	5.103	3.933	3.650
.950	.950	.950	2.576	2.513	2.422	5.736	4.542	4.218
.950	.950	.950	2.500	2.776	2.659	5.232	5.019	4.664
.950	.950	.950	1.463	1.613	1.697	5.620	5.392	5.013
.950	.950	.950	1.295	1.222	1.079	5.123	5.684	5.287
.950	.950	.950	1.476	1.431	1.273	6.152	5.915	5.504
.950	.950	.950	1.633	1.553	1.419	6.551	6.098	5.676
1.050	.950	.950	1.762	1.680	1.543	6.504	6.240	5.515
1.150	.950	.950	1.371	1.737	1.546	6.620	5.366	5.926
1.250	.950	.950	1.963	1.877	1.734	6.729	6.464	6.021
1.350	.950	.950	2.340	1.953	1.808	6.014	6.545	6.098
1.450	.950	.950	2.106	2.010	1.871	6.604	6.613	6.162
1.550	.950	.950	2.153	2.070	1.925	6.943	6.571	6.217
1.650	.950	.950	2.211	2.121	1.971	6.993	6.719	6.263
1.750	.950	.950	2.253	2.132	2.011	7.036	6.761	6.303
1.850	.950	.950	2.259	2.175	2.045	7.074	6.797	6.337
1.950	.950	.950	2.321	2.229	2.075	7.106	6.828	6.366
2.050	.950	.950	2.349	2.256	2.102	7.134	6.856	6.392
2.150	.950	.950	2.373	2.290	2.125	7.153	6.880	6.415
2.250	.950	.950	2.375	2.311	2.146	7.190	6.901	6.435
2.350	.950	.950	2.414	2.320	2.164	7.199	6.917	6.453
2.450	.950	.950	2.431	2.337	2.181	7.216	6.936	6.468
2.550	.950	.950	2.416	2.352	2.195	7.232	6.951	6.483
2.650	.950	.950	2.460	2.365	2.200	7.245	6.964	6.495
2.750	.950	.950	2.473	2.373	2.220	7.254	6.976	6.507
2.850	.950	.950	2.484	2.389	2.231	7.267	6.987	6.517

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3	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
5	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
7	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
9	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
11	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
13	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
15	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
17	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
19	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
21	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
23	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
25	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
27	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
29	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
31	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
33	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
35	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
37	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
39	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
41	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
43	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
45	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
47	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
49	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
51	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
53	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
55	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
57	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
59	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
61	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660
63	2.250	.750	.250	2.221	2.201	1.257	2.325	6.626	5.660

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1	1.250	1.350	1.450	1.550	1.650	1.750	1.850	1.950
2	1.251	1.351	1.451	1.551	1.651	1.751	1.851	1.951
3	1.252	1.352	1.452	1.552	1.652	1.752	1.852	1.952
4	1.253	1.353	1.453	1.553	1.653	1.753	1.853	1.953
5	1.254	1.354	1.454	1.554	1.654	1.754	1.854	1.954
6	1.255	1.355	1.455	1.555	1.655	1.755	1.855	1.955
7	1.256	1.356	1.456	1.556	1.656	1.756	1.856	1.956
8	1.257	1.357	1.457	1.557	1.657	1.757	1.857	1.957
9	1.258	1.358	1.458	1.558	1.658	1.758	1.858	1.958
10	1.259	1.359	1.459	1.559	1.659	1.759	1.859	1.959
11	1.260	1.360	1.460	1.560	1.660	1.760	1.860	1.960
12	1.261	1.361	1.461	1.561	1.661	1.761	1.861	1.961
13	1.262	1.362	1.462	1.562	1.662	1.762	1.862	1.962
14	1.263	1.363	1.463	1.563	1.663	1.763	1.863	1.963
15	1.264	1.364	1.464	1.564	1.664	1.764	1.864	1.964
16	1.265	1.365	1.465	1.565	1.665	1.765	1.865	1.965
17	1.266	1.366	1.466	1.566	1.666	1.766	1.866	1.966
18	1.267	1.367	1.467	1.567	1.667	1.767	1.867	1.967
19	1.268	1.368	1.468	1.568	1.668	1.768	1.868	1.968
20	1.269	1.369	1.469	1.569	1.669	1.769	1.869	1.969
21	1.270	1.370	1.470	1.570	1.670	1.770	1.870	1.970
22	1.271	1.371	1.471	1.571	1.671	1.771	1.871	1.971
23	1.272	1.372	1.472	1.572	1.672	1.772	1.872	1.972
24	1.273	1.373	1.473	1.573	1.673	1.773	1.873	1.973
25	1.274	1.374	1.474	1.574	1.674	1.774	1.874	1.974
26	1.275	1.375	1.475	1.575	1.675	1.775	1.875	1.975
27	1.276	1.376	1.476	1.576	1.676	1.776	1.876	1.976
28	1.277	1.377	1.477	1.577	1.677	1.777	1.877	1.977
29	1.278	1.378	1.478	1.578	1.678	1.778	1.878	1.978
30	1.279	1.379	1.479	1.579	1.679	1.779	1.879	1.979
31	1.280	1.380	1.480	1.580	1.680	1.780	1.880	1.980
32	1.281	1.381	1.481	1.581	1.681	1.781	1.881	1.981
33	1.282	1.382	1.482	1.582	1.682	1.782	1.882	1.982
34	1.283	1.383	1.483	1.583	1.683	1.783	1.883	1.983
35	1.284	1.384	1.484	1.584	1.684	1.784	1.884	1.984
36	1.285	1.385	1.485	1.585	1.685	1.785	1.885	1.985
37	1.286	1.386	1.486	1.586	1.686	1.786	1.886	1.986
38	1.287	1.387	1.487	1.587	1.687	1.787	1.887	1.987
39	1.288	1.388	1.488	1.588	1.688	1.788	1.888	1.988
40	1.289	1.389	1.489	1.589	1.689	1.789	1.889	1.989
41	1.290	1.390	1.490	1.590	1.690	1.790	1.890	1.990
42	1.291	1.391	1.491	1.591	1.691	1.791	1.891	1.991
43	1.292	1.392	1.492	1.592	1.692	1.792	1.892	1.992
44	1.293	1.393	1.493	1.593	1.693	1.793	1.893	1.993
45	1.294	1.394	1.494	1.594	1.694	1.794	1.894	1.994
46	1.295	1.395	1.495	1.595	1.695	1.795	1.895	1.995
47	1.296	1.396	1.496	1.596	1.696	1.796	1.896	1.996
48	1.297	1.397	1.497	1.597	1.697	1.797	1.897	1.997
49	1.298	1.398	1.498	1.598	1.698	1.798	1.898	1.998
50	1.299	1.399	1.499	1.599	1.699	1.799	1.899	1.999
51	1.300	1.400	1.500	1.600	1.700	1.800	1.900	2.000
52	1.301	1.401	1.501	1.601	1.701	1.801	1.901	2.001
53	1.302	1.402	1.502	1.602	1.702	1.802	1.902	2.002
54	1.303	1.403	1.503	1.603	1.703	1.803	1.903	2.003
55	1.304	1.404	1.504	1.604	1.704	1.804	1.904	2.004
56	1.305	1.405	1.505	1.605	1.705	1.805	1.905	2.005
57	1.306	1.406	1.506	1.606	1.706	1.806	1.906	2.006
58	1.307	1.407	1.507	1.607	1.707	1.807	1.907	2.007
59	1.308	1.408	1.508	1.608	1.708	1.808	1.908	2.008
60	1.309	1.409	1.509	1.609	1.709	1.809	1.909	2.009
61	1.310	1.410	1.510	1.610	1.710	1.810	1.910	2.010
62	1.311	1.411	1.511	1.611	1.711	1.811	1.911	2.011
63	1.312	1.412	1.512	1.612	1.712	1.812	1.912	2.012

2.750	1.750	.000	.753	.976	1.123	1.262	1.719	1.980	4
2.500	1.750	.000	.751	.974	1.121	1.262	1.719	1.980	5
2.250	1.750	.000	.750	.973	1.120	1.261	1.718	1.980	6
2.000	1.750	.000	.749	.972	1.119	1.261	1.717	1.980	7
1.750	1.750	.000	.748	.971	1.118	1.261	1.717	1.980	8
1.500	1.750	.000	.747	.970	1.117	1.260	1.716	1.980	9
1.250	1.750	.000	.746	.969	1.116	1.260	1.715	1.980	10
1.000	1.750	.000	.745	.968	1.115	1.260	1.714	1.980	11
.750	1.750	.000	.744	.967	1.114	1.259	1.713	1.980	12
.500	1.750	.000	.743	.966	1.113	1.259	1.712	1.980	13
.250	1.750	.000	.742	.965	1.112	1.258	1.711	1.980	14
.000	1.750	.000	.741	.964	1.111	1.258	1.710	1.980	15
1.000	1.750	.000	.740	.963	1.110	1.257	1.709	1.980	16
1.250	1.750	.000	.739	.962	1.109	1.257	1.708	1.980	17
1.500	1.750	.000	.738	.961	1.108	1.256	1.707	1.980	18
1.750	1.750	.000	.737	.960	1.107	1.256	1.706	1.980	19
2.000	1.750	.000	.736	.959	1.106	1.255	1.705	1.980	20
2.250	1.750	.000	.735	.958	1.105	1.255	1.704	1.980	21
2.500	1.750	.000	.734	.957	1.104	1.254	1.703	1.980	22
2.750	1.750	.000	.733	.956	1.103	1.254	1.702	1.980	23
3.000	1.750	.000	.732	.955	1.102	1.253	1.701	1.980	24
3.250	1.750	.000	.731	.954	1.101	1.253	1.700	1.980	25
3.500	1.750	.000	.730	.953	1.100	1.252	1.699	1.980	26
3.750	1.750	.000	.729	.952	1.099	1.252	1.698	1.980	27
4.000	1.750	.000	.728	.951	1.098	1.251	1.697	1.980	28
4.250	1.750	.000	.727	.950	1.097	1.251	1.696	1.980	29
4.500	1.750	.000	.726	.949	1.096	1.250	1.695	1.980	30
4.750	1.750	.000	.725	.948	1.095	1.250	1.694	1.980	31
5.000	1.750	.000	.724	.947	1.094	1.249	1.693	1.980	32
5.250	1.750	.000	.723	.946	1.093	1.249	1.692	1.980	33
5.500	1.750	.000	.722	.945	1.092	1.248	1.691	1.980	34
5.750	1.750	.000	.721	.944	1.091	1.248	1.690	1.980	35
6.000	1.750	.000	.720	.943	1.090	1.247	1.689	1.980	36
6.250	1.750	.000	.719	.942	1.089	1.247	1.688	1.980	37
6.500	1.750	.000	.718	.941	1.088	1.246	1.687	1.980	38
6.750	1.750	.000	.717	.940	1.087	1.246	1.686	1.980	39
7.000	1.750	.000	.716	.939	1.086	1.245	1.685	1.980	40
7.250	1.750	.000	.715	.938	1.085	1.245	1.684	1.980	41
7.500	1.750	.000	.714	.937	1.084	1.244	1.683	1.980	42
7.750	1.750	.000	.713	.936	1.083	1.244	1.682	1.980	43
8.000	1.750	.000	.712	.935	1.082	1.243	1.681	1.980	44
8.250	1.750	.000	.711	.934	1.081	1.243	1.680	1.980	45
8.500	1.750	.000	.710	.933	1.080	1.242	1.679	1.980	46
8.750	1.750	.000	.709	.932	1.079	1.242	1.678	1.980	47
9.000	1.750	.000	.708	.931	1.078	1.241	1.677	1.980	48
9.250	1.750	.000	.707	.930	1.077	1.241	1.676	1.980	49
9.500	1.750	.000	.706	.929	1.076	1.240	1.675	1.980	50
9.750	1.750	.000	.705	.928	1.075	1.240	1.674	1.980	51
10.000	1.750	.000	.704	.927	1.074	1.239	1.673	1.980	52
10.250	1.750	.000	.703	.926	1.073	1.239	1.672	1.980	53
10.500	1.750	.000	.702	.925	1.072	1.238	1.671	1.980	54
10.750	1.750	.000	.701	.924	1.071	1.238	1.670	1.980	55
11.000	1.750	.000	.700	.923	1.070	1.237	1.669	1.980	56
11.250	1.750	.000	.699	.922	1.069	1.237	1.668	1.980	57
11.500	1.750	.000	.698	.921	1.068	1.236	1.667	1.980	58
11.750	1.750	.000	.697	.920	1.067	1.236	1.666	1.980	59
12.000	1.750	.000	.696	.919	1.066	1.235	1.665	1.980	60
12.250	1.750	.000	.695	.918	1.065	1.235	1.664	1.980	61
12.500	1.750	.000	.694	.917	1.064	1.234	1.663	1.980	62
12.750	1.750	.000	.693	.916	1.063	1.234	1.662	1.980	63

3	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
5	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
7	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
9	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
11	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
13	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
15	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
17	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
19	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
21	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
23	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
25	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
27	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
29	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
31	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
33	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
35	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
37	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
39	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
41	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
43	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
45	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
47	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
49	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
51	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
53	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
55	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
57	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
59	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
61	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121
63	2.950	4.100	5.250	6.400	7.550	8.700	9.850	1.100	1.121

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1	2.74	2.74	2.74	2.74	2.74	2.74	2.74	2.74	2.74
2	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75	2.75
3	2.76	2.76	2.76	2.76	2.76	2.76	2.76	2.76	2.76
4	2.77	2.77	2.77	2.77	2.77	2.77	2.77	2.77	2.77
5	2.78	2.78	2.78	2.78	2.78	2.78	2.78	2.78	2.78
6	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79	2.79
7	2.80	2.80	2.80	2.80	2.80	2.80	2.80	2.80	2.80
8	2.81	2.81	2.81	2.81	2.81	2.81	2.81	2.81	2.81
9	2.82	2.82	2.82	2.82	2.82	2.82	2.82	2.82	2.82
10	2.83	2.83	2.83	2.83	2.83	2.83	2.83	2.83	2.83
11	2.84	2.84	2.84	2.84	2.84	2.84	2.84	2.84	2.84
12	2.85	2.85	2.85	2.85	2.85	2.85	2.85	2.85	2.85
13	2.86	2.86	2.86	2.86	2.86	2.86	2.86	2.86	2.86
14	2.87	2.87	2.87	2.87	2.87	2.87	2.87	2.87	2.87
15	2.88	2.88	2.88	2.88	2.88	2.88	2.88	2.88	2.88
16	2.89	2.89	2.89	2.89	2.89	2.89	2.89	2.89	2.89
17	2.90	2.90	2.90	2.90	2.90	2.90	2.90	2.90	2.90
18	2.91	2.91	2.91	2.91	2.91	2.91	2.91	2.91	2.91
19	2.92	2.92	2.92	2.92	2.92	2.92	2.92	2.92	2.92
20	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93	2.93
21	2.94	2.94	2.94	2.94	2.94	2.94	2.94	2.94	2.94
22	2.95	2.95	2.95	2.95	2.95	2.95	2.95	2.95	2.95
23	2.96	2.96	2.96	2.96	2.96	2.96	2.96	2.96	2.96
24	2.97	2.97	2.97	2.97	2.97	2.97	2.97	2.97	2.97
25	2.98	2.98	2.98	2.98	2.98	2.98	2.98	2.98	2.98
26	2.99	2.99	2.99	2.99	2.99	2.99	2.99	2.99	2.99
27	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00	3.00
28	3.01	3.01	3.01	3.01	3.01	3.01	3.01	3.01	3.01
29	3.02	3.02	3.02	3.02	3.02	3.02	3.02	3.02	3.02
30	3.03	3.03	3.03	3.03	3.03	3.03	3.03	3.03	3.03
31	3.04	3.04	3.04	3.04	3.04	3.04	3.04	3.04	3.04
32	3.05	3.05	3.05	3.05	3.05	3.05	3.05	3.05	3.05
33	3.06	3.06	3.06	3.06	3.06	3.06	3.06	3.06	3.06
34	3.07	3.07	3.07	3.07	3.07	3.07	3.07	3.07	3.07
35	3.08	3.08	3.08	3.08	3.08	3.08	3.08	3.08	3.08
36	3.09	3.09	3.09	3.09	3.09	3.09	3.09	3.09	3.09
37	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10	3.10
38	3.11	3.11	3.11	3.11	3.11	3.11	3.11	3.11	3.11
39	3.12	3.12	3.12	3.12	3.12	3.12	3.12	3.12	3.12
40	3.13	3.13	3.13	3.13	3.13	3.13	3.13	3.13	3.13
41	3.14	3.14	3.14	3.14	3.14	3.14	3.14	3.14	3.14
42	3.15	3.15	3.15	3.15	3.15	3.15	3.15	3.15	3.15
43	3.16	3.16	3.16	3.16	3.16	3.16	3.16	3.16	3.16
44	3.17	3.17	3.17	3.17	3.17	3.17	3.17	3.17	3.17
45	3.18	3.18	3.18	3.18	3.18	3.18	3.18	3.18	3.18
46	3.19	3.19	3.19	3.19	3.19	3.19	3.19	3.19	3.19
47	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20	3.20
48	3.21	3.21	3.21	3.21	3.21	3.21	3.21	3.21	3.21
49	3.22	3.22	3.22	3.22	3.22	3.22	3.22	3.22	3.22
50	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23	3.23
51	3.24	3.24	3.24	3.24	3.24	3.24	3.24	3.24	3.24
52	3.25	3.25	3.25	3.25	3.25	3.25	3.25	3.25	3.25
53	3.26	3.26	3.26	3.26	3.26	3.26	3.26	3.26	3.26
54	3.27	3.27	3.27	3.27	3.27	3.27	3.27	3.27	3.27
55	3.28	3.28	3.28	3.28	3.28	3.28	3.28	3.28	3.28
56	3.29	3.29	3.29	3.29	3.29	3.29	3.29	3.29	3.29
57	3.30	3.30	3.30	3.30	3.30	3.30	3.30	3.30	3.30
58	3.31	3.31	3.31	3.31	3.31	3.31	3.31	3.31	3.31
59	3.32	3.32	3.32	3.32	3.32	3.32	3.32	3.32	3.32
60	3.33	3.33	3.33	3.33	3.33	3.33	3.33	3.33	3.33
61	3.34	3.34	3.34	3.34	3.34	3.34	3.34	3.34	3.34
62	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35	3.35

UIC

3	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
5	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
7	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
9	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
11	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
13	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
15	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
17	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
19	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
21	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
23	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
25	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
27	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
29	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
31	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
33	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
35	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
37	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
39	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
41	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
43	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
45	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
47	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
49	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
51	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
53	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
55	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
57	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
59	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
61	2.750	2.750	.000	.355	.007	.715	.229	.510	.354
63	2.750	2.750	.000	.355	.007	.715	.229	.510	.354

UCT

[illegible]

3	2.050	.250	1.800	2.107	1.853	1.827	2.326	2.121	1.779
5	1.950	.250	1.700	-1.111	-1.107	-1.210	.039	-.024	-.072
7	1.850	.250	1.600	-2.227	-2.223	-2.332	.092	-.036	-.092
9	1.750	.250	1.500	-2.231	-2.233	-2.224	.156	.076	-.055
11	1.650	.250	1.400	-1.151	-1.233	-1.221	.221	.221	.033
13	1.550	.250	1.300	-1.115	-1.118	-1.296	.326	.408	.211
15	1.450	.250	1.200	-1.197	-1.196	-1.156	.737	.619	.395
17	1.350	.250	1.100	.387	.229	.009	.971	.826	.535
19	1.250	.250	1.000	.215	.414	.169	1.131	1.027	.775
21	1.150	.250	0.900	.722	.574	.326	1.373	1.211	.941
23	1.050	.250	0.800	.853	.729	.471	1.545	1.376	1.096
25	1.050	.250	1.000	1.026	.867	.602	1.676	1.522	1.233
27	1.150	.250	1.000	1.153	.990	.716	1.829	1.650	1.354
29	1.250	.250	1.000	1.265	1.078	.821	1.944	1.762	1.459
31	1.350	.250	1.100	1.362	1.173	.911	2.044	1.860	1.552
33	1.450	.250	1.000	1.441	1.275	.999	2.132	1.944	1.632
35	1.550	.250	1.000	1.523	1.347	1.069	2.206	2.019	1.703
37	1.650	.250	1.000	1.588	1.415	1.120	2.275	2.084	1.765
39	1.750	.250	1.000	1.646	1.469	1.174	2.333	2.141	1.819
41	1.850	.250	1.000	1.697	1.519	1.221	2.385	2.191	1.867
43	1.950	.250	1.000	1.742	1.563	1.253	2.431	2.235	1.909
45	2.050	.250	1.000	1.782	1.602	1.301	2.471	2.274	1.947
47	2.150	.250	1.000	1.818	1.636	1.334	2.507	2.309	1.980
49	2.250	.250	1.000	1.850	1.668	1.354	2.539	2.341	2.010
51	2.350	.250	1.000	1.878	1.695	1.370	2.568	2.369	2.037
53	2.450	.250	1.000	1.904	1.720	1.414	2.594	2.394	2.061
55	2.550	.250	1.000	1.927	1.743	1.436	2.617	2.416	2.083
57	2.650	.250	1.000	1.948	1.764	1.456	2.639	2.437	2.102
59	2.750	.250	1.000	1.967	1.782	1.473	2.657	2.456	2.120
61	2.850	.250	1.000	1.984	1.799	1.490	2.674	2.472	2.136
63	2.950	.250	1.000	2.002	1.814	1.514	2.690	2.488	2.151
65	3.050	.350	1.000	-1.124	-1.115	-1.164	.123	.096	.050
67	3.150	.350	1.000	-2.201	-2.205	-2.315	.272	.213	.130
69	3.250	.350	1.000	-2.267	-2.268	-2.375	.453	.301	.254
71	3.350	.350	1.000	-1.133	-1.219	-1.349	.679	.582	.420
73	3.450	.350	1.000	-1.005	-1.100	-1.260	.719	.805	.614
75	3.550	.350	1.000	.168	.050	-1.135	1.163	1.034	.820
77	3.650	.350	1.000	.135	.217	.021	1.371	1.257	1.023
79	3.750	.350	1.000	.511	.335	.175	1.614	1.465	1.215
81	3.850	.350	1.000	.675	.545	.324	1.810	1.652	1.389
83	3.950	.350	1.000	.831	.673	.463	1.900	1.819	1.545
85	4.050	.350	1.000	.969	.826	.598	2.135	1.966	1.683
87	4.150	.350	1.000	1.092	.945	.700	2.268	2.094	1.804
89	4.250	.350	1.000	1.200	1.050	.800	2.303	2.205	1.909
91	4.350	.350	1.000	1.294	1.142	.887	2.493	2.303	2.001
93	4.450	.350	1.000	1.373	1.223	.965	2.570	2.387	2.082
95	4.550	.350	1.000	1.451	1.274	1.033	2.646	2.461	2.152
97	4.650	.350	1.000	1.515	1.337	1.072	2.713	2.526	2.213
99	4.750	.350	1.000	1.572	1.412	1.115	2.771	2.582	2.267
101	4.850	.350	1.000	1.622	1.461	1.142	2.823	2.632	2.315
103	4.950	.350	1.000	1.667	1.514	1.234	2.868	2.676	2.357
105	5.050	.350	1.000	1.706	1.543	1.271	2.793	2.716	2.395
107	5.150	.350	1.000	1.741	1.577	1.304	2.744	2.750	2.420
109	5.250	.350	1.000	1.773	1.604	1.333	2.776	2.782	2.457
111	5.350	.350	1.000	1.811	1.616	1.350	3.005	2.809	2.484
113	5.450	.350	1.000	1.827	1.650	1.343	3.033	2.834	2.508
115	5.550	.350	1.000	1.850	1.643	1.405	3.053	2.857	2.530
117	5.650	.350	1.000	1.873	1.703	1.474	3.074	2.877	2.549
119	5.750	.350	1.000	1.889	1.722	1.482	3.093	2.896	2.567
121	5.850	.350	1.000	1.906	1.716	1.476	3.110	2.913	2.583

UCT

[illegible]

1	1.950	.650	1.327	1.727	1.600	1.347	3.197	3.709	3.195
5	1.750	.650	1.151	1.567	1.479	1.190	2.971	3.372	3.334
9	1.550	.650	1.000	1.400	1.313	1.073	2.731	3.135	3.063
13	1.350	.650	0.867	1.243	1.183	0.952	2.487	2.892	2.804
17	1.150	.650	0.750	1.100	1.077	0.841	2.247	2.652	2.554
21	0.950	.650	0.650	0.925	0.930	0.720	2.017	2.422	2.325
25	0.750	.650	0.567	0.800	0.822	0.610	1.793	2.198	2.100
29	0.550	.650	0.500	0.693	0.747	0.517	1.573	1.993	1.895
33	0.350	.650	0.433	0.600	0.656	0.430	1.357	1.767	1.669
37	0.150	.650	0.367	0.517	0.566	0.347	1.147	1.547	1.449
41	0.050	.650	0.300	0.433	0.476	0.260	0.937	1.327	1.229
45	0.000	.650	0.233	0.350	0.393	0.173	0.727	1.107	1.009
49	0.000	.650	0.167	0.267	0.310	0.087	0.517	0.887	0.789
53	0.000	.650	0.100	0.183	0.226	0.000	0.307	0.667	0.569
57	0.000	.650	0.033	0.100	0.143	0.000	0.097	0.457	0.369
61	0.000	.650	0.000	0.017	0.060	0.000	0.000	0.247	0.169
65	0.000	.650	0.000	0.000	0.000	0.000	0.000	0.000	0.000

UCT

1	2.750	.750	1.000	1.017	1.032	1.047	1.062	1.076	3.783
2	2.500	.500	1.000	1.013	1.028	1.043	1.058	1.073	3.791
3	2.250	.250	1.000	1.007	1.022	1.037	1.052	1.067	3.770
4	2.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
5	1.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
6	1.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
7	1.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
8	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
9	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
10	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
11	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
12	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
13	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
14	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
15	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
16	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
17	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
18	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
19	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
20	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
21	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
22	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
23	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
24	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
25	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
26	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
27	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
28	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
29	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
30	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
31	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
32	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
33	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
34	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
35	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
36	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
37	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
38	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
39	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
40	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
41	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
42	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
43	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
44	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
45	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
46	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
47	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
48	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
49	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
50	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
51	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
52	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
53	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
54	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
55	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
56	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
57	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
58	1.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750
59	.750	.750	1.000	1.000	1.015	1.030	1.045	1.060	3.750
60	.500	.500	1.000	1.000	1.015	1.030	1.045	1.060	3.750
61	.250	.250	1.000	1.000	1.015	1.030	1.045	1.060	3.750
62	.000	.000	1.000	1.000	1.015	1.030	1.045	1.060	3.750

3	2.750	1.750	1.750	1.323	1.271	1.170	4.153	4.025	3.754
5	1.750	1.750	1.750	1.319	1.017	1.022	4.119	4.002	3.749
7	1.750	1.750	1.750	1.323	1.026	1.035	4.225	4.222	3.737
9	1.750	1.750	1.750	1.311	1.017	1.032	4.213	4.162	3.731
11	1.750	1.750	1.750	1.323	1.019	1.037	4.265	4.233	3.733
13	1.750	1.750	1.750	1.310	1.034	1.032	4.286	4.211	3.685
15	1.750	1.750	1.750	1.323	1.115	1.049	4.172	4.085	3.740
17	1.750	1.750	1.750	1.299	1.130	1.158	4.423	4.326	3.765
19	1.750	1.750	1.750	1.299	1.264	1.233	4.441	4.236	3.761
21	1.750	1.750	1.750	1.264	1.345	1.310	4.231	4.218	3.531
23	1.750	1.750	1.750	1.417	1.425	1.388	4.224	4.276	3.676
25	1.750	1.750	1.750	1.525	1.532	1.467	4.136	4.012	3.605
27	1.750	1.750	1.750	1.592	1.574	1.533	4.258	4.122	3.915
29	1.750	1.750	1.750	1.568	1.642	1.599	4.361	4.231	3.610
31	1.750	1.750	1.750	1.732	1.745	1.693	4.355	4.319	3.692
33	1.750	1.750	1.750	1.700	1.762	1.716	4.335	4.396	3.764
35	1.750	1.750	1.750	1.813	1.814	1.767	4.379	4.463	3.727
37	1.750	1.750	1.750	1.891	1.852	1.813	4.355	4.522	3.782
39	1.750	1.750	1.750	1.935	1.935	1.853	4.712	4.573	3.731
41	1.750	1.750	1.750	1.974	1.974	1.893	4.756	4.619	3.774
43	1.750	1.750	1.750	1.910	1.974	1.926	4.638	4.659	3.712
45	2.050	1.750	1.750	1.943	1.911	1.959	4.445	4.695	3.745
47	2.150	1.750	1.750	1.972	1.949	1.947	4.479	4.727	3.775
49	2.250	1.750	1.750	1.979	1.967	1.913	4.708	4.756	3.502
51	2.350	1.750	1.750	1.923	1.971	1.936	4.735	4.782	3.527
53	2.450	1.750	1.750	1.915	1.913	1.959	4.759	4.805	3.548
55	2.550	1.750	1.750	1.966	1.933	1.977	4.780	4.826	3.566
57	2.650	1.750	1.750	1.984	1.951	1.995	4.800	4.845	3.586
59	2.750	1.750	1.750	1.961	1.989	1.911	4.818	4.862	3.602
61	2.850	1.750	1.750	1.917	1.933	1.926	4.834	4.878	3.617
63	2.950	1.750	1.750	1.931	1.927	1.940	4.849	4.892	3.631
65	1.750	1.750	1.750	1.927	1.938	1.910	4.893	4.977	3.651
67	1.750	1.750	1.750	1.967	1.965	1.914	4.775	4.744	3.693
69	1.750	1.750	1.750	1.968	1.914	1.905	4.137	4.092	3.617
71	1.750	1.750	1.750	1.931	1.921	1.919	4.472	4.414	3.617
73	1.750	1.750	1.750	1.976	1.959	1.950	4.776	4.706	3.589
75	1.750	1.750	1.750	1.931	1.923	1.919	4.243	4.267	3.632
77	1.750	1.750	1.750	1.995	1.936	1.971	4.287	4.197	3.646
79	1.750	1.750	1.750	1.965	1.955	1.938	4.497	4.398	3.633
81	1.750	1.750	1.750	1.938	1.927	1.908	4.679	4.573	3.646
83	1.750	1.750	1.750	1.911	1.990	1.973	4.337	4.724	3.538
85	1.750	1.750	1.750	1.991	1.960	1.947	4.773	4.856	3.660
87	1.750	1.750	1.750	1.949	1.935	1.912	4.692	4.669	3.766
89	1.750	1.750	1.750	1.912	1.997	1.973	4.194	4.064	3.658
91	1.750	1.750	1.750	1.971	1.956	1.930	4.283	4.154	3.636
93	1.750	1.750	1.750	1.925	1.909	1.933	4.361	4.229	3.608
95	1.750	1.750	1.750	1.778	1.750	1.731	4.429	4.294	3.669
97	1.750	1.750	1.750	1.820	1.803	1.775	4.483	4.351	3.623
99	1.750	1.750	1.750	1.852	1.844	1.815	4.541	4.402	3.670
101	1.750	1.750	1.750	1.930	1.932	1.951	4.587	4.446	3.612
103	1.750	1.750	1.750	1.934	1.915	1.905	4.628	4.486	3.649
105	2.050	1.750	1.750	1.965	1.916	1.915	4.365	4.521	3.682
107	2.150	1.750	1.750	1.994	1.974	1.942	4.697	4.552	3.611
109	2.250	1.750	1.750	1.920	1.900	1.967	4.726	4.581	3.637
111	2.350	1.750	1.750	1.993	1.923	1.970	4.753	4.606	3.661
113	2.450	1.750	1.750	1.965	1.965	1.911	4.774	4.629	3.643
115	2.550	1.750	1.750	1.985	1.964	1.936	4.797	4.647	3.602
117	2.650	1.750	1.750	1.903	1.982	1.948	4.817	4.668	3.619
119	2.750	1.750	1.750	1.917	1.998	1.954	4.839	4.685	3.635
121	2.850	1.750	1.750	1.935	1.914	1.975	4.850	4.700	3.650

UCT

2	2.250	1.150	1.000	1.149	1.127	1.072	3.463	3.463	
3	2.250	1.200	1.000	1.001	1.001	1.001	3.319	3.325	
4	2.250	1.250	1.000	1.000	1.000	1.000	3.241	3.241	
5	2.250	1.300	1.000	1.000	1.000	1.000	3.191	3.191	
6	2.250	1.350	1.000	1.000	1.000	1.000	3.155	3.155	
7	2.250	1.400	1.000	1.000	1.000	1.000	3.121	3.121	
8	2.250	1.450	1.000	1.000	1.000	1.000	3.089	3.089	
9	2.250	1.500	1.000	1.000	1.000	1.000	3.059	3.059	
10	2.250	1.550	1.000	1.000	1.000	1.000	3.031	3.031	
11	2.250	1.600	1.000	1.000	1.000	1.000	3.004	3.004	
12	2.250	1.650	1.000	1.000	1.000	1.000	2.979	2.979	
13	2.250	1.700	1.000	1.000	1.000	1.000	2.955	2.955	
14	2.250	1.750	1.000	1.000	1.000	1.000	2.932	2.932	
15	2.250	1.800	1.000	1.000	1.000	1.000	2.910	2.910	
16	2.250	1.850	1.000	1.000	1.000	1.000	2.889	2.889	
17	2.250	1.900	1.000	1.000	1.000	1.000	2.869	2.869	
18	2.250	1.950	1.000	1.000	1.000	1.000	2.849	2.849	
19	2.250	2.000	1.000	1.000	1.000	1.000	2.830	2.830	
20	2.250	2.050	1.000	1.000	1.000	1.000	2.811	2.811	
21	2.250	2.100	1.000	1.000	1.000	1.000	2.792	2.792	
22	2.250	2.150	1.000	1.000	1.000	1.000	2.774	2.774	
23	2.250	2.200	1.000	1.000	1.000	1.000	2.756	2.756	
24	2.250	2.250	1.000	1.000	1.000	1.000	2.739	2.739	
25	2.250	2.300	1.000	1.000	1.000	1.000	2.722	2.722	
26	2.250	2.350	1.000	1.000	1.000	1.000	2.705	2.705	
27	2.250	2.400	1.000	1.000	1.000	1.000	2.689	2.689	
28	2.250	2.450	1.000	1.000	1.000	1.000	2.672	2.672	
29	2.250	2.500	1.000	1.000	1.000	1.000	2.656	2.656	
30	2.250	2.550	1.000	1.000	1.000	1.000	2.640	2.640	
31	2.250	2.600	1.000	1.000	1.000	1.000	2.624	2.624	
32	2.250	2.650	1.000	1.000	1.000	1.000	2.608	2.608	
33	2.250	2.700	1.000	1.000	1.000	1.000	2.592	2.592	
34	2.250	2.750	1.000	1.000	1.000	1.000	2.576	2.576	
35	2.250	2.800	1.000	1.000	1.000	1.000	2.560	2.560	
36	2.250	2.850	1.000	1.000	1.000	1.000	2.544	2.544	
37	2.250	2.900	1.000	1.000	1.000	1.000	2.528	2.528	
38	2.250	2.950	1.000	1.000	1.000	1.000	2.512	2.512	
39	2.250	3.000	1.000	1.000	1.000	1.000	2.496	2.496	
40	2.250	3.050	1.000	1.000	1.000	1.000	2.480	2.480	
41	2.250	3.100	1.000	1.000	1.000	1.000	2.464	2.464	
42	2.250	3.150	1.000	1.000	1.000	1.000	2.448	2.448	
43	2.250	3.200	1.000	1.000	1.000	1.000	2.432	2.432	
44	2.250	3.250	1.000	1.000	1.000	1.000	2.416	2.416	
45	2.250	3.300	1.000	1.000	1.000	1.000	2.400	2.400	
46	2.250	3.350	1.000	1.000	1.000	1.000	2.384	2.384	
47	2.250	3.400	1.000	1.000	1.000	1.000	2.368	2.368	
48	2.250	3.450	1.000	1.000	1.000	1.000	2.352	2.352	
49	2.250	3.500	1.000	1.000	1.000	1.000	2.336	2.336	
50	2.250	3.550	1.000	1.000	1.000	1.000	2.320	2.320	
51	2.250	3.600	1.000	1.000	1.000	1.000	2.304	2.304	
52	2.250	3.650	1.000	1.000	1.000	1.000	2.288	2.288	
53	2.250	3.700	1.000	1.000	1.000	1.000	2.272	2.272	
54	2.250	3.750	1.000	1.000	1.000	1.000	2.256	2.256	
55	2.250	3.800	1.000	1.000	1.000	1.000	2.240	2.240	
56	2.250	3.850	1.000	1.000	1.000	1.000	2.224	2.224	
57	2.250	3.900	1.000	1.000	1.000	1.000	2.208	2.208	
58	2.250	3.950	1.000	1.000	1.000	1.000	2.192	2.192	
59	2.250	4.000	1.000	1.000	1.000	1.000	2.176	2.176	
60	2.250	4.050	1.000	1.000	1.000	1.000	2.160	2.160	

5	.050	1.750	1.000	.700	.000	.000	2.250	2.450	2.250
	.150	1.750	1.000	.700	.000	.000	.250	.150	.170
	.250	1.750	1.000	.700	.000	.000	.250	.370	.340
7	.350	1.750	1.000	.700	.000	.000	.250	.500	.500
	.450	1.750	1.000	.700	.000	.000	.250	.720	.560
9	.550	1.750	1.000	.700	.000	.000	.250	.940	.800
	.650	1.750	1.000	.700	.000	.000	.250	1.160	.990
11	.750	1.750	1.000	.700	.000	.000	.250	1.380	1.160
	.850	1.750	1.000	.700	.000	.000	.250	1.600	1.380
13	.950	1.750	1.000	.700	.000	.000	.250	1.820	1.590
	1.050	1.750	1.000	.700	.000	.000	.250	2.040	1.870
15	1.150	1.750	1.000	.700	.000	.000	.250	2.260	2.150
	1.250	1.750	1.000	.700	.000	.000	.250	2.480	2.430
17	1.350	1.750	1.000	.700	.000	.000	.250	2.700	2.710
	1.450	1.750	1.000	.700	.000	.000	.250	2.920	2.990
19	1.550	1.750	1.000	.700	.000	.000	.250	3.140	3.270
	1.650	1.750	1.000	.700	.000	.000	.250	3.360	3.550
21	1.750	1.750	1.000	.700	.000	.000	.250	3.580	3.830
	1.850	1.750	1.000	.700	.000	.000	.250	3.800	4.110
23	1.950	1.750	1.000	.700	.000	.000	.250	4.020	4.390
	2.050	1.750	1.000	.700	.000	.000	.250	4.240	4.670
25	2.150	1.750	1.000	.700	.000	.000	.250	4.460	4.950
	2.250	1.750	1.000	.700	.000	.000	.250	4.680	5.230
27	2.350	1.750	1.000	.700	.000	.000	.250	4.900	5.510
	2.450	1.750	1.000	.700	.000	.000	.250	5.120	5.790
29	2.550	1.750	1.000	.700	.000	.000	.250	5.340	6.070
	2.650	1.750	1.000	.700	.000	.000	.250	5.560	6.350
31	2.750	1.750	1.000	.700	.000	.000	.250	5.780	6.630
	2.850	1.750	1.000	.700	.000	.000	.250	6.000	6.910
33	2.950	1.750	1.000	.700	.000	.000	.250	6.220	7.190
	3.050	1.750	1.000	.700	.000	.000	.250	6.440	7.470
35	3.150	1.750	1.000	.700	.000	.000	.250	6.660	7.750
	3.250	1.750	1.000	.700	.000	.000	.250	6.880	8.030
37	3.350	1.750	1.000	.700	.000	.000	.250	7.100	8.310
	3.450	1.750	1.000	.700	.000	.000	.250	7.320	8.590
39	3.550	1.750	1.000	.700	.000	.000	.250	7.540	8.870
	3.650	1.750	1.000	.700	.000	.000	.250	7.760	9.150
41	3.750	1.750	1.000	.700	.000	.000	.250	7.980	9.430
	3.850	1.750	1.000	.700	.000	.000	.250	8.200	9.710
43	3.950	1.750	1.000	.700	.000	.000	.250	8.420	9.990
	4.050	1.750	1.000	.700	.000	.000	.250	8.640	10.270
45	4.150	1.750	1.000	.700	.000	.000	.250	8.860	10.550
	4.250	1.750	1.000	.700	.000	.000	.250	9.080	10.830
47	4.350	1.750	1.000	.700	.000	.000	.250	9.300	11.110
	4.450	1.750	1.000	.700	.000	.000	.250	9.520	11.390
49	4.550	1.750	1.000	.700	.000	.000	.250	9.740	11.670
	4.650	1.750	1.000	.700	.000	.000	.250	9.960	11.950
51	4.750	1.750	1.000	.700	.000	.000	.250	10.180	12.230
	4.850	1.750	1.000	.700	.000	.000	.250	10.400	12.510
53	4.950	1.750	1.000	.700	.000	.000	.250	10.620	12.790
	5.050	1.750	1.000	.700	.000	.000	.250	10.840	13.070
55	5.150	1.750	1.000	.700	.000	.000	.250	11.060	13.350
	5.250	1.750	1.000	.700	.000	.000	.250	11.280	13.630
57	5.350	1.750	1.000	.700	.000	.000	.250	11.500	13.910
	5.450	1.750	1.000	.700	.000	.000	.250	11.720	14.190
59	5.550	1.750	1.000	.700	.000	.000	.250	11.940	14.470
	5.650	1.750	1.000	.700	.000	.000	.250	12.160	14.750
61	5.750	1.750	1.000	.700	.000	.000	.250	12.380	15.030
	5.850	1.750	1.000	.700	.000	.000	.250	12.600	15.310
63	5.950	1.750	1.000	.700	.000	.000	.250	12.820	15.590
	6.050	1.750	1.000	.700	.000	.000	.250	13.040	15.870

UCT

1	2.950	1.970	1.970	.950	.727	.750	2.132	2.072	1.386
3	.950	2.990	1.970	.917	.620	.725	2.155	.150	.137
5	.150	2.990	1.970	.917	.619	.725	2.155	.299	.272
7	.250	2.990	1.970	.933	.682	.676	2.166	.443	.403
9	.350	2.990	1.970	.971	.765	.609	2.112	.581	.529
11	.450	2.990	1.970	.998	.819	.534	2.049	.711	.640
13	.550	2.990	1.970	.981	.837	.464	2.078	.833	.758
15	.650	2.990	1.970	.947	.854	.397	2.097	.946	.861
17	.750	2.990	1.970	.875	.876	.330	2.106	1.049	.955
19	.850	2.990	1.970	.805	.827	.264	2.206	1.144	1.041
21	.950	2.990	1.970	.739	.858	.208	2.296	1.229	1.118
23	1.050	2.990	1.970	.675	.890	.152	2.378	1.307	1.188
25	1.150	2.990	1.970	.613	.921	.096	2.451	1.376	1.251
27	1.250	2.990	1.970	.551	.957	.040	2.517	1.439	1.307
29	1.350	2.990	1.970	.490	.982	.000	2.577	1.495	1.358
31	1.450	2.990	1.970	.429	.991	.000	2.630	1.545	1.403
33	1.550	2.990	1.970	.368	.987	.000	2.677	1.590	1.444
35	1.650	2.990	1.970	.307	.971	.000	2.720	1.630	1.480
37	1.750	2.990	1.970	.246	.942	.000	2.759	1.666	1.513
39	1.850	2.990	1.970	.185	.899	.000	2.793	1.699	1.542
41	1.950	2.990	1.970	.124	.853	.000	2.824	1.729	1.567
43	2.050	2.990	1.970	.063	.804	.000	2.852	1.755	1.593
45	2.150	2.990	1.970	.002	.753	.000	2.878	1.779	1.615
47	2.250	2.990	1.970	.001	.701	.000	2.901	1.801	1.634
49	2.350	2.990	1.970	.000	.649	.000	2.922	1.821	1.652
51	2.450	2.990	1.970	.000	.597	.000	2.941	1.839	1.668
53	2.550	2.990	1.970	.000	.545	.000	2.958	1.855	1.683
55	2.650	2.990	1.970	.000	.493	.000	2.974	1.870	1.697
57	2.750	2.990	1.970	.000	.441	.000	2.989	1.884	1.709
59	2.850	2.990	1.970	.000	.389	.000	2.992	1.896	1.721
61	2.950	2.990	1.970	.000	.337	.000	2.994	1.908	1.731
63	.950	2.150	1.970	.017	.320	.025	2.142	.135	.122
65	.150	2.150	1.970	.035	.301	.051	2.092	.268	.243
67	.250	2.150	1.970	.053	.282	.077	2.049	.397	.360
69	.350	2.150	1.970	.073	.265	.104	2.010	.521	.473
71	.450	2.150	1.970	.095	.249	.133	1.975	.639	.579
73	.550	2.150	1.970	.114	.235	.163	1.942	.750	.679
75	.650	2.150	1.970	.133	.222	.193	1.900	.852	.772
77	.750	2.150	1.970	.159	.210	.225	1.859	.947	.858
79	.850	2.150	1.970	.176	.219	.257	1.813	1.034	.937
81	.950	2.150	1.970	.229	.238	.289	1.770	1.113	1.008
83	1.050	2.150	1.970	.252	.273	.321	1.723	1.185	1.073
85	1.150	2.150	1.970	.280	.307	.353	1.671	1.250	1.131
87	1.250	2.150	1.970	.307	.336	.384	1.613	1.308	1.183
89	1.350	2.150	1.970	.334	.364	.413	1.549	1.361	1.231
91	1.450	2.150	1.970	.360	.391	.442	1.489	1.408	1.273
93	1.550	2.150	1.970	.385	.417	.469	1.535	1.451	1.312
95	1.650	2.150	1.970	.410	.442	.496	1.575	1.489	1.346
97	1.750	2.150	1.970	.433	.465	.520	1.612	1.524	1.377
99	1.850	2.150	1.970	.454	.488	.544	1.645	1.555	1.405
101	1.950	2.150	1.970	.475	.509	.566	1.675	1.583	1.430
103	2.050	2.150	1.970	.495	.529	.586	1.702	1.609	1.453
105	2.150	2.150	1.970	.513	.548	.606	1.727	1.632	1.474
107	2.250	2.150	1.970	.530	.565	.624	1.749	1.653	1.493
109	2.350	2.150	1.970	.547	.582	.641	1.767	1.672	1.510
111	2.450	2.150	1.970	.562	.597	.657	1.780	1.689	1.526
113	2.550	2.150	1.970	.576	.612	.671	1.804	1.705	1.540
115	2.650	2.150	1.970	.589	.625	.685	1.820	1.720	1.553
117	2.750	2.150	1.970	.602	.638	.698	1.837	1.734	1.565

1	2.950	2.350	1.000	.584	.673	.669	1.369	1.489	1.330
5	2.950	2.450	1.000	.617	.628	.625	1.393	.677	.687
	2.950	2.550	1.000	.651	.619	.631	1.416	.693	.673
	2.950	2.650	1.000	.682	.631	.645	1.439	.707	.657
	2.950	2.750	1.000	.713	.642	.661	1.462	.721	.638
	2.950	2.850	1.000	.744	.653	.675	1.485	.735	.615
	2.950	2.950	1.000	.775	.664	.689	1.508	.749	.589
11	2.950	2.950	1.000	.806	.675	.703	1.531	.763	.550
	2.950	2.950	1.000	.837	.686	.717	1.554	.777	.523
13	2.950	2.950	1.000	.868	.697	.731	1.577	.791	.482
	2.950	2.950	1.000	.899	.708	.745	1.600	.805	.437
15	2.950	2.950	1.000	.930	.719	.759	1.623	.819	.388
	2.950	2.950	1.000	.961	.730	.773	1.646	.833	.333
17	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.278
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.223
19	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.168
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.113
21	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.058
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
23	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
25	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
27	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
29	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
31	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
33	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
35	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
37	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
39	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
41	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
43	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
45	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
47	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
	2.950	2.950	1.000	.992	.741	.787	1.669	.847	.003
49	2.950</								

3	2.750	2.750	1.000	.167	.510	.530	1.155	1.073	.935
5	2.750	2.750	1.000	.313	.510	.523	.869	.834	.856
7	2.750	2.750	1.000	.459	.510	.516	.737	.727	.711
9	2.750	2.750	1.000	.606	.510	.509	.628	.619	.615
11	2.750	2.750	1.000	.753	.510	.502	.520	.520	.518
13	2.750	2.750	1.000	.900	.510	.499	.433	.439	.429
15	2.750	2.750	1.000	.977	.510	.497	.393	.365	.316
17	2.750	2.750	1.000	.114	.132	.163	.451	.419	.364
19	2.750	2.750	1.000	.132	.152	.186	.505	.467	.408
21	2.750	2.750	1.000	.156	.172	.209	.557	.517	.449
23	2.750	2.750	1.000	.157	.172	.232	.605	.561	.488
25	2.750	2.750	1.000	.160	.211	.255	.650	.603	.524
27	2.750	2.750	1.000	.203	.231	.277	.692	.642	.557
29	2.750	2.750	1.000	.221	.250	.299	.731	.677	.586
31	2.750	2.750	1.000	.233	.259	.320	.767	.710	.616
33	2.750	2.750	1.000	.255	.257	.341	.799	.741	.643
35	2.750	2.750	1.000	.272	.315	.361	.830	.769	.667
37	2.750	2.750	1.000	.289	.323	.380	.858	.794	.689
39	2.750	2.750	1.000	.306	.337	.398	.883	.818	.709
41	2.750	2.750	1.000	.317	.350	.416	.907	.840	.720
43	2.750	2.750	1.000	.321	.371	.433	.924	.859	.745
45	2.750	2.750	1.000	.343	.386	.449	.948	.878	.760
47	2.750	2.750	1.000	.361	.400	.464	.967	.895	.775
49	2.750	2.750	1.000	.374	.413	.479	.983	.910	.788
51	2.750	2.750	1.000	.387	.426	.492	.999	.924	.800
53	2.750	2.750	1.000	.396	.434	.505	1.013	.938	.812
55	2.750	2.750	1.000	.409	.459	.518	1.026	.950	.822
57	2.750	2.750	1.000	.421	.451	.529	1.034	.961	.832
59	2.750	2.750	1.000	.430	.471	.540	1.051	.971	.841
61	2.750	2.750	1.000	.437	.481	.551	1.060	.981	.849
63	2.750	2.750	1.000	.448	.490	.561	1.071	.990	.856
65	2.750	2.750	1.000	.012	.013	.022	.062	.055	.050
67	2.750	2.750	1.000	.031	.036	.045	.124	.115	.100
69	2.750	2.750	1.000	.046	.054	.067	.185	.171	.146
71	2.750	2.750	1.000	.052	.072	.075	.245	.226	.196
73	2.750	2.750	1.000	.073	.071	.113	.302	.280	.242
75	2.750	2.750	1.000	.094	.110	.135	.350	.331	.286
77	2.750	2.750	1.000	.111	.120	.150	.410	.380	.328
79	2.750	2.750	1.000	.127	.147	.180	.461	.426	.368
81	2.750	2.750	1.000	.144	.166	.203	.500	.470	.405
83	2.750	2.750	1.000	.161	.185	.225	.553	.511	.441
85	2.750	2.750	1.000	.178	.204	.247	.594	.549	.474
87	2.750	2.750	1.000	.195	.222	.268	.633	.585	.504
89	2.750	2.750	1.000	.212	.241	.289	.669	.618	.533
91	2.750	2.750	1.000	.229	.259	.309	.702	.649	.559
93	2.750	2.750	1.000	.245	.276	.329	.733	.677	.583
95	2.750	2.750	1.000	.261	.293	.349	.762	.703	.605
97	2.750	2.750	1.000	.278	.310	.367	.786	.727	.626
99	2.750	2.750	1.000	.291	.326	.384	.812	.750	.645
101	2.750	2.750	1.000	.305	.342	.401	.835	.770	.662
103	2.750	2.750	1.000	.319	.356	.418	.855	.789	.678
105	2.750	2.750	1.000	.333	.371	.433	.874	.806	.693
107	2.750	2.750	1.000	.345	.384	.446	.891	.822	.707
109	2.750	2.750	1.000	.358	.397	.462	.909	.837	.719
111	2.750	2.750	1.000	.370	.410	.475	.922	.851	.731
113	2.750	2.750	1.000	.381	.421	.488	.936	.863	.742
115	2.750	2.750	1.000	.390	.432	.500	.949	.875	.752
117	2.750	2.750	1.000	.400	.443	.511	.960	.886	.761

1	2.750	.150	2.750	.751	.856	.993	.795	.700	.540
2	2.750	.200	2.750	.791	.910	.990	.793	.699	.550
3	2.750	.250	2.750	.831	.971	.985	.792	.671	.546
4	2.750	.300	2.750	.871	.107	.982	.791	.640	.534
5	2.750	.350	2.750	.911	.121	.982	.790	.614	.522
6	2.750	.400	2.750	.951	.135	.982	.789	.588	.510
7	2.750	.450	2.750	.991	.149	.982	.788	.562	.498
8	2.750	.500	2.750	1.031	.163	.982	.787	.536	.486
9	2.750	.550	2.750	1.071	.177	.982	.786	.510	.474
10	2.750	.600	2.750	1.111	.191	.982	.785	.484	.462
11	2.750	.650	2.750	1.151	.205	.982	.784	.458	.450
12	2.750	.700	2.750	1.191	.219	.982	.783	.432	.438
13	2.750	.750	2.750	1.231	.233	.982	.782	.406	.426
14	2.750	.800	2.750	1.271	.247	.982	.781	.380	.414
15	2.750	.850	2.750	1.311	.261	.982	.780	.354	.402
16	2.750	.900	2.750	1.351	.275	.982	.779	.328	.390
17	2.750	.950	2.750	1.391	.289	.982	.778	.302	.378
18	2.750	1.000	2.750	1.431	.303	.982	.777	.276	.366
19	2.750	1.050	2.750	1.471	.317	.982	.776	.250	.354
20	2.750	1.100	2.750	1.511	.331	.982	.775	.224	.342
21	2.750	1.150	2.750	1.551	.345	.982	.774	.198	.330
22	2.750	1.200	2.750	1.591	.359	.982	.773	.172	.318
23	2.750	1.250	2.750	1.631	.373	.982	.772	.146	.306
24	2.750	1.300	2.750	1.671	.387	.982	.771	.120	.294
25	2.750	1.350	2.750	1.711	.401	.982	.770	.094	.282
26	2.750	1.400	2.750	1.751	.415	.982	.769	.068	.270
27	2.750	1.450	2.750	1.791	.429	.982	.768	.042	.258
28	2.750	1.500	2.750	1.831	.443	.982	.767	.016	.246
29	2.750	1.550	2.750	1.871	.457	.982	.766	-.010	.234
30	2.750	1.600	2.750	1.911	.471	.982	.765	-.034	.222
31	2.750	1.650	2.750	1.951	.485	.982	.764	-.058	.210
32	2.750	1.700	2.750	1.991	.499	.982	.763	-.082	.198
33	2.750	1.750	2.750	2.031	.513	.982	.762	-.106	.186
34	2.750	1.800	2.750	2.071	.527	.982	.761	-.130	.174
35	2.750	1.850	2.750	2.111	.541	.982	.760	-.154	.162
36	2.750	1.900	2.750	2.151	.555	.982	.759	-.178	.150
37	2.750	1.950	2.750	2.191	.569	.982	.758	-.202	.138
38	2.750	2.000	2.750	2.231	.583	.982	.757	-.226	.126
39	2.750	2.050	2.750	2.271	.597	.982	.756	-.250	.114
40	2.750	2.100	2.750	2.311	.611	.982	.755	-.274	.102
41	2.750	2.150	2.750	2.351	.625	.982	.754	-.298	.090
42	2.750	2.200	2.750	2.391	.639	.982	.753	-.322	.078
43	2.750	2.250	2.750	2.431	.653	.982	.752	-.346	.066
44	2.750	2.300	2.750	2.471	.667	.982	.751	-.370	.054
45	2.750	2.350	2.750	2.511	.681	.982	.750	-.394	.042
46	2.750	2.400	2.750	2.551	.695	.982	.749	-.418	.030
47	2.750	2.450	2.750	2.591	.709	.982	.748	-.442	.018
48	2.750	2.500	2.750	2.631	.723	.982	.747	-.466	.006
49	2.750	2.550	2.750	2.671	.737	.982	.746	-.490	-.006
50	2.750	2.600	2.750	2.711	.751	.982	.745	-.514	-.018
51	2.750	2.650	2.750	2.751	.765	.982	.744	-.538	-.030
52	2.750	2.700	2.750	2.791	.779	.982	.743	-.562	-.042
53	2.750	2.750	2.750	2.831	.793	.982	.742	-.586	-.054
54	2.750	2.800	2.750	2.871	.807	.982	.741	-.610	-.066
55	2.750	2.850	2.750	2.911	.821	.982	.740	-.634	-.078
56	2.750	2.900	2.750	2.951	.835	.982	.739	-.658	-.090
57	2.750	2.950	2.750	2.991	.849	.982	.738	-.682	-.102
58	2.750	3.000	2.750	3.031	.863	.982	.737	-.706	-.114
59	2.750	3.050	2.750	3.071	.877	.982	.736	-.730	-.126
60	2.750	3.100	2.750	3.111	.891	.982	.735	-.754	-.138

1	1.250	.450	2.000	-.000	-.000	-.000	-.000	-.000	-.000
3	1.250	.450	2.000	-.007	-.003	-.007	-.003	-.007	-.003
5	1.250	.450	2.000	-.014	-.006	-.014	-.006	-.014	-.006
7	1.250	.450	2.000	-.021	-.013	-.021	-.013	-.021	-.013
9	1.250	.450	2.000	-.028	-.020	-.028	-.020	-.028	-.020
11	1.250	.450	2.000	-.035	-.027	-.035	-.027	-.035	-.027
13	1.250	.450	2.000	-.042	-.034	-.042	-.034	-.042	-.034
15	1.250	.450	2.000	-.049	-.041	-.049	-.041	-.049	-.041
17	1.250	.450	2.000	-.056	-.048	-.056	-.048	-.056	-.048
19	1.250	.450	2.000	-.063	-.055	-.063	-.055	-.063	-.055
21	1.250	.450	2.000	-.070	-.062	-.070	-.062	-.070	-.062
23	1.250	.450	2.000	-.077	-.069	-.077	-.069	-.077	-.069
25	1.250	.450	2.000	-.084	-.076	-.084	-.076	-.084	-.076
27	1.250	.450	2.000	-.091	-.083	-.091	-.083	-.091	-.083
29	1.250	.450	2.000	-.098	-.090	-.098	-.090	-.098	-.090
31	1.250	.450	2.000	-.105	-.097	-.105	-.097	-.105	-.097
33	1.250	.450	2.000	-.112	-.104	-.112	-.104	-.112	-.104
35	1.250	.450	2.000	-.119	-.111	-.119	-.111	-.119	-.111
37	1.250	.450	2.000	-.126	-.118	-.126	-.118	-.126	-.118
39	1.250	.450	2.000	-.133	-.125	-.133	-.125	-.133	-.125
41	1.250	.450	2.000	-.140	-.132	-.140	-.132	-.140	-.132
43	1.250	.450	2.000	-.147	-.139	-.147	-.139	-.147	-.139
45	1.250	.450	2.000	-.154	-.146	-.154	-.146	-.154	-.146
47	1.250	.450	2.000	-.161	-.153	-.161	-.153	-.161	-.153
49	1.250	.450	2.000	-.168	-.160	-.168	-.160	-.168	-.160
51	1.250	.450	2.000	-.175	-.167	-.175	-.167	-.175	-.167
53	1.250	.450	2.000	-.182	-.174	-.182	-.174	-.182	-.174
55	1.250	.450	2.000	-.189	-.181	-.189	-.181	-.189	-.181
57	1.250	.450	2.000	-.196	-.188	-.196	-.188	-.196	-.188
59	1.250	.450	2.000	-.203	-.195	-.203	-.195	-.203	-.195
61	1.250	.450	2.000	-.210	-.202	-.210	-.202	-.210	-.202
63	1.250	.450	2.000	-.217	-.209	-.217	-.209	-.217	-.209
65	1.250	.450	2.000	-.224	-.216	-.224	-.216	-.224	-.216
67	1.250	.450	2.000	-.231	-.223	-.231	-.223	-.231	-.223
69	1.250	.450	2.000	-.238	-.230	-.238	-.230	-.238	-.230
71	1.250	.450	2.000	-.245	-.237	-.245	-.237	-.245	-.237
73	1.250	.450	2.000	-.252	-.244	-.252	-.244	-.252	-.244
75	1.250	.450	2.000	-.259	-.251	-.259	-.251	-.259	-.251
77	1.250	.450	2.000	-.266	-.258	-.266	-.258	-.266	-.258
79	1.250	.450	2.000	-.273	-.265	-.273	-.265	-.273	-.265
81	1.250	.450	2.000	-.280	-.272	-.280	-.272	-.280	-.272
83	1.250	.450	2.000	-.287	-.279	-.287	-.279	-.287	-.279
85	1.250	.450	2.000	-.294	-.286	-.294	-.286	-.294	-.286
87	1.250	.450	2.000	-.301	-.2				

1	2.750	.550	2.200	.710	.932	.172	1.112	1.026	.870
5	.750	.800	2.200	-.135	-.039	-.049	.022	.016	.094
	.750	.850	2.200	-.263	-.075	-.075	.027	.033	.010
	.750	.900	2.200	-.387	-.115	-.133	.075	.055	.021
	.750	.950	2.200	-.513	-.156	-.184	.106	.091	.037
9	.750	.950	2.000	-.189	-.137	-.144	.147	.114	.059
	.950	.650	2.200	-.184	-.137	-.193	.121	.153	.086
11	.950	.650	2.000	-.351	-.128	-.191	.241	.197	.123
	.750	.550	2.200	-.645	-.110	-.130	.274	.245	.164
13	.950	.550	2.000	-.834	-.034	-.161	.351	.297	.238
	.950	.450	2.200	-.961	-.052	-.134	.410	.352	.256
15	1.050	.800	2.000	.037	-.015	-.103	.469	.400	.305
	1.150	.800	2.200	.080	.025	-.068	.529	.464	.356
17	1.250	.800	2.200	.125	.057	-.031	.597	.519	.406
	1.350	.670	2.200	.170	.110	.000	.644	.574	.456
19	1.450	.670	2.200	.215	.153	.073	.679	.626	.504
	1.550	.600	2.200	.260	.195	.087	.752	.676	.550
21	1.650	.550	2.000	.303	.236	.125	.802	.724	.595
	1.750	.600	2.200	.345	.276	.162	.849	.770	.637
23	1.850	.600	2.000	.385	.315	.195	.894	.812	.677
	1.950	.650	2.200	.422	.351	.232	.936	.853	.715
25	2.050	.550	2.000	.459	.346	.265	.975	.891	.751
	2.150	.550	2.000	.492	.410	.296	1.011	.926	.784
27	2.250	.550	2.000	.524	.449	.325	1.046	.959	.815
	2.350	.650	2.000	.561	.478	.352	1.078	.990	.844
29	2.450	.550	2.000	.592	.506	.376	1.108	1.019	.872
	2.550	.650	2.200	.633	.531	.402	1.135	1.046	.897
31	2.650	.650	2.200	.663	.555	.425	1.161	1.071	.921
	2.750	.650	2.200	.696	.576	.447	1.186	1.095	.943
33	2.850	.650	2.000	.723	.579	.467	1.208	1.117	.964
	2.950	.650	2.000	.753	.618	.486	1.229	1.137	.983
35	.350	.750	2.000	-.031	-.036	-.046	.030	.031	.020
	.150	.750	2.200	-.052	-.076	-.088	.077	.063	.041
37	.250	.750	2.000	-.051	-.097	-.124	.119	.099	.065
	.350	.750	2.000	-.095	-.117	-.152	.164	.138	.094
39	.450	.750	2.000	-.131	-.127	-.171	.214	.182	.128
	.550	.750	2.000	-.097	-.124	-.179	.267	.230	.166
41	.650	.750	2.000	-.064	-.119	-.178	.325	.281	.210
	.750	.750	2.200	-.061	-.102	-.167	.335	.337	.257
43	.850	.750	2.000	-.035	-.076	-.149	.446	.394	.307
	.950	.750	2.000	-.061	-.047	-.124	.509	.453	.358
45	1.050	.750	2.000	.037	-.012	-.044	.572	.511	.411
	1.150	.750	2.000	.073	.026	-.031	.634	.570	.464
47	1.250	.750	2.000	.121	.056	-.025	.694	.627	.516
	1.350	.750	2.000	.164	.137	.013	.752	.683	.567
49	1.450	.750	2.000	.204	.119	.051	.808	.736	.616
	1.550	.750	2.000	.251	.170	.084	.862	.787	.663
51	1.650	.750	2.000	.293	.230	.125	.912	.836	.708
	1.750	.750	2.000	.333	.259	.162	.960	.882	.751
53	1.850	.750	2.000	.372	.316	.196	1.005	.925	.791
	1.950	.750	2.000	.403	.341	.230	1.047	.965	.829
55	2.050	.750	2.000	.443	.375	.262	1.086	1.003	.865
	2.150	.750	2.000	.475	.407	.292	1.123	1.039	.898
57	2.250	.750	2.000	.513	.437	.320	1.157	1.072	.930
	2.350	.750	2.000	.557	.466	.347	1.189	1.103	.959
59	2.450	.750	2.000	.599	.473	.373	1.219	1.132	.986
	2.550	.750	2.000	.640	.514	.397	1.247	1.159	1.012
61	2.650	.750	2.000	.685	.541	.419	1.273	1.184	1.035
	2.750	.750	2.000	.731	.647				

[illegible]

2.250	1.250	2.250	.026	.071	.103	1.517	1.450	1.311
.250	1.250	2.250	-.023	-.020	-.033	.077	.071	.061
1.150	1.250	2.250	-.044	-.033	-.057	.155	.142	.122
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.150	1.250	2.250	-.072	-.042	-.116	.311	.285	.246
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.050	1.250	2.250	-.063	-.090	-.134	.546	.506	.439
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1.650	1.250	2.250	.250	.209	.127	1.205	1.133	1.013
1.750	1.250	2.250	.279	.244	.160	1.254	1.180	1.057
1.850	1.250	2.250	.327	.277	.191	1.300	1.224	1.096
1.950	1.250	2.250	.362	.310	.222	1.342	1.265	1.136
2.050	1.250	2.250	.399	.340	.251	1.381	1.303	1.172
2.150	1.250	2.250	.425	.370	.279	1.418	1.338	1.205
2.250	1.250	2.250	.453	.398	.305	1.453	1.371	1.236
2.350	1.250	2.250	.480	.424	.330	1.484	1.402	1.265
2.450	1.250	2.250	.508	.449	.354	1.514	1.431	1.293
2.550	1.250	2.250	.530	.473	.376	1.542	1.458	1.318
2.650	1.250	2.250	.553	.495	.398	1.567	1.483	1.341
2.750	1.250	2.250	.575	.516	.418	1.591	1.506	1.363
2.850	1.250	2.250	.595	.535	.436	1.614	1.529	1.384
2.950	1.250	2.250	.614	.554	.454	1.635	1.548	1.403
.350	1.150	2.250	-.021	-.025	-.031	.087	.081	.071
.150	1.150	2.250	-.050	-.047	-.069	.174	.162	.142
.250	1.150	2.250	-.055	-.055	-.094	.261	.243	.214
.350	1.150	2.250	-.065	-.074	-.103	.348	.329	.285
.450	1.150	2.250	-.068	-.096	-.116	.434	.405	.357
.550	1.150	2.250	-.065	-.096	-.121	.519	.485	.426
.650	1.150	2.250	-.055	-.079	-.120	.602	.564	.499
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.950	1.150	2.250	.008	-.024	-.077	.840	.787	.703
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1.550	1.150	2.250	.212	.169	.097	1.228	1.160	1.046
1.650	1.150	2.250	.247	.202	.128	1.281	1.210	1.093
1.750	1.150	2.250	.281	.236	.159	1.329	1.257	1.136
1.850	1.150	2.250	.315	.268	.190	1.375	1.301	1.177
1.950	1.150	2.250	.347	.299	.219	1.417	1.342	1.216
2.050	1.150	2.250	.377	.329	.247	1.457	1.380	1.252
2.150	1.150	2.250	.407	.357	.274	1.494	1.415	1.285
2.250	1.150	2.250	.435	.384	.300	1.528	1.448	1.316
2.350	1.150	2.250	.461	.410	.324	1.560	1.479	1.345
2.450	1.150	2.250	.486	.434	.347	1.589	1.508	1.372
2.550	1.150	2.250	.509	.457	.369	1.617	1.534	1.397
2.650	1.150	2.250	.532	.478	.393	1.643	1.559	1.421

3	2.750	1.750	2.750	.000	.000	.000	1.750	1.750	1.750
5	2.750	1.750	2.750	-.010	-.010	-.010	1.740	1.740	1.740
7	2.750	1.750	2.750	-.020	-.020	-.020	1.730	1.730	1.730
9	2.750	1.750	2.750	-.030	-.030	-.030	1.720	1.720	1.720
11	2.750	1.750	2.750	-.040	-.040	-.040	1.710	1.710	1.710
13	2.750	1.750	2.750	-.050	-.050	-.050	1.700	1.700	1.700
15	2.750	1.750	2.750	-.060	-.060	-.060	1.690	1.690	1.690
17	2.750	1.750	2.750	-.070	-.070	-.070	1.680	1.680	1.680
19	2.750	1.750	2.750	-.080	-.080	-.080	1.670	1.670	1.670
21	2.750	1.750	2.750	-.090	-.090	-.090	1.660	1.660	1.660
23	2.750	1.750	2.750	-.100	-.100	-.100	1.650	1.650	1.650
25	2.750	1.750	2.750	-.110	-.110	-.110	1.640	1.640	1.640
27	2.750	1.750	2.750	-.120	-.120	-.120	1.630	1.630	1.630
29	2.750	1.750	2.750	-.130	-.130	-.130	1.620	1.620	1.620
31	2.750	1.750	2.750	-.140	-.140	-.140	1.610	1.610	1.610
33	2.750	1.750	2.750	-.150	-.150	-.150	1.600	1.600	1.600
35	2.750	1.750	2.750	-.160	-.160	-.160	1.590	1.590	1.590
37	2.750	1.750	2.750	-.170	-.170	-.170	1.580	1.580	1.580
39	2.750	1.750	2.750	-.180	-.180	-.180	1.570	1.570	1.570
41	2.750	1.750	2.750	-.190	-.190	-.190	1.560	1.560	1.560
43	2.750	1.750	2.750	-.200	-.200	-.200	1.550	1.550	1.550
45	2.750	1.750	2.750	-.210	-.210	-.210	1.540	1.540	1.540
47	2.750	1.750	2.750	-.220	-.220	-.220	1.530	1.530	1.530
49	2.750	1.750	2.750	-.230	-.230	-.230	1.520	1.520	1.520
51	2.750	1.750	2.750	-.240	-.240	-.240	1.510	1.510	1.510
53	2.750	1.750	2.750	-.250	-.250	-.250	1.500	1.500	1.500
55	2.750	1.750	2.750	-.260	-.260	-.260	1.490	1.490	1.490
57	2.750	1.750	2.750	-.270	-.270	-.270	1.480	1.480	1.480
59	2.750	1.750	2.750	-.280	-.280	-.280	1.470	1.470	1.470
61	2.750	1.750	2.750	-.290	-.290	-.290	1.460	1.460	1.460
63	2.750	1.750	2.750	-.300	-.300	-.300	1.450	1.450	1.450
65	2.750	1.750	2.750	-.310	-.310	-.310	1.440	1.440	1.440
67	2.750	1.750	2.750	-.320	-.320	-.320	1.430	1.430	1.430
69	2.750	1.750	2.750	-.330	-.330	-.330	1.420	1.420	1.420
71	2.750	1.750	2.750	-.340	-.340	-.340	1.410	1.410	1.410
73	2.750	1.750	2.750	-.350	-.350	-.350	1.400	1.400	1.400
75	2.750	1.750	2.750	-.360	-.360	-.360	1.390	1.390	1.390
77	2.750	1.750	2.750	-.370	-.370	-.370	1.380	1.380	1.380
79	2.750	1.750	2.750	-.380	-.380	-.380	1.370	1.370	1.370
81	2.750	1.750	2.750	-.390	-.390	-.390	1.360	1.360	1.360
83	2.750	1.750	2.750	-.400	-.400	-.400	1.350	1.350	1.350
85	2.750	1.750	2.750	-.410	-.410	-.410	1.340	1.340	1.340
87	2.750	1.750	2.750	-.420	-.420	-.420	1.330	1.330	1.330
89	2.750	1.750	2.750	-.430	-.430	-.430	1.320	1.320	1.320
91	2.750	1.750	2.750	-.440	-.440	-.440	1.310	1.310	1.310
93	2.750	1.750	2.750	-.450	-.450	-.450	1.300	1.300	1.300
95	2.750	1.750	2.750	-.460	-.460	-.460	1.290	1.290	1.290
97	2.750	1.750	2.750	-.470	-.470	-.470	1.280	1.280	1.280
99	2.750	1.750	2.750	-.480	-.480	-.480	1.270	1.270	1.270
101	2.750	1.750	2.750	-.490	-.490	-.490	1.260	1.260	1.260
103	2.750	1.750	2.750	-.500	-.500	-.500	1.250	1.250	1.250
105	2.750	1.750	2.750	-.510	-.510	-.510	1.240	1.240	1.240
107	2.750	1.750	2.750	-.520	-.520	-.520	1.230	1.230	1.230
109	2.750	1.750	2.750	-.530	-.530	-.530	1.220	1.220	1.220
111	2.750	1.750	2.750	-.540	-.540	-.540	1.210	1.210	1.210
113	2.750	1.750	2.750	-.550	-.550	-.550	1.200	1.200	1.200
115	2.750	1.750	2.750	-.560	-.560	-.560	1.190	1.190	1.190
117	2.750	1.750	2.750	-.570	-.570	-.570	1.180	1.180	1.180
119	2.750	1.750	2.750	-.580	-.580	-.580	1.170	1.170	1.170
121	2.750	1.750	2.750	-.590	-.590	-.590	1.160	1.160	1.160
123	2.750	1.750	2.750	-.600	-.600	-.600	1.150	1.150	1.150
125	2.750	1.750	2.750	-.610	-.610	-.610	1.140	1.140	1.140
127	2.750	1.750	2.750	-.620	-.620	-.620	1.130	1.130	1.130
129	2.750	1.750	2.750	-.630	-.630	-.630	1.120	1.120	1.120
131	2.750	1.750	2.750	-.640	-.640	-.640	1.110	1.110	1.110
133	2.750	1.750	2.750	-.650	-.650	-.650	1.100	1.100	1.100
135	2.750	1.750	2.750	-.660	-.660	-.660	1.090	1.090	1.090
137	2.750	1.750	2.750	-.670	-.670	-.670	1.080	1.080	1.080
139	2.750	1.750	2.750	-.680	-.680	-.680	1.070	1.070	1.070
141	2.750	1.750	2.750	-.690	-.690	-.690	1.060	1.060	1.060
143	2.750	1.750	2.750	-.700	-.700	-.700	1.050	1.050	1.050
145	2.750	1.750	2.750	-.710	-.710	-.710	1.040	1.040	1.040
147	2.750	1.750	2.750	-.720	-.720	-.720	1.030	1.030	1.030
149	2.750	1.750	2.750	-.730	-.730	-.730	1.020	1.020	1.020
151	2.750	1.750	2.750	-.740	-.740	-.740	1.010	1.010	1.010
153	2.750	1.750	2.750	-.750	-.750	-.750	1.000	1.000	1.000
155	2.750	1.750	2.750	-.760	-.760	-.760	0.990	0.990	0.990
157	2.750	1.750	2.750	-.770	-.770	-.770	0.980	0.980	0.980
159	2.750	1.750	2.750	-.780	-.780	-.780	0.970	0.970	0.970
161	2.750	1.750	2.750	-.790	-.790	-.790	0.960	0.960	0.960
163	2.750	1.750	2.750	-.800	-.800	-.800	0.950	0.950	0.950
165	2.750	1.750	2.750	-.810	-.810	-.810	0.940	0.940	0.940
167	2.750	1.750	2.750	-.820	-.820	-.820	0.930	0.930	0.930
169	2.750	1.750	2.750	-.830	-.830	-.830	0.920	0.920	0.920
171	2.750	1.750	2.750	-.840	-.840	-.840	0.910	0.910	0.910
173	2.750	1.750	2.750	-.850	-.850	-.850	0.900	0.900	0.900
175	2.750	1.750	2.750	-.860	-.860	-.860	0.890	0.890	0.890
177	2.750	1.750	2.750	-.870	-.870	-.870	0.880	0.880	0.880
179	2.750	1.750	2.750	-.880	-.880	-.880	0.870	0.870	0.870
181	2.750	1.750	2.750	-.890	-.890	-.890	0.860	0.860	0.860
183	2.750	1.750	2.750	-.900	-.900	-.900	0.850	0.850	0.850
185	2.750	1.750	2.750	-.910	-.910	-.910	0.840	0.840	0.840
187	2.750	1.750	2.750	-.920	-.920	-.920	0.830	0.830	0.830
189	2.750	1.750	2.750	-.930	-.930	-.930	0.820	0.820	0.820
191	2.750	1.750	2.750	-.940	-.940	-.940	0.810	0.810	0.810
193	2.750	1.750	2.750	-.950	-.950	-.950	0.800	0.800	0.800
195	2.750	1.750	2.750	-.960	-.960	-.960	0.790	0.790	0.790
197	2.750	1.750	2.750	-.970	-.970	-.970	0.780	0.780	0.780
199	2.750	1.750	2.750	-.980	-.980	-.980	0.770	0.770	0.770
201	2.750	1.750	2.750	-.990	-.990	-.990	0.760	0.760	0.760
203	2.750	1.750	2.750	-1.000	-1.000	-1.000	0.750	0.750	0.750

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LINE	DATE	001277	PAGE	119
1	1.000	1.000	2.000	1.000
2	1.000	1.000	2.000	1.000
3	1.000	1.000	2.000	1.000
4	1.000	1.000	2.000	1.000
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11	1.000	1.000	2.000	1.000
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14	1.000	1.000	2.000	1.000
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29	1.000	1.000	2.000	1.000
30	1.000	1.000	2.000	1.000
31	1.000	1.000	2.000	1.000
32	1.000	1.000	2.000	1.000
33	1.000	1.000	2.000	1.000
34	1.000	1.000	2.000	1.000
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36	1.000	1.000	2.000	1.000
37	1.000	1.000	2.000	1.000
38	1.000	1.000	2.000	1.000
39	1.000	1.000	2.000	1.000
40	1.000	1.000	2.000	1.000
41	1.000	1.000	2.000	1.000
42	1.000	1.000	2.000	1.000
43	1.000	1.000	2.000	1.000
44	1.000	1.000	2.000	1.000
45	1.000	1.000	2.000	1.000
46	1.000	1.000	2.000	1.000
47	1.000	1.000	2.000	1.000
48	1.000	1.000	2.000	1.000
49	1.000	1.000	2.000	1.000
50	1.000	1.000	2.000	1.000
51	1.000	1.000	2.000	1.000
52	1.000	1.000	2.000	1.000
53	1.000	1.000	2.000	1.000
54	1.000	1.000	2.000	1.000
55	1.000	1.000	2.000	1.000
56	1.000	1.000	2.000	1.000
57	1.000	1.000	2.000	1.000
58	1.000	1.000	2.000	1.000
59	1.000	1.000	2.000	1.000
60	1.000	1.000	2.000	1.000
61	1.000	1.000	2.000	1.000
62	1.000	1.000	2.000	1.000
63	1.000	1.000	2.000	1.000

[illegible]

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3	2.750	2.500	2.250	.327	.129	.022	1.154	1.492	1.308
5	2.750	2.500	2.250	.321	.121	.001	1.195	1.484	1.076
7	2.750	2.500	2.250	.312	.112	.002	1.178	1.462	1.152
9	2.750	2.500	2.250	.303	.104	.004	1.251	1.243	1.226
11	2.750	2.500	2.250	.294	.096	.007	1.335	1.322	1.300
13	2.750	2.500	2.250	.285	.089	.010	1.415	1.399	1.371
15	2.750	2.500	2.250	.276	.081	.013	1.493	1.473	1.441
17	2.750	2.500	2.250	.267	.072	.016	1.568	1.545	1.507
19	2.750	2.500	2.250	.258	.064	.019	1.640	1.614	1.572
21	2.750	2.500	2.250	.249	.056	.022	1.707	1.681	1.633
23	2.750	2.500	2.250	.240	.049	.024	1.775	1.744	1.692
25	2.750	2.500	2.250	.231	.041	.027	1.843	1.803	1.747
27	2.750	2.500	2.250	.222	.034	.029	1.910	1.860	1.800
29	2.750	2.500	2.250	.213	.026	.031	1.974	1.913	1.850
31	2.750	2.500	2.250	.204	.019	.034	2.034	1.963	1.896
33	2.750	2.500	2.250	.195	.106	.106	1.053	1.011	1.940
35	2.750	2.500	2.250	.186	.121	.122	1.099	1.055	1.981
37	2.750	2.500	2.250	.177	.135	.137	1.142	1.096	1.919
39	2.750	2.500	2.250	.168	.150	.151	1.182	1.135	1.055
41	2.750	2.500	2.250	.159	.165	.166	1.220	1.171	1.089
43	2.750	2.500	2.250	.150	.180	.181	1.255	1.205	1.120
45	2.750	2.500	2.250	.141	.195	.196	1.290	1.235	1.149
47	2.750	2.500	2.250	.132	.209	.210	1.319	1.266	1.177
49	2.750	2.500	2.250	.123	.224	.225	1.347	1.293	1.202
51	2.750	2.500	2.250	.114	.238	.239	1.374	1.319	1.226
53	2.750	2.500	2.250	.105	.252	.252	1.399	1.342	1.248
55	2.750	2.500	2.250	.096	.265	.265	1.422	1.365	1.269
57	2.750	2.500	2.250	.087	.279	.279	1.444	1.386	1.288
59	2.750	2.500	2.250	.078	.292	.291	1.464	1.405	1.306
61	2.750	2.500	2.250	.069	.306	.306	1.483	1.423	1.323
63	2.750	2.500	2.250	.060	.319	.319	1.501	1.440	1.339
65	2.750	2.500	2.250	.051	.332	.332	1.518	1.457	1.354
67	2.750	2.500	2.250	.042	.345	.345	1.534	1.472	1.368
69	2.750	2.500	2.250	.033	.358	.358	1.549	1.486	1.381
71	2.750	2.500	2.250	.024	.371	.371	1.563	1.499	1.394
73	2.750	2.500	2.250	.015	.384	.384	1.576	1.511	1.406
75	2.750	2.500	2.250	.006	.397	.397	1.588	1.522	1.417
77	2.750	2.500	2.250	.000	.410	.410	1.599	1.532	1.427
79	2.750	2.500	2.250	.000	.423	.423	1.609	1.541	1.436
81	2.750	2.500	2.250	.000	.436	.436	1.618	1.549	1.444
83	2.750	2.500	2.250	.000	.449	.449	1.626	1.556	1.451
85	2.750	2.500	2.250	.000	.462	.462	1.634	1.563	1.457
87	2.750	2.500	2.250	.000	.475	.475	1.641	1.569	1.462
89	2.750	2.500	2.250	.000	.488	.488	1.647	1.574	1.466
91	2.750	2.500	2.250	.000	.501	.501	1.653	1.579	1.470
93	2.750	2.500	2.250	.000	.514	.514	1.658	1.583	1.473
95	2.750	2.500	2.250	.000	.527	.527	1.663	1.587	1.476
97	2.750	2.500	2.250	.000	.540	.540	1.668	1.591	1.479
99	2.750	2.500	2.250	.000	.553	.553	1.672	1.594	1.481
101	2.750	2.500	2.250	.000	.566	.566	1.676	1.597	1.483
103	2.750	2.500	2.250	.000	.579	.579	1.680	1.600	1.485
105	2.750	2.500	2.250	.000	.592	.592	1.683	1.602	1.487
107	2.750	2.500	2.250	.000	.605	.605	1.686	1.604	1.488
109	2.750	2.500	2.250	.000	.618	.618	1.689	1.606	1.489
111	2.750	2.500	2.250	.000	.631	.631	1.691	1.607	1.490
113	2.750	2.500	2.250	.000	.644	.644	1.693	1.608	1.491
115	2.750	2.500	2.250	.000	.657	.657	1.695	1.609	1.492
117	2.750	2.500	2.250	.000	.670	.670	1.697	1.610	1.493
119	2.750	2.500	2.250	.000	.683	.683	1.699	1.611	1.494
121	2.750	2.500	2.250	.000	.696	.696	1.701	1.612	1.495
123	2.750	2.500	2.250	.000	.709	.709	1.702	1.613	1.495
125	2.750	2.500	2.250	.000	.722	.722	1.703	1.614	1.496
127	2.750	2.500	2.250	.000	.735	.735	1.704	1.614	1.496
129	2.750	2.500	2.250	.000	.748	.748	1.705	1.615	1.496
131	2.750	2.500	2.250	.000	.761	.761	1.706	1.615	1.496
133	2.750	2.500	2.250	.000	.774	.774	1.707	1.615	1.496
135	2.750	2.500	2.250	.000	.787	.787	1.707	1.615	1.496
137	2.750	2.500	2.250	.000	.800	.800	1.707	1.615	1.496
139	2.750	2.500	2.250	.000	.813	.813	1.707	1.615	1.496
141	2.750	2.500	2.250	.000	.826	.826	1.707	1.615	1.496
143	2.750	2.500	2.250	.000	.839	.839	1.707	1.615	1.496
145	2.750	2.500	2.250	.000	.852	.852	1.707	1.615	1.496
147	2.750	2.500	2.250	.000	.865	.865	1.707	1.615	1.496
149	2.750	2.500	2.250	.000	.878	.878	1.707	1.615	1.496
151	2.750	2.500	2.250	.000	.891	.891	1.707	1.615	1.496
153	2.750	2.500	2.250	.000	.904	.904	1.707	1.615	1.496
155	2.750	2.500	2.250	.000	.917	.917	1.707	1.615	1.496
157	2.750	2.500	2.250	.000	.930	.930	1.707	1.615	1.496
159	2.750	2.500	2.250	.000	.943	.943	1.707	1.615	1.496
161	2.750	2.500	2.250	.000	.956	.956	1.707	1.615	1.496
163	2.750	2.500	2.250	.000	.969	.969	1.707	1.615	1.496
165	2.750	2.500	2.250	.000	.982	.982	1.707	1.615	1.496
167	2.750	2.500	2.250	.000	.995	.995	1.707	1.615	1.496
169	2.750	2.500	2.250	.000	1.008	1.008	1.707	1.615	1.496
171	2.750	2.500	2.250	.000	1.021	1.021	1.707	1.615	1.496
173	2.750	2.500	2.250	.000	1.034	1.034	1.707	1.615	1.496
175	2.750	2.500	2.250	.000	1.047	1.047	1.707	1.615	1.496
177	2.750	2.500	2.250	.000	1.060	1.060	1.707	1.615	1.496
179	2.750	2.500	2.250	.000	1.073	1.073	1.707	1.615	1.496
181	2.750	2.500	2.250	.000	1.086	1.086	1.707	1.615	1.496
183	2.750	2.500	2.250	.000	1.099	1.099	1.707	1.615	1.496
185	2.750	2.500	2.250	.000	1.112	1.112	1.707	1.615	1.496
187	2.750	2.500	2.250	.000	1.125	1.125	1.707	1.615	1.496
189	2.750	2.500	2.250	.000	1.138	1.138	1.707	1.615	1.496
191	2.750	2.500	2.250	.000	1.151	1.151	1.707	1.615	1.496
193	2.750	2.500	2.250	.000	1.164	1.164	1.707	1.615	1.496
195	2.750	2.500	2.250	.000	1.177	1.177	1.707	1.615	1.496
197	2.750	2.500	2.250	.000	1.190	1.190	1.707	1.615	1.496
199	2.750	2.500	2.250	.000	1.203	1.203	1.707	1.615	1.496
201	2.750	2.500	2.250	.000	1.216	1.216	1.707	1.615	1.496
203	2.750	2.500	2.250	.000	1.229	1.229	1.707	1.615	1.496
205	2.750	2.500	2.250	.000	1.242	1.242	1.707	1.615	1.496
207	2.750	2.500	2.250	.000	1.255	1.255	1.707	1.615	1.496
209	2.750	2.500	2.250	.000	1.268	1.268	1.707	1.615	1.496
211	2.750	2.500	2.250	.000	1.281	1.281	1.707	1.615	1.496
213	2.750	2.500	2.250	.000	1.294	1.294	1.707	1.615	1.496
215	2.750	2.500	2.250	.000	1.307	1.307	1.707	1.615	1.496
217	2.750	2.500	2.250	.000	1.320	1.320	1.707	1.615	1.496
219	2.750	2.500	2.250	.000	1.333	1.333	1.707	1.615	1.496
221	2.750	2.500	2.250	.000	1.346	1.346	1.707	1.615	1.496
223	2.750	2.500	2.250	.000	1.359	1.359	1.707	1.615	1.496
225	2.750	2.500	2.250	.000	1.372	1.372	1.707	1.615	1.496
227	2.750	2.500	2.250	.000	1.385	1.385	1.707	1.615	1.496
229	2.750	2.500	2.250	.000	1.398	1.398	1.707	1.615	1.496
231	2.750	2.500	2.250	.000	1.411	1.411	1.707	1.615	1.496
233	2.750	2.500	2.250	.000	1.424	1.424	1.707	1.615	1.496
235	2.750	2.500	2.250	.000	1.437	1.437	1.707	1.615	1.496
237	2.750	2.500	2.250	.000	1.450	1.450	1.707	1.615	1.496
239	2.750	2.500	2.250	.000	1.463	1.463	1.707	1.615	1.496
241	2.750	2.500	2.250	.000	1.476	1.476	1.707	1.615	1.496
243	2.750	2.500	2.250	.000	1.489	1.489	1.707	1.615	1.496
245	2.750	2.500	2.250	.000	1.502	1.502	1.707	1.615	1.496
247	2.750	2.500	2.250	.000	1.515	1.515	1.707	1.615	1.496
249	2.750	2.500	2.250	.000	1				

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	DATE	TIME	STATION	TYPE	WIND	TEMP	PRESS	HUMID	SEA	WAVE	CLOUDS	REMARKS
3	07/13/77	0800	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
5	07/13/77	0900	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
6	07/13/77	1000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
8	07/13/77	1100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
10	07/13/77	1200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
11	07/13/77	1300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
12	07/13/77	1400	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
13	07/13/77	1500	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
14	07/13/77	1600	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
15	07/13/77	1700	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
16	07/13/77	1800	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
17	07/13/77	1900	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
18	07/13/77	2000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
19	07/13/77	2100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
20	07/13/77	2200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
21	07/13/77	2300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
22	07/13/77	0000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
23	07/13/77	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
24	07/13/77	0200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
25	07/13/77	0300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
26	07/13/77	0400	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
27	07/13/77	0500	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
28	07/13/77	0600	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
29	07/13/77	0700	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
30	07/13/77	0800	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
31	07/13/77	0900	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
32	07/13/77	1000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
33	07/13/77	1100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
34	07/13/77	1200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
35	07/13/77	1300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
36	07/13/77	1400	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
37	07/13/77	1500	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
38	07/13/77	1600	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
39	07/13/77	1700	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
40	07/13/77	1800	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
41	07/13/77	1900	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
42	07/13/77	2000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
43	07/13/77	2100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
44	07/13/77	2200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
45	07/13/77	2300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
46	07/13/77	0000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
47	07/13/77	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
48	07/13/77	0200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
49	07/13/77	0300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
50	07/13/77	0400	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
51	07/13/77	0500	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
52	07/13/77	0600	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
53	07/13/77	0700	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
54	07/13/77	0800	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
55	07/13/77	0900	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
56	07/13/77	1000	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
57	07/13/77	1100	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
58	07/13/77	1200	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
59	07/13/77	1300	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
60	07/13/77	1400	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
61	07/13/77	1500	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100
62	07/13/77	1600	0100	0100	0100	0100	0100	0100	0100	0100	0100	0100

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UCT

3	2.950	1.250	3.200	.271	.224	.130	.710	.656	.585	40
5	2.950	1.250	3.200	-.013	-.018	-.019	.622	.619	.614	42
7	2.950	1.250	3.200	-.013	-.018	-.019	.649	.636	.629	44
9	2.950	1.250	3.200	-.013	-.018	-.019	.677	.650	.644	46
11	2.950	1.250	3.200	-.013	-.018	-.019	.705	.679	.659	48
13	2.950	1.250	3.200	-.013	-.018	-.019	.733	.680	.676	50
15	2.950	1.250	3.200	-.013	-.018	-.019	.761	.692	.694	52
17	2.950	1.250	3.200	-.013	-.018	-.019	.789	.715	.712	54
19	2.950	1.250	3.200	-.013	-.018	-.019	.817	.743	.732	56
21	2.950	1.250	3.200	-.013	-.018	-.019	.845	.769	.767	58
23	2.950	1.250	3.200	-.013	-.018	-.019	.873	.793	.791	60
25	2.950	1.250	3.200	-.013	-.018	-.019	.901	.811	.812	62
27	2.950	1.250	3.200	-.013	-.018	-.019	.929	.839	.838	64
29	2.950	1.250	3.200	-.013	-.018	-.019	.957	.867	.866	66
31	2.950	1.250	3.200	-.013	-.018	-.019	.985	.895	.894	68
33	2.950	1.250	3.200	-.013	-.018	-.019	1.013	.923	.922	70
35	2.950	1.250	3.200	-.013	-.018	-.019	1.041	.951	.950	72
37	2.950	1.250	3.200	-.013	-.018	-.019	1.069	.979	.978	74
39	2.950	1.250	3.200	-.013	-.018	-.019	1.097	.999	.998	76
41	2.950	1.250	3.200	-.013	-.018	-.019	1.125	1.019	1.018	78
43	2.950	1.250	3.200	-.013	-.018	-.019	1.153	1.039	1.038	80
45	2.950	1.250	3.200	-.013	-.018	-.019	1.181	1.059	1.058	82
47	2.950	1.250	3.200	-.013	-.018	-.019	1.209	1.079	1.078	84
49	2.950	1.250	3.200	-.013	-.018	-.019	1.237	1.099	1.098	86
51	2.950	1.250	3.200	-.013	-.018	-.019	1.265	1.119	1.118	88
53	2.950	1.250	3.200	-.013	-.018	-.019	1.293	1.139	1.138	90
55	2.950	1.250	3.200	-.013	-.018	-.019	1.321	1.159	1.158	92
57	2.950	1.250	3.200	-.013	-.018	-.019	1.349	1.179	1.178	94
59	2.950	1.250	3.200	-.013	-.018	-.019	1.377	1.199	1.198	96
61	2.950	1.250	3.200	-.013	-.018	-.019	1.405	1.219	1.218	98
63	2.950	1.250	3.200	-.013	-.018	-.019	1.433	1.239	1.238	100

UCT

3	1.350	1.350	3.000	.247	.217	.151	.807	.744	.662
5	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
7	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
9	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
11	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
13	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
15	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
17	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
19	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
21	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
23	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
25	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
27	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
29	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
31	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
33	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
35	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
37	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
39	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
41	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
43	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
45	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
47	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
49	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
51	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
53	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
55	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
57	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
59	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
61	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022
63	1.350	1.350	3.000	-.014	-.013	-.017	.140	.027	.022

UCT

3	2.700	1.700	3.000	.240	.125	.146	.752	.902	.815
5	2.700	1.700	3.000	-.000	-.011	-.112	.742	.897	.835
7	2.700	1.700	3.000	-.000	-.017	-.220	.731	.892	.820
9	2.700	1.700	3.000	-.000	-.024	-.326	.720	.889	.805
11	2.700	1.700	3.000	-.000	-.033	-.430	.707	.882	.789
13	2.700	1.700	3.000	-.000	-.043	-.532	.693	.874	.774
15	2.700	1.700	3.000	-.000	-.053	-.632	.679	.865	.759
17	2.700	1.700	3.000	-.000	-.064	-.730	.664	.856	.749
19	2.700	1.700	3.000	-.000	-.075	-.826	.649	.846	.739
21	2.700	1.700	3.000	-.000	-.086	-.920	.634	.836	.730
23	2.700	1.700	3.000	-.000	-.097	-.1000	.619	.826	.720
25	2.700	1.700	3.000	-.000	-.108	-.1000	.604	.816	.710
27	2.700	1.700	3.000	-.000	-.119	-.1000	.589	.806	.700
29	2.700	1.700	3.000	-.000	-.130	-.1000	.574	.796	.690
31	2.700	1.700	3.000	-.000	-.141	-.1000	.559	.786	.680
33	2.700	1.700	3.000	-.000	-.152	-.1000	.544	.776	.670
35	2.700	1.700	3.000	-.000	-.163	-.1000	.529	.766	.660
37	2.700	1.700	3.000	-.000	-.174	-.1000	.514	.756	.650
39	2.700	1.700	3.000	-.000	-.185	-.1000	.499	.746	.640
41	2.700	1.700	3.000	-.000	-.196	-.1000	.484	.736	.630
43	2.700	1.700	3.000	-.000	-.207	-.1000	.469	.726	.620
45	2.700	1.700	3.000	-.000	-.218	-.1000	.454	.716	.610
47	2.700	1.700	3.000	-.000	-.229	-.1000	.439	.706	.600
49	2.700	1.700	3.000	-.000	-.240	-.1000	.424	.696	.590
51	2.700	1.700	3.000	-.000	-.251	-.1000	.409	.686	.580
53	2.700	1.700	3.000	-.000	-.262	-.1000	.394	.676	.570
55	2.700	1.700	3.000	-.000	-.273	-.1000	.379	.666	.560
57	2.700	1.700	3.000	-.000	-.284	-.1000	.364	.656	.550
59	2.700	1.700	3.000	-.000	-.295	-.1000	.349	.646	.540
61	2.700	1.700	3.000	-.000	-.306	-.1000	.334	.636	.530
63	2.700	1.700	3.000	-.000	-.317	-.1000	.319	.626	.520
65	2.700	1.700	3.000	-.000	-.328	-.1000	.304	.616	.510

UCT

3	1.150	2.150	3.150	.010	.110	.193	1.003	.959	.873
5	1.150	2.150	3.150	-.017	-.119	-.196	.046	.043	.039
7	1.150	2.150	3.150	-.014	-.118	-.191	.191	.066	.076
9	1.150	2.150	3.150	-.020	-.124	-.196	.136	.127	.117
11	1.150	2.150	3.150	-.025	-.130	-.207	.181	.172	.155
13	1.150	2.150	3.150	-.030	-.135	-.210	.226	.214	.193
15	1.150	2.150	3.150	-.032	-.138	-.212	.277	.255	.231
17	1.150	2.150	3.150	-.034	-.142	-.215	.313	.297	.269
19	1.150	2.150	3.150	-.034	-.143	-.216	.355	.337	.306
21	1.150	2.150	3.150	-.032	-.140	-.214	.393	.377	.347
23	1.150	2.150	3.150	-.029	-.137	-.211	.437	.416	.378
25	1.150	2.150	3.150	-.024	-.133	-.208	.479	.454	.412
27	1.150	2.150	3.150	-.019	-.128	-.204	.517	.492	.447
29	1.150	2.150	3.150	-.016	-.125	-.201	.557	.526	.480
31	1.150	2.150	3.150	-.013	-.124	-.199	.593	.563	.512
33	1.150	2.150	3.150	.009	-.107	-.196	.629	.597	.544
35	1.150	2.150	3.150	.023	-.083	-.190	.664	.630	.574
37	1.150	2.150	3.150	.032	.014	-.180	.697	.662	.603
39	1.150	2.150	3.150	.046	.026	-.165	.729	.692	.632
41	1.150	2.150	3.150	.059	.034	-.156	.760	.722	.654
43	1.150	2.150	3.150	.072	.051	-.140	.789	.750	.685
45	1.150	2.150	3.150	.086	.065	-.130	.817	.777	.710
47	1.150	2.150	3.150	.100	.075	-.115	.844	.803	.734
49	1.150	2.150	3.150	.114	.092	-.105	.870	.828	.754
51	1.150	2.150	3.150	.128	.115	-.096	.895	.852	.780
53	1.150	2.150	3.150	.142	.119	-.086	.919	.875	.801
55	1.150	2.150	3.150	.155	.132	-.073	.941	.896	.821
57	1.150	2.150	3.150	.169	.145	-.066	.963	.917	.840
59	1.150	2.150	3.150	.183	.157	-.056	.983	.937	.859
61	1.150	2.150	3.150	.195	.171	-.048	1.003	.956	.877
63	1.150	2.150	3.150	.209	.184	-.042	1.021	.973	.893
65	1.150	2.150	3.150	-.014	-.010	-.040	.047	.045	.040
67	1.150	2.150	3.150	-.013	-.015	-.039	.074	.089	.081
69	1.150	2.150	3.150	-.010	-.022	-.027	.143	.133	.121
71	1.150	2.150	3.150	-.005	-.026	-.032	.197	.177	.161
73	1.150	2.150	3.150	-.007	-.035	-.042	.232	.220	.201
75	1.150	2.150	3.150	-.009	-.036	-.047	.273	.263	.240
77	1.150	2.150	3.150	-.007	-.039	-.052	.322	.306	.278
79	1.150	2.150	3.150	-.000	-.039	-.054	.366	.347	.316
81	1.150	2.150	3.150	-.020	-.039	-.055	.409	.388	.354
83	1.150	2.150	3.150	-.024	-.036	-.054	.450	.428	.390
85	1.150	2.150	3.150	-.021	-.043	-.052	.491	.467	.426
87	1.150	2.150	3.150	-.015	-.027	-.049	.531	.504	.460
89	1.150	2.150	3.150	.007	-.021	-.043	.569	.541	.494
91	1.150	2.150	3.150	.011	-.013	-.037	.607	.577	.527
93	1.150	2.150	3.150	.021	-.004	-.030	.643	.611	.559
95	1.150	2.150	3.150	.033	.014	-.021	.677	.645	.590
97	1.150	2.150	3.150	.045	.027	-.011	.711	.677	.619
99	1.150	2.150	3.150	.057	.039	.000	.743	.707	.648
101	1.150	2.150	3.150	.070	.052	.021	.774	.737	.675
103	1.150	2.150	3.150	.083	.059	.032	.804	.765	.702
105	1.150	2.150	3.150	.097	.077	.044	.832	.793	.727
107	1.150	2.150	3.150	.110	.090	.056	.859	.819	.751
109	1.150	2.150	3.150	.124	.103	.069	.885	.843	.774
111	1.150	2.150	3.150	.138	.115	.081	.910	.867	.796
113	1.150	2.150	3.150	.151	.127	.093	.936	.892	.838
115	1.150	2.150	3.150	.165	.142	.105	.967	.932	.857
117	1.150	2.150	3.150	.177	.155	.117	.992	.952	.876
119	1.150	2.150	3.150	.190	.167	.129	1.017	.971	.895

UCT

[illegible]

2	2.750	2.750	3.000	.170	.171	.153	1.000	.931	
3	2.750	2.750	3.000	.169	.168	.152	.997	.943	
4	2.750	2.750	3.000	.167	.166	.151	.994	.938	
5	2.750	2.750	3.000	.165	.164	.149	.991	.935	
6	2.750	2.750	3.000	.163	.162	.147	.987	.932	
7	2.750	2.750	3.000	.161	.160	.145	.984	.929	
8	2.750	2.750	3.000	.159	.158	.143	.981	.926	
9	2.750	2.750	3.000	.157	.156	.141	.978	.923	
10	2.750	2.750	3.000	.155	.154	.139	.975	.920	
11	2.750	2.750	3.000	.153	.152	.137	.972	.917	
12	2.750	2.750	3.000	.151	.150	.135	.969	.914	
13	2.750	2.750	3.000	.149	.148	.133	.966	.911	
14	2.750	2.750	3.000	.147	.146	.131	.963	.908	
15	2.750	2.750	3.000	.145	.144	.129	.960	.905	
16	2.750	2.750	3.000	.143	.142	.127	.957	.902	
17	2.750	2.750	3.000	.141	.140	.125	.954	.899	
18	2.750	2.750	3.000	.139	.138	.123	.951	.896	
19	2.750	2.750	3.000	.137	.136	.121	.948	.893	
20	2.750	2.750	3.000	.135	.134	.119	.945	.890	
21	2.750	2.750	3.000	.133	.132	.117	.942	.887	
22	2.750	2.750	3.000	.131	.130	.115	.939	.884	
23	2.750	2.750	3.000	.129	.128	.113	.936	.881	
24	2.750	2.750	3.000	.127	.126	.111	.933	.878	
25	2.750	2.750	3.000	.125	.124	.109	.930	.875	
26	2.750	2.750	3.000	.123	.122	.107	.927	.872	
27	2.750	2.750	3.000	.121	.120	.105	.924	.869	
28	2.750	2.750	3.000	.119	.118	.103	.921	.866	
29	2.750	2.750	3.000	.117	.116	.101	.918	.863	
30	2.750	2.750	3.000	.115	.114	.099	.915	.860	
31	2.750	2.750	3.000	.113	.112	.097	.912	.857	
32	2.750	2.750	3.000	.111	.110	.095	.909	.854	
33	2.750	2.750	3.000	.109	.108	.093	.906	.851	
34	2.750	2.750	3.000	.107	.106	.091	.903	.848	
35	2.750	2.750	3.000	.105	.104	.089	.900	.845	
36	2.750	2.750	3.000	.103	.102	.087	.897	.842	
37	2.750	2.750	3.000	.101	.100	.085	.894	.839	
38	2.750	2.750	3.000	.099	.098	.083	.891	.836	
39	2.750	2.750	3.000	.097	.096	.081	.888	.833	
40	2.750	2.750	3.000	.095	.094	.079	.885	.830	
41	2.750	2.750	3.000	.093	.092	.077	.882	.827	
42	2.750	2.750	3.000	.091	.090	.075	.879	.824	
43	2.750	2.750	3.000	.089	.088	.073	.876	.821	
44	2.750	2.750	3.000	.087	.086	.071	.873	.818	
45	2.750	2.750	3.000	.085	.084	.069	.870	.815	
46	2.750	2.750	3.000	.083	.082	.067	.867	.812	
47	2.750	2.750	3.000	.081	.080	.065	.864	.809	
48	2.750	2.750	3.000	.079	.078	.063	.861	.806	
49	2.750	2.750	3.000	.077	.076	.061	.858	.803	
50	2.750	2.750	3.000	.075	.074	.059	.855	.800	
51	2.750	2.750	3.000	.073	.072	.057	.852	.797	
52	2.750	2.750	3.000	.071	.070	.055	.849	.794	
53	2.750	2.750	3.000	.069	.068	.053	.846	.791	
54	2.750	2.750	3.000	.067	.066	.051	.843	.788	
55	2.750	2.750	3.000	.065	.064	.049	.840	.785	
56	2.750	2.750	3.000	.063	.062	.047	.837	.782	
57	2.750	2.750	3.000	.061	.060	.045	.834	.779	
58	2.750	2.750	3.000	.059	.058	.043	.831	.776	
59	2.750	2.750	3.000	.057	.056	.041	.828	.773	
60	2.750	2.750	3.000	.055	.054	.039	.825	.770	
61	2.750	2.750	3.000	.053	.052	.037	.822	.767	
62	2.750	2.750	3.000	.051	.050	.035	.819	.764	
63	2.750	2.750	3.000	.049	.048	.033	.816	.761	
64	2.750	2.750	3.000	.047	.046	.031	.813	.758	
65	2.750	2.750	3.000	.045	.044	.029	.810	.755	
66	2.750	2.750	3.000	.043	.042	.027	.807	.752	
67	2.750	2.750	3.000	.041	.040	.025	.804	.749	
68	2.750	2.750	3.000	.039	.038	.023	.801	.746	
69	2.750	2.750	3.000	.037	.036	.021	.798	.743	
70	2.750	2.750	3.000	.035	.034	.019	.795	.740	
71	2.750	2.750	3.000	.033	.032	.017	.792	.737	
72	2.750	2.750	3.000	.031	.030	.015	.789	.734	
73	2.750	2.750	3.000	.029	.028	.013	.786	.731	
74	2.750	2.750	3.000	.027	.026	.011	.783	.728	
75	2.750	2.750	3.000	.025	.024	.009	.780	.725	
76	2.750	2.750	3.000	.023	.022	.007	.777	.722	
77	2.750	2.750	3.000	.021	.020	.005	.774	.719	
78	2.750	2.750	3.000	.019	.018	.003	.771	.716	
79	2.750	2.750	3.000	.017	.016	.001	.768	.713	
80	2.750	2.750	3.000	.015	.014	.000	.765	.710	
81	2.750	2.750	3.000	.013	.012	.000	.762	.707	
82	2.750	2.750	3.000	.011	.010	.000	.759	.704	
83	2.750	2.750	3.000	.009	.008	.000	.756	.701	
84	2.750	2.750	3.000	.007	.006	.000	.753	.698	
85	2.750	2.750	3.000	.005	.004	.000	.750	.695	
86	2.750	2.750	3.000	.003	.002	.000	.747	.692	
87	2.750	2.750	3.000	.001	.000	.000	.744	.689	
88	2.750	2.750	3.000	.000	.000	.000	.741	.686	
89	2.750	2.750	3.000	.000	.000	.000	.738	.683	
90	2.750	2.750	3.000	.000	.000	.000	.735	.680	
91	2.750	2.750	3.000	.000	.000	.000	.732	.677	
92	2.750	2.750	3.000	.000	.000	.000	.729	.674	
93	2.750	2.750	3.000	.000	.000	.000	.726	.671	
94	2.750	2.750	3.000	.000	.000	.000	.723	.668	
95	2.750	2.750	3.000	.000	.000	.000	.720	.665	
96	2.750	2.750	3.000	.000	.000	.000	.717	.662	
97	2.750	2.750	3.000	.000	.000	.000	.714	.659	
98	2.750	2.750	3.000	.000	.000	.000	.711	.656	
99	2.750	2.750	3.000	.000	.000	.000	.708	.653	
100	2.750	2.750	3.000	.000	.000	.000	.705	.650	

1	2.750	2.750	3.100	.170	.182	.198	1.055	1.011	.938
2	2.750	2.750	3.100	.169	.181	.196	1.049	1.007	.934
3	2.750	2.750	3.100	.168	.180	.195	1.043	1.001	.929
4	2.750	2.750	3.100	.167	.179	.194	1.037	.995	.924
5	2.750	2.750	3.100	.166	.178	.193	1.031	.989	.919
6	2.750	2.750	3.100	.165	.177	.192	1.025	.983	.914
7	2.750	2.750	3.100	.164	.176	.191	1.019	.977	.909
8	2.750	2.750	3.100	.163	.175	.190	1.013	.971	.904
9	2.750	2.750	3.100	.162	.174	.189	1.007	.965	.899
10	2.750	2.750	3.100	.161	.173	.188	1.001	.959	.894
11	2.750	2.750	3.100	.160	.172	.187	.995	.953	.889
12	2.750	2.750	3.100	.159	.171	.186	.989	.947	.884
13	2.750	2.750	3.100	.158	.170	.185	.983	.941	.879
14	2.750	2.750	3.100	.157	.169	.184	.977	.935	.874
15	2.750	2.750	3.100	.156	.168	.183	.971	.929	.869
16	2.750	2.750	3.100	.155	.167	.182	.965	.923	.864
17	2.750	2.750	3.100	.154	.166	.181	.959	.917	.859
18	2.750	2.750	3.100	.153	.165	.180	.953	.911	.854
19	2.750	2.750	3.100	.152	.164	.179	.947	.905	.849
20	2.750	2.750	3.100	.151	.163	.178	.941	.900	.844
21	2.750	2.750	3.100	.150	.162	.177	.935	.894	.839
22	2.750	2.750	3.100	.149	.161	.176	.929	.888	.834
23	2.750	2.750	3.100	.148	.160	.175	.923	.882	.829
24	2.750	2.750	3.100	.147	.159	.174	.917	.876	.824
25	2.750	2.750	3.100	.146	.158	.173	.911	.870	.819
26	2.750	2.750	3.100	.145	.157	.172	.905	.864	.814
27	2.750	2.750	3.100	.144	.156	.171	.899	.858	.809
28	2.750	2.750	3.100	.143	.155	.170	.893	.852	.804
29	2.750	2.750	3.100	.142	.154	.169	.887	.846	.799
30	2.750	2.750	3.100	.141	.153	.168	.881	.840	.794
31	2.750	2.750	3.100	.140	.152	.167	.875	.834	.789
32	2.750	2.750	3.100	.139	.151	.166	.869	.828	.784
33	2.750	2.750	3.100	.138	.150	.165	.863	.822	.779
34	2.750	2.750	3.100	.137	.149	.164	.857	.816	.774
35	2.750	2.750	3.100	.136	.148	.163	.851	.810	.769
36	2.750	2.750	3.100	.135	.147	.162	.845	.804	.764
37	2.750	2.750	3.100	.134	.146	.161	.839	.798	.759
38	2.750	2.750	3.100	.133	.145	.160	.833	.792	.754
39	2.750	2.750	3.100	.132	.144	.159	.827	.786	.749
40	2.750	2.750	3.100	.131	.143	.158	.821	.780	.744
41	2.750	2.750	3.100	.130	.142	.157	.815	.774	.739
42	2.750	2.750	3.100	.129	.141	.156	.809	.768	.734
43	2.750	2.750	3.100	.128	.140	.155	.803	.762	.729
44	2.750	2.750	3.100	.127	.139	.154	.797	.756	.724
45	2.750	2.750	3.100	.126	.138	.153	.791	.750	.719
46	2.750	2.750	3.100	.125	.137	.152	.785	.744	.714
47	2.750	2.750	3.100	.124	.136	.151	.779	.738	.709
48	2.750	2.750	3.100	.123	.135	.150	.773	.732	.704
49	2.750	2.750	3.100	.122	.134	.149	.767	.726	.699
50	2.750	2.750	3.100	.121	.133	.148	.761	.720	.694
51	2.750	2.750	3.100	.120	.132	.147	.755	.714	.689
52	2.750	2.750	3.100	.119	.131	.146	.749	.708	.684
53	2.750	2.750	3.100	.118	.130	.145	.743	.702	.679
54	2.750	2.750	3.100	.117	.129	.144	.737	.696	.674
55	2.750	2.750	3.100	.116	.128	.143	.731	.690	.669
56	2.750	2.750	3.100	.115	.127	.142	.725	.684	.664
57	2.750	2.750	3.100	.114	.126	.141	.719	.678	.659
58	2.750	2.750	3.100	.113	.125	.140	.713	.672	.654
59	2.750	2.750	3.100	.112	.124	.139	.707	.666	.649
60	2.750	2.750	3.100	.111	.123	.138	.701	.660	.644
61	2.750	2.750	3.100	.110	.122	.137	.695	.654	.639
62	2.750	2.750	3.100	.109	.121	.136	.689	.648	.634

1	2.25	.13	4.300	.12	.013	.019	.126	.087	.023
5	1.95	.20	4.300	-.010	-.012	-.015	-.010	-.012	-.015
6	1.95	.20	4.300	-.011	-.012	-.011	-.012	-.023	-.025
7	1.95	.20	4.300	-.010	-.036	-.045	-.020	-.034	-.040
8	1.95	.20	4.300	-.010	-.047	-.054	-.037	-.044	-.056
9	1.95	.20	4.300	-.017	-.056	-.072	-.044	-.053	-.069
10	1.95	.20	4.300	-.010	-.055	-.063	-.050	-.061	-.079
11	1.95	.20	4.300	-.010	-.072	-.093	-.055	-.068	-.089
12	1.95	.20	4.300	-.013	-.078	-.102	-.059	-.073	-.097
13	1.95	.20	4.300	-.016	-.082	-.109	-.060	-.077	-.103
14	1.95	.20	4.300	-.017	-.089	-.114	-.061	-.079	-.108
15	1.95	.20	4.300	-.016	-.095	-.117	-.060	-.079	-.111
16	1.95	.20	4.300	-.019	-.095	-.119	-.057	-.078	-.112
17	1.95	.20	4.300	-.011	-.093	-.117	-.053	-.075	-.112
18	1.95	.20	4.300	-.016	-.079	-.118	-.050	-.071	-.111
19	1.95	.20	4.300	-.010	-.074	-.115	-.041	-.066	-.108
20	1.95	.20	4.300	-.012	-.050	-.111	-.034	-.060	-.103
21	1.95	.20	4.300	-.014	-.051	-.106	-.025	-.052	-.098
22	1.95	.20	4.300	-.014	-.053	-.100	-.015	-.044	-.091
23	1.95	.20	4.300	-.011	-.044	-.092	-.005	-.034	-.084
24	1.95	.20	4.300	-.013	-.034	-.086	-.004	-.024	-.075
25	1.95	.20	4.300	.003	-.023	-.076	.018	-.014	-.066
26	1.95	.20	4.300	.010	-.012	-.053	.030	-.003	-.057
27	1.95	.20	4.300	.012	-.001	-.056	.042	.009	-.047
28	1.95	.20	4.300	.015	.011	-.046	.055	.021	-.036
29	1.95	.20	4.300	.017	.023	-.036	.068	.033	-.026
30	1.95	.20	4.300	.070	.035	-.025	.081	.045	-.015
31	1.95	.20	4.300	.013	.047	-.014	.094	.057	-.004
32	1.95	.20	4.300	.070	.059	-.003	.107	.070	.007
33	1.95	.20	4.300	.107	.071	.000	.120	.082	.019
34	1.95	.20	4.300	.121	.083	.019	.132	.094	.030
35	1.95	.30	4.300	-.010	-.012	-.015	-.009	-.011	-.014
36	1.95	.30	4.300	-.021	-.024	-.030	-.018	-.022	-.028
37	1.95	.30	4.300	-.000	-.005	-.015	-.026	-.032	-.041
38	1.95	.30	4.300	-.019	-.016	-.030	-.034	-.041	-.054
39	1.95	.30	4.300	-.017	-.006	-.021	-.041	-.050	-.065
40	1.95	.30	4.300	-.014	-.004	-.002	-.046	-.057	-.075
41	1.95	.30	4.300	-.019	-.012	-.012	-.050	-.063	-.084
42	1.95	.30	4.300	-.013	-.017	-.011	-.053	-.068	-.092
43	1.95	.30	4.300	-.003	-.011	-.003	-.055	-.071	-.097
44	1.95	.30	4.300	-.004	-.013	-.013	-.056	-.072	-.102
45	1.95	.30	4.300	-.005	-.005	-.016	-.053	-.072	-.104
46	1.95	.30	4.300	-.004	-.004	-.018	-.050	-.071	-.105
47	1.95	.30	4.300	-.000	-.002	-.010	-.046	-.068	-.105
48	1.95	.30	4.300	-.005	-.008	-.017	-.040	-.064	-.103
49	1.95	.30	4.300	-.017	-.014	-.014	-.033	-.058	-.099
50	1.95	.30	4.300	-.012	-.015	-.010	-.025	-.051	-.095
51	1.95	.30	4.300	-.013	-.000	-.005	-.016	-.044	-.089
52	1.95	.30	4.300	-.029	-.002	-.009	-.007	-.035	-.082
53	1.95	.30	4.300	-.011	-.013	-.012	.004	-.025	-.074
54	1.95	.30	4.300	-.013	-.013	-.014	.015	-.015	-.066
55	1.95	.30	4.300	.004	-.023	-.025	.027	-.004	-.057
56	1.95	.30	4.300	.020	-.012	-.003	.039	.007	-.047
57	1.95	.30	4.300	.012	-.001	-.003	.052	.019	-.037
58	1.95	.30	4.300	.015	.011	-.016	.065	.030	-.027
59	1.95	.30	4.300	.007	.023	-.015	.078	.043	-.016
60	1.95	.30	4.300	.010	.005	-.024	.091	.055	-.005
61	1.95	.30	4.300	.013	.017	-.019	.104	.067	.006
62	1.95	.30	4.300	.015	.015	-.017	.117	.079	.017

LIST

3									
5	1.150	.400	9.100	-.010	-.012	-.015	-.018	-.019	-.020
7	1.200	.400	9.200	-.010	-.012	-.015	-.018	-.019	-.020
9	1.250	.400	9.300	-.010	-.012	-.015	-.018	-.019	-.020
11	1.300	.400	9.400	-.010	-.012	-.015	-.018	-.019	-.020
13	1.350	.400	9.500	-.010	-.012	-.015	-.018	-.019	-.020
15	1.400	.400	9.600	-.010	-.012	-.015	-.018	-.019	-.020
17	1.450	.400	9.700	-.010	-.012	-.015	-.018	-.019	-.020
19	1.500	.400	9.800	-.010	-.012	-.015	-.018	-.019	-.020
21	1.550	.400	9.900	-.010	-.012	-.015	-.018	-.019	-.020
23	1.600	.400	10.000	-.010	-.012	-.015	-.018	-.019	-.020
25	1.650	.400	10.100	-.010	-.012	-.015	-.018	-.019	-.020
27	1.700	.400	10.200	-.010	-.012	-.015	-.018	-.019	-.020
29	1.750	.400	10.300	-.010	-.012	-.015	-.018	-.019	-.020
31	1.800	.400	10.400	-.010	-.012	-.015	-.018	-.019	-.020
33	1.850	.400	10.500	-.010	-.012	-.015	-.018	-.019	-.020
35	1.900	.400	10.600	-.010	-.012	-.015	-.018	-.019	-.020
37	1.950	.400	10.700	-.010	-.012	-.015	-.018	-.019	-.020
39	2.000	.400	10.800	-.010	-.012	-.015	-.018	-.019	-.020
41	2.050	.400	10.900	-.010	-.012	-.015	-.018	-.019	-.020
43	2.100	.400	11.000	-.010	-.012	-.015	-.018	-.019	-.020
45	2.150	.400	11.100	-.010	-.012	-.015	-.018	-.019	-.020
47	2.200	.400	11.200	-.010	-.012	-.015	-.018	-.019	-.020
49	2.250	.400	11.300	-.010	-.012	-.015	-.018	-.019	-.020
51	2.300	.400	11.400	-.010	-.012	-.015	-.018	-.019	-.020
53	2.350	.400	11.500	-.010	-.012	-.015	-.018	-.019	-.020
55	2.400	.400	11.600	-.010	-.012	-.015	-.018	-.019	-.020
57	2.450	.400	11.700	-.010	-.012	-.015	-.018	-.019	-.020
59	2.500	.400	11.800	-.010	-.012	-.015	-.018	-.019	-.020
61	2.550	.400	11.900	-.010	-.012	-.015	-.018	-.019	-.020
63	2.600	.400	12.000	-.010	-.012	-.015	-.018	-.019	-.020

LIST

1	1.750	.500	4.000	.119	.012	.028	.171	.133	.069
3	1.750	.500	4.000	-.112	-.012	-.015	-.086	-.008	-.011
5	1.750	.500	4.000	-.023	-.023	-.029	-.011	-.015	-.021
7	1.750	.500	4.000	-.027	-.034	-.043	-.016	-.022	-.031
9	1.750	.500	4.000	-.037	-.047	-.056	-.021	-.028	-.040
11	1.750	.500	4.000	-.045	-.054	-.068	-.024	-.033	-.049
13	1.750	.500	4.000	-.051	-.062	-.079	-.027	-.038	-.056
15	1.750	.500	4.000	-.057	-.069	-.089	-.030	-.041	-.062
17	1.750	.500	4.000	-.061	-.074	-.097	-.032	-.043	-.066
19	1.750	.500	4.000	-.063	-.078	-.103	-.034	-.043	-.070
21	1.750	.500	4.000	-.064	-.081	-.108	-.035	-.043	-.072
23	1.750	.500	4.000	-.063	-.081	-.112	-.032	-.041	-.072
25	1.750	.500	4.000	-.061	-.081	-.114	-.031	-.037	-.071
27	1.750	.500	4.000	-.058	-.079	-.114	-.031	-.033	-.069
29	1.750	.500	4.000	-.053	-.075	-.113	-.030	-.027	-.065
31	1.750	.500	4.000	-.047	-.071	-.110	-.030	-.020	-.060
33	1.750	.500	4.000	-.040	-.065	-.106	-.034	-.012	-.055
35	1.750	.500	4.000	-.032	-.059	-.101	-.034	-.003	-.048
37	1.750	.500	4.000	-.023	-.050	-.095	-.035	-.007	-.040
39	1.750	.500	4.000	-.013	-.041	-.088	-.036	-.017	-.031
41	1.750	.500	4.000	-.003	-.032	-.080	-.036	-.028	-.022
43	2.250	.500	4.000	.003	-.022	-.072	-.031	-.040	-.012
45	2.250	.500	4.000	.026	-.011	-.063	-.034	-.052	-.002
47	2.250	.500	4.000	.031	-.008	-.053	-.037	-.064	.009
49	2.250	.500	4.000	.044	.011	-.043	-.040	-.076	.020
51	2.250	.500	4.000	.055	.023	-.033	-.043	-.089	.031
53	2.250	.500	4.000	.063	.035	-.023	-.043	-.101	.042
55	2.250	.500	4.000	.061	.048	-.012	-.040	-.114	.054
57	2.250	.500	4.000	.045	.038	-.001	-.033	-.126	.065
59	2.250	.500	4.000	.026	.026	.009	-.026	-.139	.076
61	2.250	.500	4.000	.013	.031	.020	-.019	-.151	.088
63	2.250	.500	4.000	-.010	-.012	-.014	-.004	-.096	-.009
65	2.250	.500	4.000	-.019	-.023	-.024	-.000	-.012	-.018
67	2.250	.500	4.000	-.027	-.034	-.032	-.012	-.017	-.027
69	2.250	.500	4.000	-.037	-.044	-.045	-.015	-.022	-.034
71	2.250	.500	4.000	-.044	-.053	-.057	-.017	-.026	-.041
73	2.250	.500	4.000	-.050	-.061	-.069	-.019	-.029	-.047
75	2.250	.500	4.000	-.055	-.067	-.077	-.021	-.031	-.052
77	2.250	.500	4.000	-.059	-.073	-.085	-.023	-.032	-.055
79	2.250	.500	4.000	-.062	-.077	-.091	-.026	-.032	-.053
81	2.250	.500	4.000	-.063	-.079	-.096	-.028	-.030	-.059
83	2.250	.500	4.000	-.062	-.080	-.100	-.030	-.027	-.058
85	2.250	.500	4.000	-.060	-.079	-.101	-.032	-.023	-.056
87	2.250	.500	4.000	-.057	-.077	-.102	-.034	-.017	-.053
89	2.250	.500	4.000	-.052	-.074	-.100	-.031	-.011	-.049
91	2.250	.500	4.000	-.046	-.070	-.098	-.021	-.003	-.043
93	2.250	.500	4.000	-.039	-.064	-.094	-.013	.006	-.037
95	2.250	.500	4.000	-.032	-.057	-.089	-.004	.015	-.030
97	2.250	.500	4.000	-.023	-.049	-.083	.003	.025	-.021
99	2.250	.500	4.000	-.013	-.041	-.076	.006	.036	-.012
101	2.250	.500	4.000	.003	-.031	-.067	.007	.047	-.003
103	2.250	.500	4.000	.021	-.021	-.057	.009	.059	.007
105	2.250	.500	4.000	.042	-.011	-.047	.013	.071	.018
107	2.250	.500	4.000	.063	-.000	-.036	.016	.084	.029
109	2.250	.500	4.000	.083	.011	-.024	.019	.096	.040
111	2.250	.500	4.000	.103	.023	-.012	.043	.109	.051
113	2.250	.500	4.000	.122	.034	-.001	.057	.122	.063
115	2.250	.500	4.000	.143	.048	.011	.070	.134	.074
117	2.250	.500	4.000	.162	.067	.021	.084	.147	.086

[illegible]

1	2.05	1.10	4.000	.111	.70	.023	.309	.272	.210
2	2.10	1.10	4.000	.112	.70	.023	.309	.272	.210
3	2.15	1.10	4.000	.113	.70	.023	.309	.272	.210
4	2.20	1.10	4.000	.114	.70	.023	.309	.272	.210
5	2.25	1.10	4.000	.115	.70	.023	.309	.272	.210
6	2.30	1.10	4.000	.116	.70	.023	.309	.272	.210
7	2.35	1.10	4.000	.117	.70	.023	.309	.272	.210
8	2.40	1.10	4.000	.118	.70	.023	.309	.272	.210
9	2.45	1.10	4.000	.119	.70	.023	.309	.272	.210
10	2.50	1.10	4.000	.120	.70	.023	.309	.272	.210
11	2.55	1.10	4.000	.121	.70	.023	.309	.272	.210
12	2.60	1.10	4.000	.122	.70	.023	.309	.272	.210
13	2.65	1.10	4.000	.123	.70	.023	.309	.272	.210
14	2.70	1.10	4.000	.124	.70	.023	.309	.272	.210
15	2.75	1.10	4.000	.125	.70	.023	.309	.272	.210
16	2.80	1.10	4.000	.126	.70	.023	.309	.272	.210
17	2.85	1.10	4.000	.127	.70	.023	.309	.272	.210
18	2.90	1.10	4.000	.128	.70	.023	.309	.272	.210
19	2.95	1.10	4.000	.129	.70	.023	.309	.272	.210
20	3.00	1.10	4.000	.130	.70	.023	.309	.272	.210
21	3.05	1.10	4.000	.131	.70	.023	.309	.272	.210
22	3.10	1.10	4.000	.132	.70	.023	.309	.272	.210
23	3.15	1.10	4.000	.133	.70	.023	.309	.272	.210
24	3.20	1.10	4.000	.134	.70	.023	.309	.272	.210
25	3.25	1.10	4.000	.135	.70	.023	.309	.272	.210
26	3.30	1.10	4.000	.136	.70	.023	.309	.272	.210
27	3.35	1.10	4.000	.137	.70	.023	.309	.272	.210
28	3.40	1.10	4.000	.138	.70	.023	.309	.272	.210
29	3.45	1.10	4.000	.139	.70	.023	.309	.272	.210
30	3.50	1.10	4.000	.140	.70	.023	.309	.272	.210
31	3.55	1.10	4.000	.141	.70	.023	.309	.272	.210
32	3.60	1.10	4.000	.142	.70	.023	.309	.272	.210
33	3.65	1.10	4.000	.143	.70	.023	.309	.272	.210
34	3.70	1.10	4.000	.144	.70	.023	.309	.272	.210
35	3.75	1.10	4.000	.145	.70	.023	.309	.272	.210
36	3.80	1.10	4.000	.146	.70	.023	.309	.272	.210
37	3.85	1.10	4.000	.147	.70	.023	.309	.272	.210
38	3.90	1.10	4.000	.148	.70	.023	.309	.272	.210
39	3.95	1.10	4.000	.149	.70	.023	.309	.272	.210
40	4.00	1.10	4.000	.150	.70	.023	.309	.272	.210
41	4.05	1.10	4.000	.151	.70	.023	.309	.272	.210
42	4.10	1.10	4.000	.152	.70	.023	.309	.272	.210
43	4.15	1.10	4.000	.153	.70	.023	.309	.272	.210
44	4.20	1.10	4.000	.154	.70	.023	.309	.272	.210
45	4.25	1.10	4.000	.155	.70	.023	.309	.272	.210
46	4.30	1.10	4.000	.156	.70	.023	.309	.272	.210
47	4.35	1.10	4.000	.157	.70	.023	.309	.272	.210
48	4.40	1.10	4.000	.158	.70	.023	.309	.272	.210
49	4.45	1.10	4.000	.159	.70	.023	.309	.272	.210
50	4.50	1.10	4.000	.160	.70	.023	.309	.272	.210
51	4.55	1.10	4.000	.161	.70	.023	.309	.272	.210
52	4.60	1.10	4.000	.162	.70	.023	.309	.272	.210
53	4.65	1.10	4.000	.163	.70	.023	.309	.272	.210
54	4.70	1.10	4.000	.164	.70	.023	.309	.272	.210
55	4.75	1.10	4.000	.165	.70	.023	.309	.272	.210
56	4.80	1.10	4.000	.166	.70	.023	.309	.272	.210
57	4.85	1.10	4.000	.167	.70	.023	.309	.272	.210
58	4.90	1.10	4.000	.168	.70	.023	.309	.272	.210
59	4.95	1.10	4.000	.169	.70	.023	.309	.272	.210
60	5.00	1.10	4.000	.170	.70	.023	.309	.272	.210
61	5.05	1.10	4.000	.171	.70	.023	.309	.272	.210
62	5.10	1.10	4.000	.172	.70	.023	.309	.272	.210
63	5.15	1.10	4.000	.173	.70	.023	.309	.272	.210
64	5.20	1.10	4.000	.174	.70	.023	.309	.272	.210
65	5.25	1.10	4.000	.175	.70	.023	.309	.272	.210
66	5.30	1.10	4.000	.176	.70	.023	.309	.272	.210
67	5.35	1.10	4.000	.177	.70	.023	.309	.272	.210
68	5.40	1.10	4.000	.178	.70	.023	.309	.272	.210
69	5.45	1.10	4.000	.179	.70	.023	.309	.272	.210
70	5.50	1.10	4.000	.180	.70	.023	.309	.272	.210
71	5.55	1.10	4.000	.181	.70	.023	.309	.272	.210
72	5.60	1.10	4.000	.182	.70	.023	.309	.272	.210
73	5.65	1.10	4.000	.183	.70	.023	.309	.272	.210
74	5.70	1.10	4.000	.184	.70	.023	.309	.272	.210
75	5.75	1.10	4.000	.185	.70	.023	.309	.272	.210
76	5.80	1.10	4.000	.186	.70	.023	.309	.272	.210
77	5.85	1.10	4.000	.187	.70	.023	.309	.272	.210
78	5.90	1.10	4.000	.188	.70	.023	.309	.272	.210
79	5.95	1.10	4.000	.189	.70	.023	.309	.272	.210
80	6.00	1.10	4.000	.190	.70	.023	.309	.272	.210
81	6.05	1.10	4.000	.191	.70	.023	.309	.272	.210
82	6.10	1.10	4.000	.192	.70	.023	.309	.272	.210
83	6.15	1.10	4.000	.193	.70	.023	.309	.272	.210
84	6.20	1.10	4.000	.194	.70	.023	.309	.272	.210
85	6.25	1.10	4.000	.195	.70	.023	.309	.272	.210
86	6.30	1.10	4.000	.196	.70	.023	.309	.272	.210
87	6.35	1.10	4.000	.197	.70	.023	.309	.272	.210
88	6.40	1.10	4.000	.198	.70	.023	.309	.272	.210
89	6.45	1.10	4.000	.199	.70	.023	.309	.272	.210
90	6.50	1.10	4.000	.200	.70	.023	.309	.272	.210
91	6.55	1.10	4.000	.201	.70	.023	.309	.272	.210
92	6.60	1.10	4.000	.202	.70	.023	.309	.272	.210
93	6.65	1.10	4.000	.203	.70	.023	.309	.272	.210
94	6.70	1.10	4.000	.204	.70	.023	.309	.272	.210
95	6.75	1.10	4.000	.205	.70	.023	.309	.272	.210
96	6.80	1.10	4.000	.206	.70	.023	.309	.272	.210
97	6.85	1.10	4.000	.207	.70	.023	.309	.272	.210
98	6.90	1.10	4.000	.208	.70	.023	.309	.272	.210
99	6.95	1.10	4.000	.209	.70	.023	.309	.272	.210
100	7.00	1.10	4.000	.210	.70	.023	.309	.272	.210

UICF

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3	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
5	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
7	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
9	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
11	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
13	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
15	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
17	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
19	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
21	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
23	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
25	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
27	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
29	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
31	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
33	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
35	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
37	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
39	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
41	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
43	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
45	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
47	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
49	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
51	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
53	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
55	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
57	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
59	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
61	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000
63	2.250	4.100	4.100	-.000	-.000	-.000	-.000	-.000

UCT

[illegible]

1	2.150	4.150	9.150	-.007	-.013	-.013	.025	.032	.037
2	2.150	4.150	9.150	-.005	-.010	-.010	.023	.022	.019
3	2.150	4.150	9.150	-.005	-.011	-.011	.027	.022	.035
4	2.150	4.150	9.150	-.011	-.017	-.021	.020	.066	.058
5	2.150	4.150	9.150	-.013	-.022	-.027	.021	.033	.078
6	2.150	4.150	9.150	-.022	-.026	-.033	.117	.109	.097
7	2.150	4.150	9.150	-.035	-.039	-.038	.120	.131	.117
8	2.150	4.150	9.150	-.026	-.033	-.043	.103	.155	.136
9	2.150	4.150	9.150	-.022	-.030	-.047	.186	.175	.155
10	2.150	4.150	9.150	-.031	-.036	-.050	.208	.196	.174
11	2.150	4.150	9.150	-.031	-.039	-.054	.231	.217	.193
12	2.150	4.150	9.150	-.031	-.040	-.054	.253	.238	.212
13	2.150	4.150	9.150	-.029	-.039	-.055	.275	.259	.231
14	2.150	4.150	9.150	-.026	-.030	-.055	.277	.280	.250
15	2.150	4.150	9.150	-.025	-.036	-.054	.319	.300	.268
16	2.150	4.150	9.150	-.021	-.033	-.053	.340	.320	.267
17	2.150	4.150	9.150	-.017	-.045	-.054	.361	.340	.305
18	2.150	4.150	9.150	-.013	-.030	-.047	.382	.360	.323
19	2.150	4.150	9.150	-.012	-.021	-.044	.402	.379	.340
20	2.150	4.150	9.150	-.001	-.015	-.039	.422	.398	.357
21	2.150	4.150	9.150	.005	-.010	-.034	.441	.416	.374
22	2.150	4.150	9.150	.012	-.003	-.029	.460	.434	.391
23	2.150	4.150	9.150	.019	.003	-.023	.479	.452	.407
24	2.150	4.150	9.150	.027	.010	-.017	.497	.469	.423
25	2.150	4.150	9.150	.034	.016	-.010	.515	.486	.438
26	2.150	4.150	9.150	.040	.023	-.013	.531	.502	.453
27	2.150	4.150	9.150	.043	.033	-.011	.543	.518	.468
28	2.150	4.150	9.150	.047	.041	-.011	.564	.534	.482
29	2.150	4.150	9.150	.050	.049	-.015	.585	.549	.496
30	2.150	4.150	9.150	.053	.050	-.026	.597	.563	.510
31	2.150	4.150	9.150	.055	.055	-.034	.610	.577	.523
32	2.150	4.150	9.150	-.015	-.009	-.007	.624	.624	.620
33	2.150	4.150	9.150	-.017	-.011	-.013	.632	.645	.641
34	2.150	4.150	9.150	-.017	-.016	-.020	.630	.668	.661
35	2.150	4.150	9.150	-.017	-.017	-.020	.637	.691	.682
36	2.150	4.150	9.150	-.020	-.020	-.021	.621	.614	.602
37	2.150	4.150	9.150	-.023	-.028	-.026	.605	.636	.622
38	2.150	4.150	9.150	-.026	-.031	-.031	.609	.659	.642
39	2.150	4.150	9.150	-.023	-.034	-.034	.612	.631	.662
40	2.150	4.150	9.150	-.029	-.030	-.037	.616	.603	.682
41	2.150	4.150	9.150	-.027	-.037	-.033	.629	.625	.632
42	2.150	4.150	9.150	-.027	-.037	-.031	.662	.662	.622
43	2.150	4.150	9.150	-.020	-.037	-.032	.685	.666	.641
44	2.150	4.150	9.150	-.025	-.035	-.032	.607	.690	.666
45	2.150	4.150	9.150	-.020	-.033	-.031	.629	.611	.679
46	2.150	4.150	9.150	-.020	-.031	-.039	.651	.631	.698
47	2.150	4.150	9.150	-.016	-.027	-.037	.672	.651	.617
48	2.150	4.150	9.150	-.014	-.023	-.035	.693	.671	.635
49	2.150	4.150	9.150	-.015	-.019	-.030	.614	.691	.653
50	2.150	4.150	9.150	-.010	-.014	-.036	.634	.610	.670
51	2.150	4.150	9.150	.006	-.005	-.031	.653	.629	.687
52	2.150	4.150	9.150	.012	-.002	-.026	.670	.647	.604
53	2.150	4.150	9.150	.019	.005	-.020	.691	.665	.621
54	2.150	4.150	9.150	.027	.011	-.014	.610	.682	.637
55	2.150	4.150	9.150	.034	.015	-.010	.627	.699	.652
56	2.150	4.150	9.150	.040	.020	-.001	.644	.616	.660
57	2.150	4.150	9.150	.050	.036	.006	.651	.632	.682
58	2.150	4.150	9.150	.057	.041	.013	.677	.647	.697
59	2.150	4.150	9.150	.067	.046	.020	.693	.662	.611
60	2.150	4.150	9.150	.075	.057	.027	.603	.677	.624

UCT

1	2.250	2.250	4.000	-.000	-.000	-.000	.023	.591	.537
2	2.250	2.250	4.000	-.000	-.000	-.000	.025	.024	.021
3	2.250	2.250	4.000	-.000	-.000	-.000	.027	.047	.043
4	2.250	2.250	4.000	-.012	-.015	-.010	.075	.071	.064
5	2.250	2.250	4.000	-.018	-.017	-.024	.100	.094	.085
6	2.250	2.250	4.000	-.019	-.023	-.024	.125	.110	.106
7	2.250	2.250	4.000	-.022	-.024	-.034	.149	.141	.127
8	2.250	2.250	4.000	-.024	-.029	-.036	.174	.164	.148
9	2.250	2.250	4.000	-.026	-.032	-.041	.198	.187	.169
10	2.250	2.250	4.000	-.027	-.033	-.044	.222	.210	.189
11	2.250	2.250	4.000	-.027	-.034	-.046	.246	.232	.210
12	2.250	2.250	4.000	-.027	-.035	-.048	.270	.255	.230
13	2.250	2.250	4.000	-.026	-.034	-.048	.293	.277	.250
14	2.250	2.250	4.000	-.029	-.033	-.048	.316	.298	.270
15	2.250	2.250	4.000	-.031	-.031	-.047	.338	.320	.289
16	2.250	2.250	4.000	-.031	-.028	-.046	.360	.341	.308
17	2.250	2.250	4.000	-.031	-.025	-.043	.382	.361	.327
18	2.250	2.250	4.000	-.030	-.021	-.041	.403	.382	.346
19	2.250	2.250	4.000	-.030	-.017	-.037	.424	.401	.364
20	2.250	2.250	4.000	-.030	-.012	-.033	.444	.421	.382
21	2.250	2.250	4.000	-.030	-.009	-.028	.464	.440	.399
22	2.250	2.250	4.000	-.030	-.001	-.020	.483	.458	.416
23	2.250	2.250	4.000	-.030	-.016	-.016	.502	.476	.433
24	2.250	2.250	4.000	-.027	-.012	-.012	.521	.494	.449
25	2.250	2.250	4.000	-.024	-.019	-.006	.539	.511	.465
26	2.250	2.250	4.000	-.026	-.026	-.001	.555	.527	.480
27	2.250	2.250	4.000	-.029	-.024	-.007	.573	.543	.495
28	2.250	2.250	4.000	-.037	-.041	-.014	.587	.559	.509
29	2.250	2.250	4.000	-.045	-.049	-.021	.605	.574	.523
30	2.250	2.250	4.000	-.053	-.056	-.028	.620	.589	.537
31	2.250	2.250	4.000	-.061	-.054	-.035	.635	.603	.550
32	2.250	2.250	4.000	-.064	-.055	-.036	.676	.624	.572
33	2.250	2.250	4.000	-.063	-.049	-.032	.651	.604	.554
34	2.250	2.250	4.000	-.062	-.044	-.027	.677	.623	.566
35	2.250	2.250	4.000	-.065	-.046	-.022	.693	.637	.588
36	2.250	2.250	4.000	-.063	-.041	-.027	.715	.651	.600
37	2.250	2.250	4.000	-.065	-.045	-.032	.735	.669	.615
38	2.250	2.250	4.000	-.068	-.048	-.034	.753	.687	.632
39	2.250	2.250	4.000	-.072	-.051	-.036	.770	.704	.648
40	2.250	2.250	4.000	-.075	-.053	-.037	.787	.721	.665
41	2.250	2.250	4.000	-.078	-.055	-.038	.803	.737	.681
42	2.250	2.250	4.000	-.082	-.057	-.039	.820	.754	.698
43	2.250	2.250	4.000	-.085	-.059	-.041	.836	.770	.714
44	2.250	2.250	4.000	-.088	-.061	-.042	.852	.786	.730
45	2.250	2.250	4.000	-.092	-.063	-.044	.868	.802	.746
46	2.250	2.250	4.000	-.095	-.065	-.045	.884	.818	.762
47	2.250	2.250	4.000	-.098	-.067	-.046	.900	.834	.778
48	2.250	2.250	4.000	-.102	-.069	-.047	.916	.850	.794
49	2.250	2.250	4.000	-.105	-.071	-.048	.932	.866	.810
50	2.250	2.250	4.000	-.108	-.073	-.049	.948	.882	.826
51	2.250	2.250	4.000	-.112	-.075	-.050	.964	.898	.842
52	2.250	2.250	4.000	-.115	-.077	-.051	.980	.914	.858
53	2.250	2.250	4.000	-.118	-.079	-.052	.996	.930	.874
54	2.250	2.250	4.000	-.122	-.081	-.053	.1012	.946	.890
55	2.250	2.250	4.000	-.125	-.083	-.054	.1028	.962	.906
56	2.250	2.250	4.000	-.128	-.085	-.055	.1044	.978	.922
57	2.250	2.250	4.000	-.132	-.087	-.056	.1060	.994	.938
58	2.250	2.250	4.000	-.135	-.089	-.057	.1076	.1010	.954
59	2.250	2.250	4.000	-.138	-.091	-.058	.1092	.1026	.970
60	2.250	2.250	4.000	-.142	-.093	-.059	.1108	.1042	.986
61	2.250	2.250	4.000	-.145	-.095	-.060	.1124	.1058	.1002
62	2.250	2.250	4.000	-.148	-.097	-.061	.1140	.1074	.1018
63	2.250	2.250	4.000	-.152	-.099	-.062	.1156	.1090	.1034

1	2.150	2.150	2.150	-.000	-.000	-.000	.000	.000	.000
2	2.150	2.150	2.150	-.001	-.001	-.001	.001	.001	.001
3	2.150	2.150	2.150	-.002	-.002	-.002	.002	.002	.002
4	2.150	2.150	2.150	-.003	-.003	-.003	.003	.003	.003
5	2.150	2.150	2.150	-.004	-.004	-.004	.004	.004	.004
6	2.150	2.150	2.150	-.005	-.005	-.005	.005	.005	.005
7	2.150	2.150	2.150	-.006	-.006	-.006	.006	.006	.006
8	2.150	2.150	2.150	-.007	-.007	-.007	.007	.007	.007
9	2.150	2.150	2.150	-.008	-.008	-.008	.008	.008	.008
10	2.150	2.150	2.150	-.009	-.009	-.009	.009	.009	.009
11	2.150	2.150	2.150	-.010	-.010	-.010	.010	.010	.010
12	2.150	2.150	2.150	-.011	-.011	-.011	.011	.011	.011
13	2.150	2.150	2.150	-.012	-.012	-.012	.012	.012	.012
14	2.150	2.150	2.150	-.013	-.013	-.013	.013	.013	.013
15	2.150	2.150	2.150	-.014	-.014	-.014	.014	.014	.014
16	2.150	2.150	2.150	-.015	-.015	-.015	.015	.015	.015
17	2.150	2.150	2.150	-.016	-.016	-.016	.016	.016	.016
18	2.150	2.150	2.150	-.017	-.017	-.017	.017	.017	.017
19	2.150	2.150	2.150	-.018	-.018	-.018	.018	.018	.018
20	2.150	2.150	2.150	-.019	-.019	-.019	.019	.019	.019
21	2.150	2.150	2.150	-.020	-.020	-.020	.020	.020	.020
22	2.150	2.150	2.150	-.021	-.021	-.021	.021	.021	.021
23	2.150	2.150	2.150	-.022	-.022	-.022	.022	.022	.022
24	2.150	2.150	2.150	-.023	-.023	-.023	.023	.023	.023
25	2.150	2.150	2.150	-.024	-.024	-.024	.024	.024	.024
26	2.150	2.150	2.150	-.025	-.025	-.025	.025	.025	.025
27	2.150	2.150	2.150	-.026	-.026	-.026	.026	.026	.026
28	2.150	2.150	2.150	-.027	-.027	-.027	.027	.027	.027
29	2.150	2.150	2.150	-.028	-.028	-.028	.028	.028	.028
30	2.150	2.150	2.150	-.029	-.029	-.029	.029	.029	.029
31	2.150	2.150	2.150	-.030	-.030	-.030	.030	.030	.030
32	2.150	2.150	2.150	-.031	-.031	-.031	.031	.031	.031
33	2.150	2.150	2.150	-.032	-.032	-.032	.032	.032	.032
34	2.150	2.150	2.150	-.033	-.033	-.033	.033	.033	.033
35	2.150	2.150	2.150	-.034	-.034	-.034	.034	.034	.034
36	2.150	2.150	2.150	-.035	-.035	-.035	.035	.035	.035
37	2.150	2.150	2.150	-.036	-.036	-.036	.036	.036	.036
38	2.150	2.150	2.150	-.037	-.037	-.037	.037	.037	.037
39	2.150	2.150	2.150	-.038	-.038	-.038	.038	.038	.038
40	2.150	2.150	2.150	-.039	-.039	-.039	.039	.039	.039
41	2.150	2.150	2.150	-.040	-.040	-.040	.040	.040	.040
42	2.150	2.150	2.150	-.041	-.041	-.041	.041	.041	.041
43	2.150	2.150	2.150	-.042	-.042	-.042	.042	.042	.042
44	2.150	2.150	2.150	-.043	-.043	-.043	.043	.043	.043

3	2.050	1.100	4.000	.171	.062	.037	.060	.029	.074
5	1.950	1.000	3.000	-.007	-.008	-.010	-.007	-.008	-.010
	1.850	.900	2.000	-.013	-.015	-.020	-.013	-.016	-.020
	1.750	.800	1.000	-.020	-.023	-.029	-.020	-.023	-.029
	1.650	.700	0.000	-.026	-.031	-.037	-.026	-.031	-.037
9	1.550	.600	0.000	-.032	-.038	-.043	-.032	-.038	-.048
	1.450	.500	0.000	-.037	-.044	-.050	-.037	-.044	-.056
11	1.350	.400	0.000	-.042	-.050	-.056	-.041	-.050	-.063
	1.250	.300	0.000	-.045	-.055	-.060	-.045	-.055	-.070
13	1.150	.200	0.000	-.049	-.059	-.067	-.049	-.059	-.077
	1.050	.100	0.000	-.051	-.063	-.072	-.051	-.063	-.082
15	1.000	.000	0.000	-.053	-.066	-.077	-.053	-.066	-.086
	1.100	.100	0.000	-.054	-.067	-.079	-.054	-.067	-.090
17	1.200	.200	0.000	-.054	-.069	-.083	-.054	-.068	-.093
	1.300	.300	0.000	-.054	-.069	-.085	-.053	-.069	-.095
19	1.400	.400	0.000	-.052	-.068	-.086	-.052	-.068	-.096
	1.500	.500	0.000	-.051	-.067	-.086	-.049	-.067	-.096
21	1.600	.600	0.000	-.047	-.065	-.086	-.047	-.065	-.096
	1.750	.750	0.000	-.041	-.062	-.084	-.043	-.062	-.094
23	1.850	.850	0.000	-.034	-.059	-.082	-.039	-.059	-.092
	1.950	.950	0.000	-.026	-.055	-.079	-.034	-.055	-.090
25	2.050	1.050	0.000	-.019	-.050	-.076	-.028	-.050	-.086
	2.150	1.150	0.000	-.011	-.045	-.073	-.023	-.045	-.082
27	2.250	1.250	0.000	-.006	-.040	-.070	-.016	-.039	-.078
	2.350	1.350	0.000	-.003	-.034	-.067	-.010	-.033	-.073
29	2.450	1.450	0.000	-.003	-.027	-.063	-.003	-.027	-.068
	2.550	1.550	0.000	.000	-.021	-.058	.005	-.020	-.062
31	2.650	1.650	0.000	.002	-.014	-.056	.012	-.013	-.056
	2.750	1.750	0.000	.006	-.006	-.050	.020	-.006	-.050
33	2.850	1.850	0.000	.010	.001	-.044	.028	.001	-.044
	2.950	1.950	0.000	.016	.007	-.037	.036	.009	-.037
35	3.050	2.050	0.000	.023	.014	-.030	.047	.008	-.030
	3.150	2.150	0.000	.031	.020	-.020	.053	.016	-.020
37	3.250	2.250	0.000	.040	.023	-.029	.060	.023	-.029
	3.350	2.350	0.000	.050	.031	-.037	.070	.030	-.038
39	3.450	2.450	0.000	.062	.039	-.047	.081	.037	-.047
	3.550	2.550	0.000	.077	.049	-.056	.093	.043	-.056
41	3.650	2.650	0.000	.091	.059	-.063	.104	.049	-.063
	3.750	2.750	0.000	.095	.065	-.070	.115	.054	-.070
43	3.850	2.850	0.000	.099	.069	-.076	.126	.058	-.076
	3.950	2.950	0.000	.091	.063	-.082	.137	.062	-.081
45	4.050	3.050	0.000	.053	.055	-.086	.148	.064	-.085
	4.150	3.150	0.000	.054	.057	-.090	.159	.066	-.089
47	4.250	3.250	0.000	.054	.054	-.093	.163	.067	-.092
	4.350	3.350	0.000	.053	.054	-.095	.162	.068	-.094
49	4.450	3.450	0.000	.052	.053	-.096	.160	.067	-.095
	4.550	3.550	0.000	.050	.050	-.096	.158	.066	-.095
51	4.650	3.650	0.000	.047	.045	-.096	.155	.064	-.094
	4.750	3.750	0.000	.043	.042	-.094	.152	.061	-.093
53	4.850	3.850	0.000	.039	.039	-.092	.149	.057	-.091
	4.950	3.950	0.000	.034	.034	-.090	.146	.053	-.088
55	5.050	4.050	0.000	.029	.030	-.086	.143	.049	-.085
	5.150	4.150	0.000	.023	.025	-.082	.140	.043	-.081
57	5.250	4.250	0.000	.016	.018	-.078	.135	.038	-.076
	5.350	4.350	0.000	.010	.013	-.073	.130	.032	-.072
59	5.450	4.450	0.000	.003	.007	-.068	.125	.025	-.066
	5.550	4.550	0.000	.000	.002	-.062	.120	.019	-.061
61	5.650	4.650	0.000	.002	.004	-.056	.114	.012	-.055
	5.750	4.750	0.000	.008	.010	-.050	.108	.005	-.048
63	5.850	4.850	0.000	.013	.014	-.044	.103	.003	-.042

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1	2.250	.450	5.000	.034	.009	-.037	.040	.019	-.027
5	.950	.450	5.000	-.067	-.030	-.010	-.006	-.007	-.009
	.150	.450	5.000	-.013	-.015	-.012	-.011	-.014	-.018
7	.350	.450	5.000	-.028	-.023	-.022	-.017	-.021	-.026
	.050	.450	5.000	-.025	-.030	-.038	-.022	-.027	-.035
9	.450	.450	5.000	-.031	-.037	-.047	-.027	-.033	-.043
	.050	.450	5.000	-.036	-.043	-.055	-.031	-.038	-.050
11	.550	.450	5.000	-.041	-.049	-.062	-.035	-.043	-.057
	.750	.450	5.000	-.045	-.054	-.069	-.038	-.047	-.063
13	.850	.450	5.000	-.049	-.058	-.075	-.040	-.051	-.068
	.950	.450	5.000	-.052	-.062	-.081	-.042	-.054	-.073
15	1.050	.450	5.000	-.052	-.064	-.085	-.043	-.056	-.077
	1.150	.450	5.000	-.053	-.066	-.087	-.043	-.057	-.080
17	1.250	.450	5.000	-.053	-.067	-.091	-.043	-.057	-.082
	1.350	.450	5.000	-.052	-.068	-.093	-.042	-.057	-.083
19	1.450	.450	5.000	-.051	-.067	-.094	-.040	-.056	-.084
	1.550	.450	5.000	-.047	-.066	-.095	-.037	-.054	-.083
21	1.650	.450	5.000	-.046	-.064	-.094	-.033	-.052	-.082
	1.750	.450	5.000	-.043	-.061	-.093	-.029	-.049	-.080
23	1.850	.450	5.000	-.038	-.058	-.091	-.025	-.045	-.078
	1.950	.450	5.000	-.033	-.054	-.088	-.020	-.040	-.075
25	2.050	.450	5.000	-.028	-.049	-.085	-.014	-.035	-.071
	2.150	.450	5.000	-.022	-.044	-.081	-.008	-.030	-.067
27	2.250	.450	5.000	-.016	-.039	-.077	-.001	-.024	-.063
	2.350	.450	5.000	-.010	-.033	-.072	.006	-.018	-.057
29	2.450	.450	5.000	-.003	-.027	-.067	.013	-.011	-.052
	2.550	.450	5.000	.005	-.020	-.061	.021	-.004	-.046
31	2.650	.450	5.000	.012	-.013	-.055	.028	.003	-.040
	2.750	.450	5.000	.020	-.006	-.049	.036	.010	-.034
33	2.850	.450	5.000	.028	.001	-.043	.044	.018	-.027
	2.950	.450	5.000	.036	.009	-.036	.053	.025	-.020
35	.350	.550	5.000	-.007	-.008	-.010	-.005	-.007	-.008
	.150	.550	5.000	-.013	-.015	-.019	-.011	-.013	-.017
37	.250	.550	5.000	-.019	-.023	-.029	-.016	-.019	-.025
	.050	.550	5.000	-.025	-.030	-.036	-.020	-.025	-.033
39	.450	.550	5.000	-.031	-.037	-.045	-.025	-.030	-.040
	.650	.550	5.000	-.034	-.043	-.054	-.028	-.035	-.047
41	.850	.550	5.000	-.038	-.048	-.062	-.032	-.040	-.054
	.750	.550	5.000	-.044	-.053	-.069	-.034	-.044	-.057
43	.950	.550	5.000	-.047	-.058	-.075	-.036	-.047	-.064
	.750	.550	5.000	-.050	-.061	-.080	-.038	-.049	-.068
45	1.050	.550	5.000	-.052	-.064	-.084	-.038	-.051	-.072
	1.150	.550	5.000	-.052	-.066	-.086	-.038	-.052	-.074
47	1.250	.550	5.000	-.053	-.067	-.091	-.039	-.052	-.076
	1.350	.550	5.000	-.052	-.067	-.093	-.036	-.051	-.077
49	1.450	.550	5.000	-.051	-.067	-.094	-.034	-.050	-.078
	1.550	.550	5.000	-.048	-.065	-.094	-.031	-.048	-.077
51	1.650	.550	5.000	-.045	-.063	-.093	-.027	-.045	-.076
	1.750	.550	5.000	-.042	-.061	-.092	-.023	-.042	-.074
53	1.850	.550	5.000	-.038	-.057	-.090	-.018	-.038	-.071
	1.950	.550	5.000	-.033	-.054	-.087	-.013	-.033	-.068
55	2.050	.550	5.000	-.029	-.049	-.084	-.007	-.028	-.064
	2.150	.550	5.000	-.022	-.044	-.080	-.000	-.023	-.060
57	2.250	.550	5.000	-.016	-.039	-.076	.006	-.017	-.055
	2.350	.550	5.000	-.009	-.033	-.071	.013	-.010	-.050
59	2.450	.550	5.000	-.003	-.026	-.066	.021	-.004	-.044
	2.550	.550	5.000	.005	-.020	-.061	.028	.003	-.038
61	2.650	.550	5.000	.012	-.013	-.055	.036	.011	-.032
	2.750	.550	5.000	.020	-.006	-.049	.044	.018	-.026
63	2.850	.550	5.000	.028	.001	-.043	.052	.026	-.019

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1	1.000	.000	5.000	-.005	-.007	-.010	-.013	-.016	-.012
2	1.000	.000	5.000	-.007	-.009	-.010	-.010	-.009	-.008
3	1.000	.000	5.000	-.010	-.013	-.015	-.017	-.017	-.016
4	1.000	.000	5.000	-.013	-.017	-.020	-.020	-.017	-.023
5	1.000	.000	5.000	-.017	-.022	-.025	-.025	-.023	-.031
6	1.000	.000	5.000	-.022	-.028	-.030	-.030	-.028	-.037
7	1.000	.000	5.000	-.028	-.034	-.036	-.036	-.032	-.044
8	1.000	.000	5.000	-.034	-.040	-.041	-.041	-.036	-.050
9	1.000	.000	5.000	-.040	-.046	-.046	-.046	-.039	-.055
10	1.000	.000	5.000	-.046	-.052	-.052	-.052	-.042	-.059
11	1.000	.000	5.000	-.052	-.058	-.058	-.058	-.044	-.063
12	1.000	.000	5.000	-.058	-.064	-.064	-.064	-.045	-.066
13	1.000	.000	5.000	-.064	-.070	-.070	-.070	-.046	-.068
14	1.000	.000	5.000	-.070	-.076	-.076	-.076	-.046	-.070
15	1.000	.000	5.000	-.076	-.082	-.082	-.082	-.045	-.071
16	1.000	.000	5.000	-.082	-.088	-.088	-.088	-.043	-.070
17	1.000	.000	5.000	-.088	-.094	-.094	-.094	-.041	-.070
18	1.000	.000	5.000	-.094	-.100	-.100	-.100	-.038	-.068
19	1.000	.000	5.000	-.100	-.106	-.106	-.106	-.034	-.066
20	1.000	.000	5.000	-.106	-.112	-.112	-.112	-.030	-.063
21	1.000	.000	5.000	-.112	-.118	-.118	-.118	-.025	-.060
22	1.000	.000	5.000	-.118	-.124	-.124	-.124	-.020	-.056
23	1.000	.000	5.000	-.124	-.130	-.130	-.130	-.014	-.051
24	1.000	.000	5.000	-.130	-.136	-.136	-.136	-.008	-.046
25	1.000	.000	5.000	-.136	-.142	-.142	-.142	-.001	-.041
26	1.000	.000	5.000	-.142	-.148	-.148	-.148	.005	-.035
27	1.000	.000	5.000	-.148	-.154	-.154	-.154	.012	-.029
28	1.000	.000	5.000	-.154	-.160	-.160	-.160	.020	-.023
29	1.000	.000	5.000	-.160	-.166	-.166	-.166	.027	-.016
30	1.000	.000	5.000	-.166	-.172	-.172	-.172	.035	-.009
31	1.000	.000	5.000	-.172	-.178	-.178	-.178	.043	-.003
32	1.000	.000	5.000	-.178	-.184	-.184	-.184	.050	-.007
33	1.000	.000	5.000	-.184	-.190	-.190	-.190	.058	-.014
34	1.000	.000	5.000	-.190	-.196	-.196	-.196	.066	-.021
35	1.000	.000	5.000	-.196	-.202	-.202	-.202	.074	-.026
36	1.000	.000	5.000	-.202	-.208	-.208	-.208	.082	-.034
37	1.000	.000	5.000	-.208	-.214	-.214	-.214	.090	-.040
38	1.000	.000	5.000	-.214	-.220	-.220	-.220	.098	-.045
39	1.000	.000	5.000	-.220	-.226	-.226	-.226	.106	-.050
40	1.000	.000	5.000	-.226	-.232	-.232	-.232	.114	-.054
41	1.000	.000	5.000	-.232	-.238	-.238	-.238	.122	-.057
42	1.000	.000	5.000	-.238	-.244	-.244	-.244	.130	-.060
43	1.000	.000	5.000	-.244	-.250	-.250	-.250	.138	-.062
44	1.000	.000	5.000	-.250	-.256	-.256	-.256	.146	-.063
45	1.000	.000	5.000	-.256	-.262	-.262	-.262	.154	-.063
46	1.000	.000	5.000	-.262	-.268	-.268	-.268	.162	-.062
47	1.000	.000	5.000	-.268	-.274	-.274	-.274	.170	-.061
48	1.000	.000	5.000	-.274	-.280	-.280	-.280	.178	-.059
49	1.000	.000	5.000	-.280	-.286	-.286	-.286	.186	-.057
50	1.000	.000	5.000	-.286	-.292	-.292	-.292	.194	-.054
51	1.000	.000	5.000	-.292	-.298	-.298	-.298	.202	-.051
52	1.000	.000	5.000	-.298	-.304	-.304	-.304	.210	-.048
53	1.000	.000	5.000	-.304	-.310	-.310	-.310	.218	-.045
54	1.000	.000	5.000	-.310	-.316	-.316	-.316	.226	-.042
55	1.000	.000	5.000	-.316	-.322	-.322	-.322	.234	-.039
56	1.000	.000	5.000	-.322	-.328	-.328	-.328	.242	-.036
57	1.000	.000	5.000	-.328	-.334	-.334	-.334	.250	-.033
58	1.000	.000	5.000	-.334	-.340	-.340	-.340	.258	-.030
59	1.000	.000	5.000	-.340	-.346	-.346	-.346	.266	-.027
60	1.000	.000	5.000	-.346	-.352	-.352	-.352	.274	-.024
61	1.000	.000	5.000	-.352	-.358	-.358	-.358	.282	-.021
62	1.000	.000	5.000	-.358	-.364	-.364	-.364	.290	-.018
63	1.000	.000	5.000	-.364	-.370	-.370	-.370	.298	-.015

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LINE NO.	DATE	TIME	AMOUNT	DEBIT	CREDIT	BALANCE	DEBIT	CREDIT	BALANCE
3	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
5	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
7	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
9	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
11	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
13	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
15	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
17	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
19	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
21	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
23	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
25	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
27	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
29	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
31	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
33	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
35	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
37	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
39	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
41	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
43	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
45	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
47	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
49	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
51	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
53	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
55	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
57	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
59	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
61	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000
63	1.250	1.450	5.000	-0.000	-0.000	-0.000	-0.000	-0.000	-0.000

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A	EXPER. DATA FOR STRESS-STRAIN CURVES FOR SOILS							DATE 091377		PAGE 167	2
	EXPER. DATA FOR STRESS-STRAIN CURVES FOR SOILS										
3	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	4
5	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	6
7	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	8
9	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	10
11	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	12
13	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	14
15	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	16
17	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	18
19	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	20
21	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	22
23	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	24
25	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	26
27	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	28
29	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	30
31	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	32
33	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	34
35	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	36
37	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	38
39	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	40
41	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	42
43	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	44
45	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	46
47	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	48
49	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	50
51	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	52
53	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	54
55	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	56
57	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	58
59	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	60
61	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	62
63	1.000	2.000	5.000	-.000	-.000	-.000	-.000	.000	.000	.000	64

2	2.250	2.550	5.000	-.029	-.012	-.015	.155	.331	.291
4	2.300	2.550	5.000	-.029	-.019	-.005	.013	.012	.010
6	2.350	2.550	5.000	-.027	-.019	-.011	.025	.023	.020
8	2.400	2.550	5.000	-.011	-.013	-.016	.038	.035	.030
10	2.450	2.550	5.000	-.010	-.017	-.021	.050	.036	.040
12	2.500	2.550	5.000	-.013	-.021	-.020	.063	.059	.050
14	2.550	2.550	5.000	-.020	-.024	-.031	.075	.067	.060
16	2.600	2.550	5.000	-.023	-.028	-.035	.088	.081	.070
18	2.650	2.550	5.000	-.025	-.030	-.039	.101	.093	.080
20	2.700	2.550	5.000	-.027	-.033	-.043	.113	.109	.090
22	2.750	2.550	5.000	-.029	-.035	-.046	.126	.116	.100
24	2.800	2.550	5.000	-.027	-.037	-.040	.137	.128	.110
26	2.850	2.550	5.000	-.030	-.038	-.040	.151	.150	.121
28	2.900	2.550	5.000	-.030	-.038	-.052	.164	.152	.131
30	2.950	2.550	5.000	-.030	-.038	-.053	.177	.164	.142
32	3.000	2.550	5.000	-.029	-.038	-.054	.189	.175	.152
34	3.050	2.550	5.000	-.028	-.037	-.054	.202	.187	.163
36	3.100	2.550	5.000	-.025	-.036	-.053	.215	.199	.173
38	3.150	2.550	5.000	-.024	-.034	-.053	.227	.211	.184
40	3.200	2.550	5.000	-.021	-.032	-.051	.239	.222	.194
42	3.250	2.550	5.000	-.019	-.030	-.050	.252	.234	.204
44	3.300	2.550	5.000	-.019	-.027	-.047	.264	.246	.215
46	3.350	2.550	5.000	-.011	-.024	-.045	.276	.257	.225
48	3.400	2.550	5.000	-.007	-.020	-.042	.288	.268	.236
50	3.450	2.550	5.000	-.002	-.015	-.039	.300	.280	.244
52	3.500	2.550	5.000	.002	-.012	-.035	.312	.291	.256
54	3.550	2.550	5.000	.007	-.007	-.031	.323	.302	.266
56	3.600	2.550	5.000	.012	-.003	-.027	.335	.313	.276
58	3.650	2.550	5.000	.018	.002	-.023	.346	.323	.285
60	3.700	2.550	5.000	.023	.007	-.019	.357	.334	.295
62	3.750	2.550	5.000	.029	.013	-.014	.369	.344	.305
64	3.800	2.550	5.000	.034	-.005	-.005	.381	.356	.311
66	3.850	2.550	5.000	.037	-.005	-.010	.392	.367	.321
68	3.900	2.550	5.000	.041	-.012	-.016	.400	.377	.332
70	3.950	2.550	5.000	.043	-.015	-.020	.405	.384	.342
72	4.000	2.550	5.000	.047	-.020	-.025	.416	.391	.353
74	4.050	2.550	5.000	.050	-.023	-.030	.427	.397	.364
76	4.100	2.550	5.000	.052	-.024	-.034	.432	.406	.374
78	4.150	2.550	5.000	.054	-.029	-.037	.436	.408	.385
80	4.200	2.550	5.000	.055	-.031	-.041	.441	.410	.396
82	4.250	2.550	5.000	.057	-.033	-.045	.443	.413	.397
84	4.300	2.550	5.000	.058	-.034	-.046	.445	.415	.397
86	4.350	2.550	5.000	.059	-.036	-.050	.447	.417	.398
88	4.400	2.550	5.000	.059	-.037	-.050	.447	.417	.398
90	4.450	2.550	5.000	.059	-.037	-.051	.447	.417	.398
92	4.500	2.550	5.000	.059	-.037	-.051	.447	.417	.398
94	4.550	2.550	5.000	.059	-.037	-.051	.447	.417	.398
96	4.600	2.550	5.000	.059	-.037	-.051	.447	.417	.398
98	4.650	2.550	5.000	.059	-.037	-.051	.447	.417	.398
100	4.700	2.550	5.000	.059	-.037	-.051	.447	.417	.398

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1	2.250	2.250	5.000	-.008	-.013	-.012	.130	.356	.317	2
3	2.250	2.250	5.000	-.008	-.014	-.009	.014	.014	.011	4
5	2.250	2.250	5.000	-.007	-.015	-.010	.020	.026	.022	6
7	2.250	2.250	5.000	-.010	-.012	-.015	.041	.039	.034	8
9	2.250	2.250	5.000	-.011	-.014	-.016	.055	.051	.045	10
11	2.250	2.250	5.000	-.016	-.019	-.024	.069	.064	.056	12
13	2.250	2.250	5.000	-.017	-.022	-.028	.083	.077	.067	14
15	2.250	2.250	5.000	-.021	-.025	-.032	.097	.090	.079	16
17	2.250	2.250	5.000	-.023	-.029	-.036	.110	.103	.090	18
19	2.250	2.250	5.000	-.025	-.030	-.039	.124	.116	.101	20
21	2.250	2.250	5.000	-.026	-.032	-.042	.138	.128	.113	22
23	2.250	2.250	5.000	-.027	-.033	-.044	.151	.141	.124	24
25	2.250	2.250	5.000	-.027	-.034	-.046	.165	.154	.135	26
27	2.250	2.250	5.000	-.027	-.035	-.047	.179	.167	.147	28
29	2.250	2.250	5.000	-.027	-.035	-.048	.192	.179	.158	30
31	2.250	2.250	5.000	-.026	-.035	-.049	.206	.192	.169	32
33	2.250	2.250	5.000	-.025	-.034	-.049	.219	.205	.181	34
35	2.250	2.250	5.000	-.023	-.033	-.049	.232	.217	.192	36
37	2.250	2.250	5.000	-.021	-.031	-.048	.245	.229	.203	38
39	2.250	2.250	5.000	-.019	-.029	-.047	.258	.242	.214	40
41	2.250	2.250	5.000	-.016	-.027	-.045	.271	.254	.225	42
43	2.250	2.250	5.000	-.013	-.024	-.043	.284	.266	.236	44
45	2.250	2.250	5.000	-.009	-.021	-.041	.297	.278	.247	46
47	2.250	2.250	5.000	-.005	-.018	-.038	.309	.290	.258	48
49	2.250	2.250	5.000	-.001	-.014	-.035	.321	.301	.268	50
51	2.250	2.250	5.000	.003	-.010	-.031	.333	.313	.279	52
53	2.250	2.250	5.000	.007	-.006	-.028	.345	.324	.289	54
55	2.250	2.250	5.000	.011	-.001	-.024	.357	.335	.299	56
57	2.250	2.250	5.000	.018	.004	-.016	.369	.346	.309	58
59	2.250	2.250	5.000	.023	.014	-.011	.380	.357	.319	60
61	2.250	2.250	5.000	.028	.023	-.008	.391	.367	.327	62
63	2.250	2.250	5.000	.033	.029	-.005	.404	.379	.339	64
65	2.250	2.250	5.000	.036	.033	-.003	.414	.388	.347	66
67	2.250	2.250	5.000	.038	.035	-.002	.424	.397	.355	68
69	2.250	2.250	5.000	.039	.036	-.001	.433	.405	.363	70
71	2.250	2.250	5.000	.040	.037	.000	.442	.413	.371	72
73	2.250	2.250	5.000	.040	.037	.001	.450	.420	.378	74
75	2.250	2.250	5.000	.040	.037	.002	.458	.427	.385	76
77	2.250	2.250	5.000	.040	.037	.003	.466	.434	.391	78
79	2.250	2.250	5.000	.040	.037	.004	.474	.441	.397	80
81	2.250	2.250	5.000	.040	.037	.005	.482	.448	.403	82
83	2.250	2.250	5.000	.040	.037	.006	.490	.455	.409	84
85	2.250	2.250	5.000	.040	.037	.007	.498	.462	.415	86
87	2.250	2.250	5.000	.040	.037	.008	.506	.469	.421	88
89	2.250	2.250	5.000	.040	.037	.009	.514	.476	.427	90
91	2.250	2.250	5.000	.040	.037	.010	.522	.483	.433	92
93	2.250	2.250	5.000	.040	.037	.011	.530	.490	.439	94
95	2.250	2.250	5.000	.040	.037	.012	.538	.497	.445	96
97	2.250	2.250	5.000	.040	.037	.013	.546	.504	.451	98
99	2.250	2.250	5.000	.040	.037	.014	.554	.511	.457	100

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1	1.000	1.000	0.000	-0.002	-0.021	-0.002	.054	.031	.024
2	1.000	1.000	0.000	-0.005	-0.035	-0.010	.081	-.002	-.005
3	1.000	1.000	0.000	-0.007	-0.047	-0.013	.093	-.004	-.007
4	1.000	1.000	0.000	-0.013	-0.015	-0.019	.084	-.006	-.010
5	1.000	1.000	0.000	-0.017	-0.020	-0.026	.085	-.008	-.013
6	1.000	1.000	0.000	-0.022	-0.024	-0.030	.086	-.010	-.016
7	1.000	1.000	0.000	-0.027	-0.028	-0.036	.087	-.011	-.017
8	1.000	1.000	0.000	-0.037	-0.033	-0.041	.087	-.013	-.022
9	1.000	1.000	0.000	-0.047	-0.045	-0.050	.087	-.014	-.024
10	1.000	1.000	0.000	-0.053	-0.045	-0.051	.087	-.014	-.026
11	1.000	1.000	0.000	-0.053	-0.043	-0.055	.087	-.014	-.026
12	1.000	1.000	0.000	-0.057	-0.045	-0.059	.086	-.015	-.029
13	1.000	1.000	0.000	-0.057	-0.048	-0.062	.085	-.015	-.030
14	1.000	1.000	0.000	-0.060	-0.049	-0.065	.084	-.014	-.031
15	1.000	1.000	0.000	-0.061	-0.051	-0.068	.083	-.013	-.031
16	1.000	1.000	0.000	-0.064	-0.052	-0.073	.081	-.012	-.031
17	1.000	1.000	0.000	-0.064	-0.052	-0.071	.082	-.010	-.031
18	1.000	1.000	0.000	-0.068	-0.052	-0.072	.084	-.008	-.030
19	1.000	1.000	0.000	-0.072	-0.051	-0.073	.087	-.006	-.029
20	1.000	1.000	0.000	-0.075	-0.051	-0.073	.081	-.004	-.027
21	1.000	1.000	0.000	-0.075	-0.050	-0.070	.081	-.004	-.025
22	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
23	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
24	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
25	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
26	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
27	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
28	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
29	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
30	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
31	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
32	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
33	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
34	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
35	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
36	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
37	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
38	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
39	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
40	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
41	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
42	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
43	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
44	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
45	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
46	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
47	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
48	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
49	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
50	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
51	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
52	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
53	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
54	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
55	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
56	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
57	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
58	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
59	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
60	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
61	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
62	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
63	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025
64	1.000	1.000	0.000	-0.075	-0.050	-0.073	.081	-.004	-.025

1	2.950	1.475	6.363	-.007	-.000	-.001	.029	.002	.020
2	2.950	1.475	6.363	-.007	-.000	-.000	-.000	-.001	-.002
3	2.950	1.475	6.363	-.007	-.001	-.012	-.001	-.002	-.005
4	2.950	1.475	6.363	-.007	-.014	-.016	-.001	-.003	-.007
5	2.950	1.475	6.363	-.007	-.017	-.024	-.001	-.004	-.009
6	2.950	1.475	6.363	-.007	-.020	-.029	-.001	-.005	-.011
7	2.950	1.475	6.363	-.007	-.023	-.035	-.001	-.005	-.013
8	2.950	1.475	6.363	-.007	-.026	-.040	-.000	-.006	-.015
9	2.950	1.475	6.363	-.007	-.029	-.045	.001	-.006	-.016
10	2.950	1.475	6.363	-.007	-.032	-.050	.001	-.006	-.017
11	2.950	1.475	6.363	-.007	-.035	-.055	.001	-.005	-.018
12	2.950	1.475	6.363	-.007	-.038	-.060	.004	-.005	-.019
13	2.950	1.475	6.363	-.007	-.041	-.065	.006	-.004	-.019
14	2.950	1.475	6.363	-.007	-.044	-.070	.009	-.002	-.019
15	2.950	1.475	6.363	-.007	-.047	-.075	.010	-.001	-.018
16	2.950	1.475	6.363	-.007	-.050	-.080	.013	.001	-.017
17	2.950	1.475	6.363	-.007	-.053	-.085	.016	.004	-.016
18	2.950	1.475	6.363	-.007	-.056	-.090	.019	.006	-.015
19	2.950	1.475	6.363	-.007	-.059	-.095	.022	.009	-.013
20	2.950	1.475	6.363	-.007	-.062	-.100	.026	.012	-.011
21	2.950	1.475	6.363	-.007	-.065	-.105	.030	.016	-.008
22	2.950	1.475	6.363	-.007	-.068	-.110	.035	.020	-.006
23	2.950	1.475	6.363	-.007	-.071	-.115	.039	.024	-.003
24	2.950	1.475	6.363	-.007	-.074	-.120	.044	.028	.001
25	2.950	1.475	6.363	-.007	-.077	-.125	.049	.032	.004
26	2.950	1.475	6.363	-.007	-.080	-.130	.054	.037	.008
27	2.950	1.475	6.363	-.007	-.083	-.135	.060	.042	.012
28	2.950	1.475	6.363	-.007	-.086	-.140	.065	.047	.016
29	2.950	1.475	6.363	-.007	-.089	-.145	.071	.052	.021
30	2.950	1.475	6.363	-.007	-.092	-.150	.077	.057	.025
31	2.950	1.475	6.363	-.007	-.095	-.155	.083	.063	.030
32	2.950	1.475	6.363	-.007	-.098	-.160	.090	.070	.036
33	2.950	1.475	6.363	-.007	-.101	-.165	.097	.077	.042
34	2.950	1.475	6.363	-.007	-.104	-.170	.104	.084	.048
35	2.950	1.475	6.363	-.007	-.107	-.175	.111	.091	.054
36	2.950	1.475	6.363	-.007	-.110	-.180	.118	.098	.060
37	2.950	1.475	6.363	-.007	-.113	-.185	.125	.105	.066
38	2.950	1.475	6.363	-.007	-.116	-.190	.132	.112	.072
39	2.950	1.475	6.363	-.007	-.119	-.195	.139	.119	.078
40	2.950	1.475	6.363	-.007	-.122	-.200	.146	.126	.084
41	2.950	1.475	6.363	-.007	-.125	-.205	.153	.133	.090
42	2.950	1.475	6.363	-.007	-.128	-.210	.160	.140	.096
43	2.950	1.475	6.363	-.007	-.131	-.215	.167	.147	.102
44	2.950	1.475	6.363	-.007	-.134	-.220	.174	.154	.108
45	2.950	1.475	6.363	-.007	-.137	-.225	.181	.161	.114
46	2.950	1.475	6.363	-.007	-.140	-.230	.188	.168	.120
47	2.950	1.475	6.363	-.007	-.143	-.235	.195	.175	.126
48	2.950	1.475	6.363	-.007	-.146	-.240	.202	.182	.132
49	2.950	1.475	6.363	-.007	-.149	-.245	.209	.189	.138
50	2.950	1.475	6.363	-.007	-.152	-.250	.216	.196	.144
51	2.950	1.475	6.363	-.007	-.155	-.255	.223	.203	.150
52	2.950	1.475	6.363	-.007	-.158	-.260	.230	.210	.156
53	2.950	1.475	6.363	-.007	-.161	-.265	.237	.217	.162
54	2.950	1.475	6.363	-.007	-.164	-.270	.244	.224	.168
55	2.950	1.475	6.363	-.007	-.167	-.275	.251	.231	.174
56	2.950	1.475	6.363	-.007	-.170	-.280	.258	.238	.180
57	2.950	1.475	6.363	-.007	-.173	-.285	.265	.245	.186
58	2.950	1.475	6.363	-.007	-.176	-.290	.272	.252	.192
59	2.950	1.475	6.363	-.007	-.179	-.295	.279	.259	.198
60	2.950	1.475	6.363	-.007	-.182	-.300	.286	.266	.204
61	2.950	1.475	6.363	-.007	-.185	-.305	.293	.273	.210
62	2.950	1.475	6.363	-.007	-.188	-.310	.300	.280	.216
63	2.950	1.475	6.363	-.007	-.191	-.315	.307	.287	.222

1	1.750	1.750	0.000	-0.001	-0.012	-0.049	.093	.075	.091	
2	1.750	1.750	0.000	-0.001	-0.005	-0.010	.001	-0.000	-0.001	
3	1.750	1.750	0.000	-0.001	-0.007	-0.012	.002	.000	-0.003	
4	1.750	1.750	0.000	-0.001	-0.010	-0.017	.002	.000	-0.004	
5	1.750	1.750	0.000	-0.001	-0.013	-0.020	.003	.000	-0.005	
6	1.750	1.750	0.000	-0.001	-0.017	-0.026	.005	.001	-0.006	
7	1.750	1.750	0.000	-0.001	-0.022	-0.034	.006	.001	-0.007	
8	1.750	1.750	0.000	-0.001	-0.028	-0.040	.007	.002	-0.007	
9	1.750	1.750	0.000	-0.001	-0.034	-0.048	.009	.003	-0.008	
10	1.750	1.750	0.000	-0.001	-0.040	-0.057	.011	.004	-0.008	
11	1.750	1.750	0.000	-0.001	-0.047	-0.066	.013	.005	-0.008	
12	1.750	1.750	0.000	-0.001	-0.055	-0.076	.015	.007	-0.007	
13	1.750	1.750	0.000	-0.001	-0.063	-0.087	.017	.008	-0.007	
14	1.750	1.750	0.000	-0.001	-0.072	-0.099	.020	.011	-0.006	
15	1.750	1.750	0.000	-0.001	-0.081	-0.112	.023	.013	-0.004	
16	1.750	1.750	0.000	-0.001	-0.091	-0.126	.027	.016	-0.003	
17	1.750	1.750	0.000	-0.001	-0.101	-0.141	.031	.019	-0.001	
18	1.750	1.750	0.000	-0.001	-0.112	-0.157	.034	.022	.001	
19	1.750	1.750	0.000	-0.001	-0.123	-0.174	.039	.025	.002	
20	1.750	1.750	0.000	-0.001	-0.135	-0.192	.043	.029	.006	
21	1.750	1.750	0.000	-0.001	-0.147	-0.211	.048	.033	.009	
22	1.750	1.750	0.000	-0.001	-0.160	-0.231	.052	.038	.013	
23	1.750	1.750	0.000	-0.001	-0.173	-0.252	.057	.042	.016	
24	1.750	1.750	0.000	-0.001	-0.187	-0.274	.063	.047	.020	
25	1.750	1.750	0.000	-0.001	-0.201	-0.297	.069	.052	.024	
26	1.750	1.750	0.000	-0.001	-0.216	-0.321	.074	.057	.028	
27	1.750	1.750	0.000	-0.001	-0.231	-0.346	.079	.062	.033	
28	1.750	1.750	0.000	-0.001	-0.247	-0.372	.085	.067	.037	
29	1.750	1.750	0.000	-0.001	-0.263	-0.399	.091	.073	.042	
30	1.750	1.750	0.000	-0.001	-0.280	-0.427	.097	.078	.047	
31	1.750	1.750	0.000	-0.001	-0.297	-0.456	.104	.084	.052	
32	1.750	1.750	0.000	-0.001	-0.315	-0.486	.111	.091	.057	
33	1.750	1.750	0.000	-0.001	-0.333	-0.517	.119	.098	.062	
34	1.750	1.750	0.000	-0.001	-0.352	-0.549	.127	.106	.067	
35	1.750	1.750	0.000	-0.001	-0.371	-0.582	.136	.114	.072	
36	1.750	1.750	0.000	-0.001	-0.391	-0.616	.145	.123	.077	
37	1.750	1.750	0.000	-0.001	-0.411	-0.651	.155	.132	.082	
38	1.750	1.750	0.000	-0.001	-0.431	-0.687	.165	.142	.087	
39	1.750	1.750	0.000	-0.001	-0.452	-0.724	.175	.152	.092	
40	1.750	1.750	0.000	-0.001	-0.473	-0.762	.186	.163	.097	
41	1.750	1.750	0.000	-0.001	-0.494	-0.801	.197	.174	.102	
42	1.750	1.750	0.000	-0.001	-0.516	-0.841	.208	.185	.107	
43	1.750	1.750	0.000	-0.001	-0.538	-0.882	.220	.196	.112	
44	1.750	1.750	0.000	-0.001	-0.561	-0.924	.232	.207	.117	
45	1.750	1.750	0.000	-0.001	-0.584	-0.967	.245	.218	.122	
46	1.750	1.750	0.000	-0.001	-0.607	-1.011	.258	.229	.127	
47	1.750	1.750	0.000	-0.001	-0.631	-1.056	.271	.240	.132	
48	1.750	1.750	0.000	-0.001	-0.655	-1.102	.285	.251	.137	
49	1.750	1.750	0.000	-0.001	-0.679	-1.149	.299	.262	.142	
50	1.750	1.750	0.000	-0.001	-0.704	-1.197	.313	.273	.147	
51	1.750	1.750	0.000	-0.001	-0.729	-1.246	.328	.284	.152	
52	1.750	1.750	0.000	-0.001	-0.754	-1.296	.343	.295	.157	
53	1.750	1.750	0.000	-0.001	-0.779	-1.347	.358	.306	.162	
54	1.750	1.750	0.000	-0.001	-0.804	-1.399	.373	.317	.167	
55	1.750	1.750	0.000	-0.001	-0.829	-1.452	.389	.328	.172	
56	1.750	1.750	0.000	-0.001	-0.854	-1.506	.405	.339	.177	
57	1.750	1.750	0.000	-0.001	-0.879	-1.561	.421	.350	.182	
58	1.750	1.750	0.000	-0.001	-0.904	-1.617	.437	.361	.187	
59	1.750	1.750	0.000	-0.001	-0.929	-1.674	.453	.372	.192	
60	1.750	1.750	0.000	-0.001	-0.954	-1.732	.469	.383	.197	
61	1.750	1.750	0.000	-0.001	-0.979	-1.791	.485	.394	.202	
62	1.750	1.750	0.000	-0.001	-1.004	-1.851	.501	.405	.207	

UIC

	DATE 07/13/77						PAGE 162		
1	1.250	2.150	6.000	-.001	-.017	-.000	.137	.117	.085
2	1.250	2.150	6.000	-.004	-.009	-.005	.003	.002	.001
3	1.250	2.150	6.000	-.007	-.008	-.011	.005	.000	.002
4	1.250	2.150	6.000	-.011	-.013	-.010	.009	.007	.003
5	1.250	2.150	6.000	-.014	-.017	-.021	.012	.009	.004
6	1.250	2.150	6.000	-.017	-.021	-.020	.016	.012	.005
7	1.250	2.150	6.000	-.021	-.024	-.031	.019	.014	.007
8	1.250	2.150	6.000	-.023	-.028	-.035	.023	.017	.006
9	1.250	2.150	6.000	-.026	-.031	-.040	.026	.020	.010
10	1.250	2.150	6.000	-.029	-.034	-.043	.030	.023	.012
11	1.250	2.150	6.000	-.032	-.037	-.047	.034	.026	.014
12	1.250	2.150	6.000	-.035	-.039	-.050	.038	.030	.016
13	1.250	2.150	6.000	-.038	-.041	-.053	.042	.034	.019
14	1.250	2.150	6.000	-.041	-.044	-.056	.047	.037	.021
15	1.250	2.150	6.000	-.044	-.047	-.059	.052	.041	.024
16	1.250	2.150	6.000	-.046	-.049	-.060	.057	.046	.027
17	1.250	2.150	6.000	-.049	-.052	-.063	.062	.050	.031
18	1.250	2.150	6.000	-.051	-.054	-.065	.067	.055	.034
19	1.250	2.150	6.000	-.054	-.057	-.068	.072	.060	.038
20	1.250	2.150	6.000	-.056	-.059	-.070	.078	.065	.042
21	1.250	2.150	6.000	-.059	-.062	-.073	.084	.070	.046
22	1.250	2.150	6.000	-.061	-.064	-.075	.090	.075	.051
23	1.250	2.150	6.000	-.064	-.067	-.078	.095	.081	.055
24	1.250	2.150	6.000	-.066	-.069	-.080	.102	.086	.060
25	1.250	2.150	6.000	-.069	-.072	-.083	.105	.092	.065
26	1.250	2.150	6.000	-.071	-.074	-.085	.115	.098	.070
27	1.250	2.150	6.000	-.074	-.077	-.088	.121	.104	.075
28	1.250	2.150	6.000	-.076	-.079	-.090	.126	.110	.080
29	1.250	2.150	6.000	-.079	-.082	-.093	.134	.116	.084
30	1.250	2.150	6.000	-.081	-.084	-.095	.141	.122	.091
31	1.250	2.150	6.000	-.084	-.087	-.098	.146	.129	.097
32	1.250	2.150	6.000	-.086	-.089	-.100	.154	.133	.002
33	1.250	2.150	6.000	-.089	-.092	-.103	.157	.136	.003
34	1.250	2.150	6.000	-.091	-.094	-.105	.161	.139	.005
35	1.250	2.150	6.000	-.094	-.097	-.108	.165	.142	.007
36	1.250	2.150	6.000	-.096	-.099	-.110	.168	.145	.008
37	1.250	2.150	6.000	-.099	-.102	-.113	.172	.148	.010
38	1.250	2.150	6.000	-.101	-.104	-.115	.176	.151	.012
39	1.250	2.150	6.000	-.104	-.107	-.118	.180	.154	.015
40	1.250	2.150	6.000	-.106	-.109	-.120	.184	.157	.017
41	1.250	2.150	6.000	-.109	-.112	-.123	.188	.160	.019
42	1.250	2.150	6.000	-.111	-.114	-.125	.192	.163	.021
43	1.250	2.150	6.000	-.114	-.117	-.128	.196	.166	.023
44	1.250	2.150	6.000	-.116					

3	2.250	4.250	6.250	-0.000	-0.010	-0.010	.159	.190	.106
5	2.250	4.250	6.250	-0.000	-0.014	-0.005	.189	.183	.102
7	2.250	4.250	6.250	-0.000	-0.018	-0.010	.188	.187	.105
9	2.250	4.250	6.250	-0.010	-0.012	-0.015	.183	.189	.107
11	2.250	4.250	6.250	-0.010	-0.016	-0.020	.177	.184	.109
13	2.250	4.250	6.250	-0.017	-0.020	-0.025	.171	.187	.111
15	2.250	4.250	6.250	-0.020	-0.023	-0.029	.166	.181	.114
17	2.250	4.250	6.250	-0.023	-0.026	-0.034	.160	.175	.116
19	2.250	4.250	6.250	-0.026	-0.030	-0.038	.155	.170	.119
21	2.250	4.250	6.250	-0.027	-0.032	-0.041	.150	.165	.122
23	2.250	4.250	6.250	-0.027	-0.035	-0.045	.145	.160	.125
25	2.250	4.250	6.250	-0.030	-0.037	-0.048	.140	.155	.128
27	2.250	4.250	6.250	-0.032	-0.039	-0.051	.135	.150	.131
29	2.250	4.250	6.250	-0.033	-0.040	-0.053	.130	.145	.135
31	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.139
33	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.143
35	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.147
37	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.151
39	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.155
41	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.159
43	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.163
45	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.167
47	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.171
49	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.175
51	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.179
53	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.183
55	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.187
57	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.191
59	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.195
61	2.250	4.250	6.250	-0.033	-0.043	-0.056	.125	.140	.199

3	2.750	2.750	0.000	-0.014	-0.018	0.002	.104	.152
5	2.750	2.750	0.000	-0.015	-0.019	0.006	.005	.001
	2.750	2.750	0.000	-0.016	-0.020	0.010	.011	.009
	2.750	2.750	0.000	-0.017	-0.021	0.014	.017	.013
	2.750	2.750	0.000	-0.018	-0.022	0.018	.022	.018
9	2.750	2.750	0.000	-0.019	-0.023	0.022	.024	.022
	2.750	2.750	0.000	-0.020	-0.024	0.026	.028	.027
11	2.750	2.750	0.000	-0.021	-0.025	0.030	.032	.031
	2.750	2.750	0.000	-0.022	-0.026	0.034	.036	.036
13	2.750	2.750	0.000	-0.023	-0.027	0.038	.040	.041
	2.750	2.750	0.000	-0.024	-0.028	0.042	.044	.046
15	2.750	2.750	0.000	-0.025	-0.029	0.046	.048	.051
	2.750	2.750	0.000	-0.026	-0.030	0.050	.052	.055
17	2.750	2.750	0.000	-0.027	-0.031	0.054	.056	.059
	2.750	2.750	0.000	-0.028	-0.032	0.058	.060	.063
19	2.750	2.750	0.000	-0.029	-0.033	0.062	.064	.067
	2.750	2.750	0.000	-0.030	-0.034	0.066	.068	.071
21	2.750	2.750	0.000	-0.031	-0.035	0.070	.072	.075
	2.750	2.750	0.000	-0.032	-0.036	0.074	.076	.079
23	2.750	2.750	0.000	-0.033	-0.037	0.078	.080	.083
	2.750	2.750	0.000	-0.034	-0.038	0.082	.084	.087
25	2.750	2.750	0.000	-0.035	-0.039	0.086	.088	.091
	2.750	2.750	0.000	-0.036	-0.040	0.090	.092	.095
27	2.750	2.750	0.000	-0.037	-0.041	0.094	.096	.099
	2.750	2.750	0.000	-0.038	-0.042	0.098	.100	.103
29	2.750	2.750	0.000	-0.039	-0.043	0.102	.104	.107
	2.750	2.750	0.000	-0.040	-0.044	0.106	.108	.111
31	2.750	2.750	0.000	-0.041	-0.045	0.110	.112	.115
	2.750	2.750	0.000	-0.042	-0.046	0.114	.116	.119
33	2.750	2.750	0.000	-0.043	-0.047	0.118	.120	.123
	2.750	2.750	0.000	-0.044	-0.048	0.122	.124	.127
35	2.750	2.750	0.000	-0.045	-0.049	0.126	.128	.131
	2.750	2.750	0.000	-0.046	-0.050	0.130	.132	.135
37	2.750	2.750	0.000	-0.047	-0.051	0.134	.136	.139
	2.750	2.750	0.000	-0.048	-0.052	0.138	.140	.143
39	2.750	2.750	0.000	-0.049	-0.053	0.142	.144	.147
	2.750	2.750	0.000	-0.050	-0.054	0.146	.148	.151
41	2.750	2.750	0.000	-0.051	-0.055	0.150	.152	.155
	2.750	2.750	0.000	-0.052	-0.056	0.154	.156	.159
43	2.750	2.750	0.000	-0.053	-0.057	0.158	.160	.163
	2.750	2.750	0.000	-0.054	-0.058	0.162	.164	.167
45	2.750	2.750	0.000	-0.055	-0.059	0.166	.168	.171
	2.750	2.750	0.000	-0.056	-0.060	0.170	.172	.175
47	2.750	2.750	0.000	-0.057	-0.061	0.174	.176	.179
	2.750	2.750	0.000	-0.058	-0.062	0.178	.180	.183
49	2.750	2.750	0.000	-0.059	-0.063	0.182	.184	.187
	2.750	2.750	0.000	-0.060	-0.064	0.186	.188	.191
51	2.750	2.750	0.000	-0.061	-0.065	0.190	.192	.195
	2.750	2.750	0.000	-0.062	-0.066	0.194	.196	.199
53	2.750	2.750	0.000	-0.063	-0.067	0.198	.200	.203
	2.750	2.750	0.000	-0.064	-0.068	0.202	.204	.207
55	2.750	2.750	0.000	-0.065	-0.069	0.206	.208	.211
	2.750	2.750	0.000	-0.066	-0.070	0.210	.212	.215
57	2.750	2.750	0.000	-0.067	-0.071	0.214	.216	.219
	2.750	2.750	0.000	-0.068	-0.072	0.218	.220	.223
59	2.750	2.750	0.000	-0.069	-0.073	0.222	.224	.227
	2.750	2.750	0.000	-0.070	-0.074	0.226	.228	.231
61	2.750	2.750	0.000	-0.071	-0.075	0.230	.232	.235
	2.750	2.750	0.000	-0.072	-0.076	0.234	.236	.239

DATE: 07/13 OCT. 1964 - 11 PROJECT: 8002

FILE: 104; 60104-28.471 CDS-605: 315340671

CPU: 0.00:04:27.513 I/O: 0.0:00:07.027

007:11 07:10.750 007:11 07:10.750

DATE TIME

50107: 14:43:10 10.1.77 FILE: 11:00:50 SEP 10, 1977

APPENDIX B

507. SAMPLE DESCRIPTION Berea Road - Fine reddish brown collapsing sand -
undisturbed, air dried sample

SPECIFIC GRAVITY 2.68

WEIGHT SOLID SAMPLE

TEST NO. H - BR - 1

Mass container + dry soil (g) 128.5

DATE 20-2-75

Mass container (g) 78.5

TESTED BY L.A.E.

Mass dry soil (g) 50.0

HYDROMETER NO. 9843 A.S.T.M. 151H

DISPERSING AGENTS 5ml Sodium Oxalate Solution

+ 5ml Sodium Silicate Solution

[illegible]

РЕМДЖК.

Sample soaked for 16 hours.

For the 2 and 5 minute readings Zr uncorrected is used.

Hydrometer tests (A.S.T.M. Standards, Ref. 15, Lambe, Ref. 23, Akroyd, Ref. 48.)

The hydrometer sample was oven dried. If the sample had a relatively high percentage of fines then 50 grams was weighed off for the analysis. For sandy soils 100 grams was used.

After the sample had been weighed, the dispersing agent was added. Varying dispersing agents were used. Solutions of Sodium Oxalate and Sodium Silicate were used for these tests. The dispersing agents were added to the sample, which was in a 250 ml beaker. Distilled water was then added until the 125 ml mark was reached. The sample was allowed to soak for a minimum of sixteen hours.

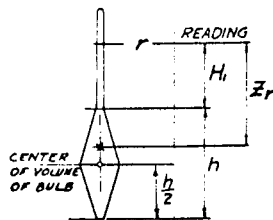
After the soaking time had elapsed the sample was mixed thoroughly with a mechanical stirrer (at 5000 revolutions per minute) for 60 seconds. The mixture was then put into a 1000 ml cylinder.

Corrections had to be made to the hydrometer readings. Initially the tabulated "corrected" reading was corrected only for temperature and the dispersing agent. The corrections are read off from a predetermined curve. (Page B/4) To determine this curve a 1000 ml cylinder filled with distilled water and dispersing agent was subjected to controlled temperatures. A hydrometer reading was taken at the lowest and highest temperatures experienced during the hydrometer tests. These temperatures and the hydrometer readings were plotted and a linear relationship was assumed between these points. (see page B/5)

When the hydrometer was inserted into the measuring cylinder it caused a rise in water level. This also had to be corrected. Therefore Z_r , which is the distance in millimeters from the hydrometer reading to the centre of gravity of the hydrometer bulb, had to be corrected.

therefore

$$\begin{aligned} Z_r &= H_1 + \frac{1}{2} \left(h - \frac{\text{volume of hydrometer bulb}}{\text{area of graduate}} \right) \\ &= H_1 + \frac{1}{2} \left(h - \frac{V_H}{A_{jar}} \right) \end{aligned}$$



Curves defining Z_r corrected and Z_r uncorrected are shown on page B/5. The uncorrected values are used for the 2 and 5 minute readings as the hydrometer was inserted at zero time interval and was not removed until these readings had been taken.

The percentage of particles smaller than a size D is given by;

$$p = R \times \frac{G_s}{G_s - G_w} \times \frac{100}{W} \%$$

where

- p = percentage finer than size D
- G_s = specific gravity of soil grains
- $G_w = 1,000$
- W = weight of soil dispersed in grams/ml.
- R = corrected hydrometer reading

Page B/6 shows a graphical solution of the formula

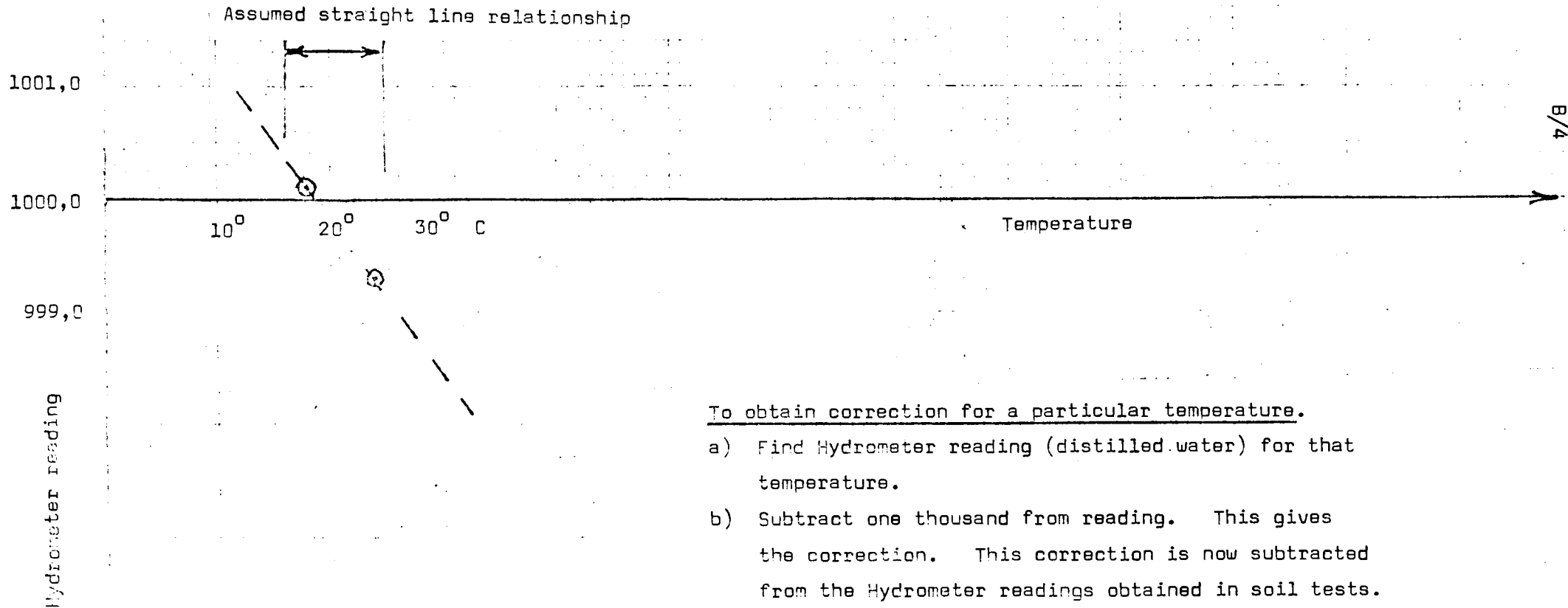
$$p = R \times \frac{G_s}{G_s - G_w} \times \frac{100}{W} \%$$

HYDROMETER TESTS - CORRECTION - 1000 ml distilled water corrected for temperature and dispersing agent.

Dispersing agents:

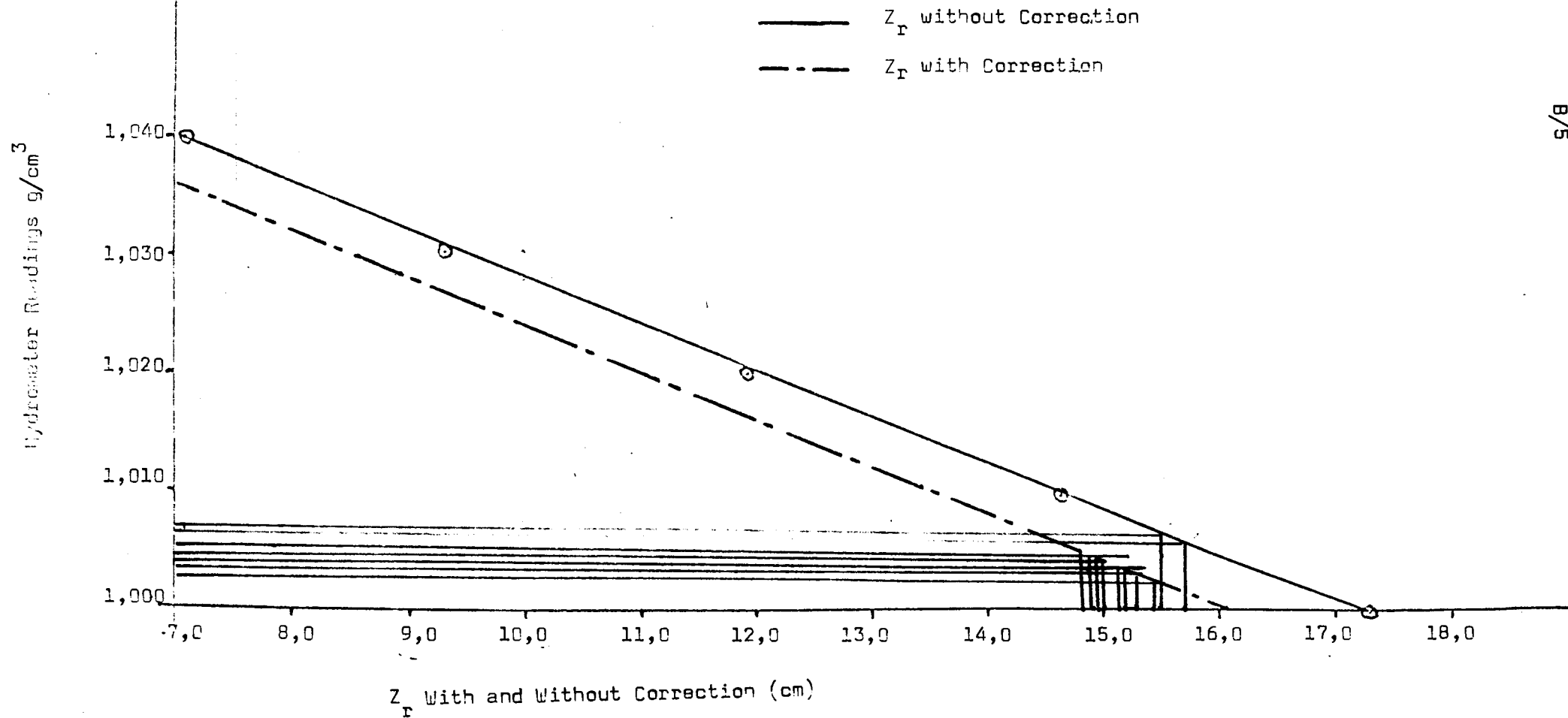
10 ml Sodium acetate solution

10 ml Sodium silicate solution



Hydrometer Readings Against Z_r

Chart for Hydrometer No. 9840 A.S.T.M. 151 H



Graphical solution of formula

$$p = R \times \frac{G_s}{G_s - G_w} \times \frac{100}{W} \%$$

where:

p = percentage finer than size D

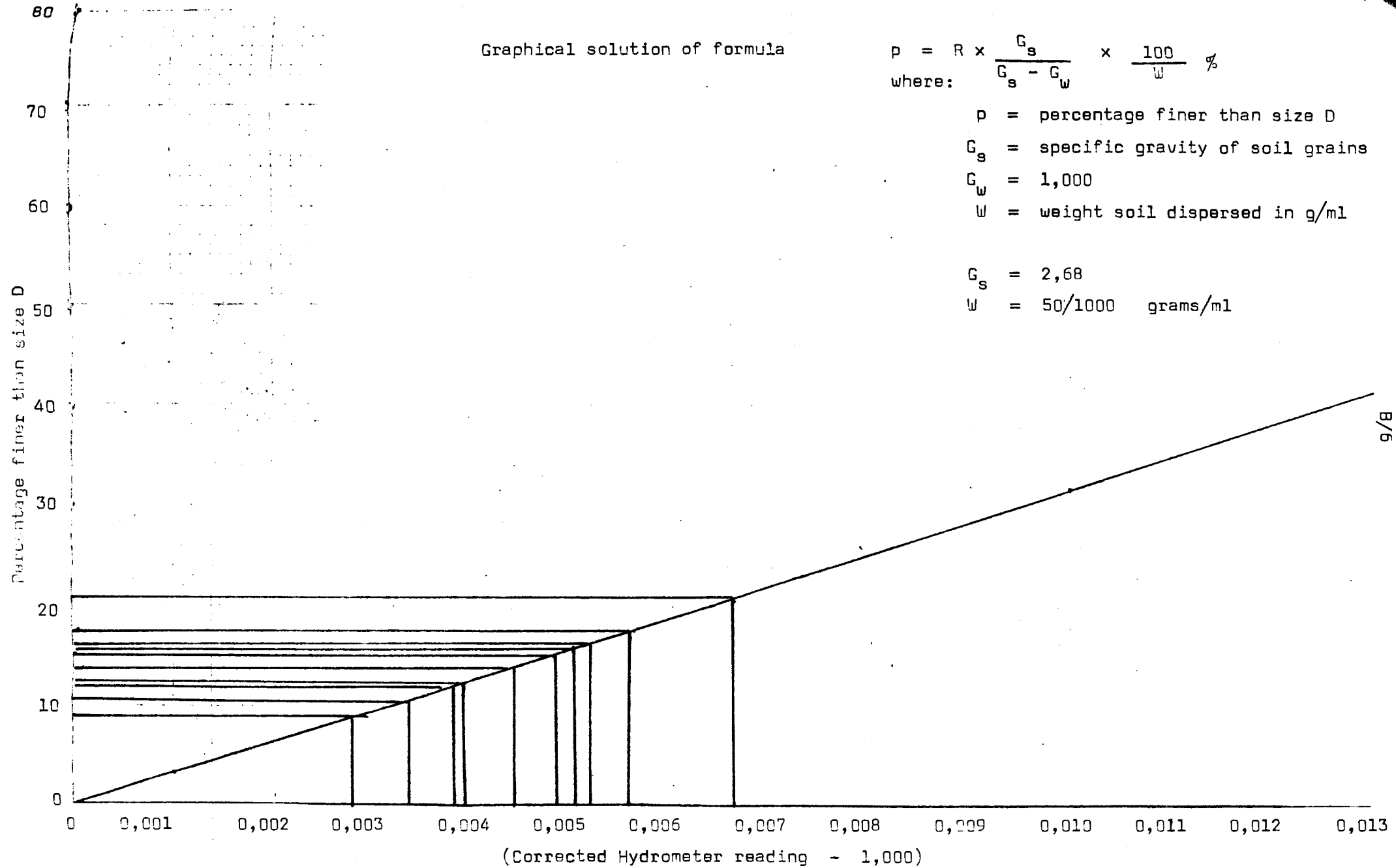
G_s = specific gravity of soil grains

G_w = 1,000

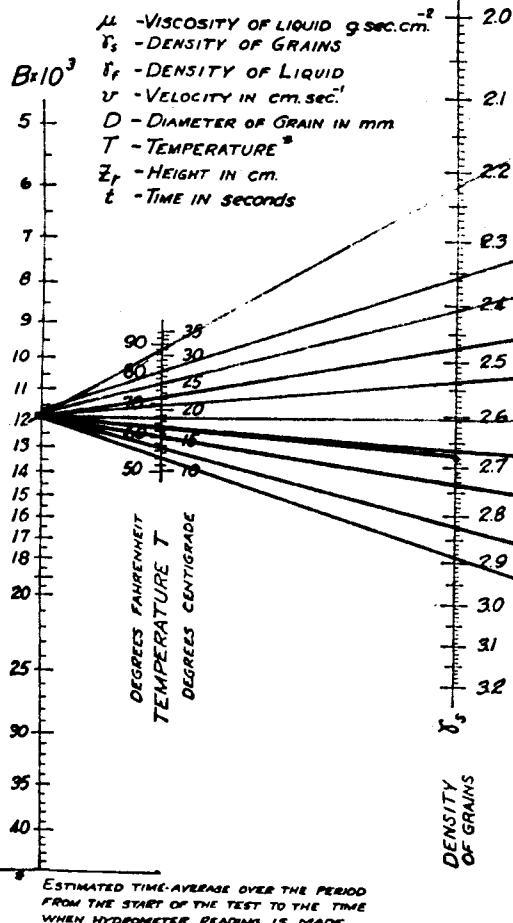
W = weight soil dispersed in g/ml

G_s = 2,68

W = 50/1000 grams/ml



NOMOGRAPHIC CHART FOR SOLUTION OF STOKES' LAW



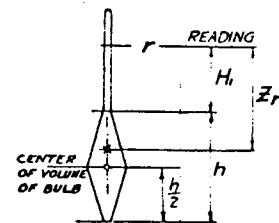
ESTIMATED TIME-AVERAGE OVER THE PERIOD FROM THE START OF THE TEST TO THE TIME WHEN HYDROMETER READING IS MADE.

STOKES' LAW:

$$Q = \sqrt{Bv}$$

$$B = \frac{1800\mu}{\gamma_s - \gamma_f}$$

$$v = \frac{Z_r}{t}$$



HEIGHT H WHICH CORRESPONDS TO READING r DETERMINED FROM

$$Z_r = H + \frac{1}{2} \left(\frac{\text{VOLUME OF HYD. BULB}}{\text{AREA OF GRADUATE}} \right) \text{ CONSTANT}$$

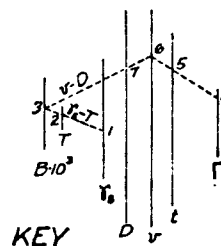
HYDROMETER READING

Z_r TO BE DETERMINED FOR DIFFERENT VALUES OF r CORRESPONDING VALUES OF r TO BE PLOTTED ON RIGHT SIDE OF (Z_r r) SCALE AND CONVENIENT SUBDIVISIONS MADE.

FOR SOIL SUSPENSIONS IN WATER ANY HYDROMETER MEASURING DENSITIES BETWEEN 0.995 AND 1.040 WITH AN ACCURACY OF 0.0002 MAY BE USED

SUGGESTED: CALIBRATION AT 20°C. IN DENSITIES. STREAM LINE BULB. MAX. H_b = 14 TO 16 CM. h = 15 TO 17 CM.

FOR LIQUIDS OTHER THAN WATER THE (B) VALUES MUST BE COMPUTED. THE (γ_s) AND (T) SCALES APPLY ONLY TO SUSPENSIONS IN WATER.



KEY

8/8

SOIL SAMPLE DESCRIPTION Fine Reddish brown Collapsing sand - Undisturbed Berea Road
Sample, Air dried.

SPECIFIC GRAVITY 2,68

MASS SOIL SAMPLE

TEST NO. SA - BR - 1

Mass container + dry soil (g) 130,0

DATE 3-3-75

Mass container (g) 80,0

TESTED BY

mass dry soil (g)	50,0
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[illegible]

REMARKS: Sample wet sieved after hydrometer test to ensure that no fine particles adhered to the larger grains.

5011 SAMPLE DESCRIPTION Fine reddish brown Collapsing sand - Undisturbed Berea
Road sample, Air dried.

SPECIFIC GRAVITY 2,68

MASS SOUTHERN SAMPLE

TEST NO. SA-BR-2

Mass container + dry soil (g) 128,5

DATE 3-3-75

Mass container (g) 78,5

TESTED BY

mass dry soil (g) 50,0

[illegible]

REMARKS: Sample wet sieved after hydrometer test to ensure that no fine particles adhered to the larger grains.

B/11
CONSOLIDOMETER TEST

SAMPLE DESCRIPTION Berea Road - Fine reddish Brown Collapsing sand - Undisturbed
air dried sample.

SPECIFIC GRAVITY 2,68

TEST NO. C - BR - 1

TESTED BY _____

DATE 29-4-75

CONSOLIDOMETER NO. A

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (INITIAL) 892,5 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (INITIAL) 651,5 g

MASS SOIL + RING (INITIAL) 241,4 g

MASS RING 99,0 g

MASS SOIL (INITIAL) 142,4 g

DRY MASS SOIL 138,3 g

MASS WATER INITIAL 4,1 g

FIELD MOISTURE CONTENT % 3%

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (FINAL) 915,1 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (FINAL) 655,0 g

MASS SOIL + RING (FINAL) 260,1 g

MASS RING 99,0 g

MASS SOIL (FINAL) 161,1 g

DRY MASS SOIL 138,3 g

MASS WATER (FINAL) 22,8 g

FINAL MOISTURE CONTENT 16,5%

REMARKS:

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0	12:0000	Monday	Air dry	Load on arm	2100,0
0,25	12:0025	27-1 -75	"undisturbed"	varied from	2021,0
0,50	12:0050		sample	0 to 5 lbs.	2018,5
1,00	12:0100				2017,5
2,25	12:0225				2016,5
4,00	12:0400				2016,0
6,25	12:0625				2015,0
9,00	12:0900				2014,5
12,25	12:1225				2014,0
16,00	12:1600				2013,5
25,00	12:2500				2013,0
36,00	12:3600				2012,0
49,00	12:4900				2011,0
64,00	13:0400				2011,0
144,00	14:2400				2010,0
0	14:3000	Monday	Air dry	Load on arm	2010,0
0,25	14:3025	27-1-75	"undisturbed"	varied from	1981,5
0,50	14:3050		sample	5 to 10 lbs.	1980,0
1,00	14:3100				1979,0
2,25	14:3225				1978,0
4,00	14:3400				1977,0
6,25	14:3625				1976,0
9,00	14:3900				1975,5
12,25	14:4225				1975,0
16,00	14:4600				1974,5
25,00	14:5500				1974,0
36,00	15:0600				1973,5
49,00	15:1900				1973,0
64,00	15:3400				1972,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0	9:3000	Tuesday	Air dry sample	10lb reapplied	1972,0
0,25	9:3025	28-1-75	+ 2 ml of water	after strain	1953,5
0,50	9:3050			being kept	1952,5
1,00	9:3100			constant	1952,0
2,25	9:3225				1951,5
4,00	9:3400				1951,0
6,25	9:3625		Time of soaking		1950,5
9,00	9:3900		18 hrs.		1950,0
12,25	9:4225				1949,5
16,00	9:4600				1949,0
25,00	9:5500				1948,5
36,00	10:0600				1948,0
49,00	10:1900				1947,5
64,00	10:3400				1947,0
0	9:0000	Wednesday	Air dry sample	10lb reapplied	1947,0
0,25	9:0025	29-1-75	+ 4 ml. of water	after strain	1934,0
0,50	9:0050			being kept	1933,0
1,00	9:0100			constant	1932,5
2,25	9:0225				1932,0
4,00	9:0400				1931,5
6,25	9:0625				1931,0
9,00	9:0900				1930,5
12,25	9:1225				1930,0
16,00	9:1600				1929,5
25,00	9:2500				1929,0
36,00	9:3600		Time of soaking		1928,5
49,00	9:4900		22½ hrs.		1928,5
64,00	10:0400				1928,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:0000	Thursday	Air dry sample	101b reapplied	1928,0
0,25	9:0025	30-1-75	+ 6ml. of water	after strain	1913,5
0,50	9:0050			being kept	1912,5
1,00	9:0100			constant	1912,0
2,25	9:0225				1911,0
4,00	9:0400				1910,5
6,25	9:0625				1910,0
9,00	9:0900		Time of soaking		1910,0
12,25	9:1225		23 hrs.		1909,5
16,00	9:1600				1909,5
25,00	9:2500				1909,0
36,00	9:3600				1908,5
49,00	9:4900				1908,0
64,00	10:0400				1908,0
0,00	8:4500	Friday	Air dry sample	10 lb reapplied	1908,0
0,25	8:4525	31-1-75	+ 8ml. of water	after strain	1895,5
0,50	8:4550			being kept	1894,5
1,00	8:4600			constant	1894,0
2,25	8:4725				1893,5
4,00	8:4900				1893,0
6,25	8:5125				1892,5
9,00	8:5400				1892,0
12,25	8:5725		Time of soaking		1892,0
16,00	9:0100		23 hrs.		1891,5
25,00	9:1000				1891,0
36,00	9:2100				1890,5
49,00	9:3400				1890,0
64,00	9:4900				1889,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	10:4500	Saturday	Air dry sample	10lb. reapplied	1889,5
0,25	10:4525	1-2-75	+ 10ml. of water	after strain	1873,0
0,50	10:4550			being kept	1872,5
1,00	10:4600			constant	1872,0
2,25	10:4725				1871,0
4,00	10:4900				1870,0
6,25	10:5125				1869,5
9,00	10:5400		Time of soaking		1869,0
12,25	10:5725		25 hrs.		1868,5
16,00	11:0100				1868,0
25,00	11:1000				1867,5
36,00	11:2100				1866,5
49,00	11:3400				1866,0
64,00	11:4900				1865,5
0,00	9:4500	Monday	Air dry sample	10lb reapplied	1865,5
0,25	9:4525	3-2-75	+ 11ml. of water	after strain	1849,0
0,50	9:4550			being kept	1847,5
1,00	9:4600			constant	1845,5
2,25	9:4725				1844,0
4,00	9:4900				1842,5
6,25	9:5125				1841,5
9,00	9:5400				1840,5
12,25	9:5725		Time of soaking		1839,5
16:00	10:0100		46 hrs.		1838,5
25,00	10:1000				1837,5
36,00	10:2100				1836,5
49,00	10:3400				1835,5
64,00	10:4900				1835,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:4500	Tuesday	Air dry sample	10lb reapplied	1835,0
0,25	9:4525	4-2-75	+ 12ml. of water	after strain	1827,0
0,50	9:4550			being kept	1825,0
1,00	9:4600			constant	1822,5
2,25	9:4725				1820,0
4,00	9:4900		Time of soaking		1818,0
6,25	9:5125		23 hrs.		1816,0
9,00	9:5400				1815,0
12,25	9:5725				1814,0
16,00	10:0100				1813,0
25,00	10:1000				1812,0
36,00	10:2100				1810,0
49,00	10:3400				1809,0
64,00	10:4900				1808,0
0,00	8:4500	Wednesday	Air dry sample	10lb reapplied	1808,0
0,25	8:4525	5-2-75	+ 13 ml of water	after strain	1806,5
0,50	8:4550			being kept	1806,0
1,00	8:4600			constant	1805,5
2,25	8:4725		Time of soaking		1805,0
4,00	8:4900		22 hrs.		1805,0
6,25	8:5125				1804,5
9,00	8:5400				1804,0
12,25	8:5725				1803,5
16,00	9:0100				1803,0
25,00	9:1000				1802,5
36,00	9:2100				1802,0
49,00	9:3400				1801,0
64,00	9:4900				1800,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	8:4500	Thursday	Air dry sample	101b reapplied	1800,0
0,25	8:4525	6-2-75	+ 14ml. of water	after strain	1798,0
0,50	8:4550			being kept	1797,5
1,00	8:4600			constant	1797,0
2,25	8:4725				1796,0
4,00	8:4900		Time of soaking		1795,0
6,25	8:5125		23 hrs.		1794,5
9,00	8:5400				1794,0
12,25	8:5725				1793,5
16,00	9:0100				1793,0
25,00	9:1000				1792,5
36,00	9:2100				1791,5
49,00	9:3400				1791,0
64,00	9:4900				1790,5
0,00	8:4500	Friday	Air dry sample	101b reapplied	1790,5
0,25	8:4525	7-2-75	+ 15ml. of water	after strain	1788,0
0,50	8:4500			being kept	1787,5
1,00	8:4600			constant	1787,0
2,25	8:4725				1786,5
4,00	8:4900				1786,0
6,25	8:5125				1785,5
9,00	8:5400				1785,0
12,25	8:5725				1784,5
16,00	9:0100				1784,0
25,00	9:1000				1783,0
36,00	9:2100				1782,0
49,00	9:3400				1781,0
64,00	9:4900				1780,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	3:4500	Saturday	Air dry sample	10lb reapplied	1780,0
0,25	3:4525	8-2-75	+ 16ml. of water	after strain	1779,0
0,50	3:4550			being kept	1778,5
1,00	3:4600			constant	1778,0
2,25	3:4725				1777,5
4,00	3:4900				1777,0
6,25	3:5125		Time of soaking		1776,5
9,00	3:5400		30 hrs.		1776,0
12,25	3:5725				1775,5
16,00	4:0100				1775,0
25,00	4:1000				1774,5
36,00	4:2100				1774,0
49,00	4:3400				1773,5
64,00	4:4900				1773,0
0,00	3:1500	Sunday	Air dry sample	10lb reapplied	1773,0
0,25	3:1525	9-2-75	+ 17ml. of water	after strain	1772,0
0,50	3:1550			being kept	1771,5
1,00	3:1600			constant	1771,0
2,25	3:1725				1771,0
4,00	3:1900		Time of soaking		1770,5
6,25	3:2125		22½ hrs.		1770,5
9,00	3:2400				1770,0
12,25	3:2725				1770,0
16,00	3:3100				1769,5
25,00	3:4000				1769,5
36,00	3:5100				1769,0
49,00	4:0400				1769,0
64,00	4:1900				1768,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:1500	Monday	Air dry sample	101b reapplied	1768,5
0,25	9:1525	10-2-75	+ 18ml. of water	after strain	1767,5
0,50	9:1550			being kept	1767,5
1,00	9:1600			constant	1767,0
2,25	9:1725				1767,0
4,00	9:1900		Time of soaking		1766,5
6,25	9:2125		17hrs.		1766,0
9,00	9:2400				1766,0
12,25	9:2725				1765,5
16,00	9:3100				1765,5
25,00	9:4000				1765,0
36,00	9:5100				1764,0
49,00	10:0400				1763,0
64,00	10:1900				1762,5
0,00	9:0000	Tuesday	Air dry sample	101b reapplied	1762,5
0,25	9:0025	11-2-75	+ 19ml. of water	after strain	1761,5
0,50	9:0050			being kept	1761,5
1,00	9:0100			constant	1761,0
2,25	9:0225				1761,0
4,00	9:0400				1760,5
6,25	9:0625				1760,5
9,00	9:0900		Time of soaking		1760,5
12,25	9:1225		22 $\frac{3}{4}$ hrs.		1760,5
16,00	9:1600				1760,0
25,00	9:2500				1760,0
36,00	9:3600				1759,5
49,00	9:4900				1759,5
64,00	10:0400				1759,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:0000	Wednesday	Air dry sample	10lb reapplied	1759,0
0,25	9:0025	12-2-75	+ 20ml. of water	after strain	1758,5
0,50	9:0050			being kept	1758,0
1,00	9:0100			constant	1758,0
2,25	9:0225				1758,0
4,00	9:0400				1757,5
6,25	9:0625				1757,5
9,00	9:0900				1757,5
12,25	9:1225		Time of soaking		1757,5
16,00	9:1600		23 hrs.		1757,5
25,00	9:2500				1757,0
36,00	9:3600				1757,0
49,00	9:4900				1756,5
64,00	10:0400				1756,0
0,00	2:3000	Thursday	Air dry sample	10lb reapplied	1756,0
0,25	2:3025	13-2-75	+ 21ml of water	after strain	1755,0
0,50	2:3050			being kept	1755,0
1,00	2:3100			constant	1755,0
2,25	2:3225				1754,5
4,00	2:3400		Time of soaking		1754,5
6,25	2:3625		28½ hrs.		1754,0
9,00	2:3900				1754,0
12,25	2:4225				1754,0
16,00	2:4600				1753,5
25,00	2:5500				1753,5
36,00	3:0600				1753,0
49,00	3:1900				1752,5
64,00	3:3400				1752,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	2:1500	Monday	Air dry sample	Load on arm	1747,0
0,25	2:1525	17-2-75	+ 23ml of water	Varied from	1543,0
0,50	2:1550			10 to 20 lbs.	1534,0
1,00	2:1600				1526,0
2,25	2:1725				1519,0
4,00	2:1900				1515,0
6,25	2:2125				1512,0
9,00	2:2400				1510,0
12,25	2:2725				1508,0
16,00	2:3100				1507,0
25,00	2:4000				1505,0
36,00	2:5100				1503,0
49,00	3:0400				1502,0
64,00	3:1900				1501,0
0,00	3:2000	Monday	Air dry sample	Load on arm	1501,0
0,25	3:2025	17-2-75	+ 23ml of water	Varied from	1521,0
0,50	3:2050			20 to 5 lb.	1522,0
1,00	3:2100				1522,5
2,25	3:2225				1523,0
4,00	3:2400				1523,5
6,25	3:2625				1524,0
9,00	3:2900				1524,0
12,25	3:3225				1524,5
16,00	3:3600				1524,5
25,00	3:4500				1525,0
36,00	3:5600				1525,0
49,00	4:0900				1525,0
64,00	4:2400				1525,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:1500	Friday	Air dry sample	101b reapplied	1752,0
0,25	9:1525	14-2-75	+ 22ml of water	after strain	1752,0
0,50	9:1550			being kept	1752,0
1,00	9:1600			constant	1752,0
2,25	9:1725				1752,0
4,00	9:1900		Time of soaking		1752,0
6,25	9:2125		17 $\frac{3}{4}$ hrs.		1751,5
9,00	9:2400				1751,5
12,25	9:2725				1751,5
16,00	9:3100				1751,0
25,00	9:4000				1751,0
36,00	9:5100				1750,5
49,00	10:0400				1750,5
64,00	10:1900				1750,0
0,00	11:4500	Monday	Air dry sample	101b reapplied	1750,0
0,25	11:4525	17-2-75	+ 23ml of water	after strain	1750,0
0,50	11:4550			being kept	1750,0
1,00	11:4600			constant	1749,5
2,25	11:4725				1749,0
4,00	11:4900				1749,0
6,25	11:5125				1749,0
9,00	11:5400				1748,5
12,25	11:5725		Time of soaking		1748,5
16,00	12:0100		72 hrs.		1748,0
25,00	12:1000				1747,5
36,00	12:2100				1747,5
49,00	12:3400				1747,0
64,00	12:4900				1747,0

[illegible]


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0000 15
0001 4.107 11/03-14:11-
0002 0101: DIMENSION W(50),PAT(50),DATA(50),WCA(50),DEFL(50),E(50),TLOAD(50),
0003 STRESS(50),DELTAW(50),DELTA(50),WCA1(50),IBUF(1000),DEGSAT(50)
0004 0102: READ(8,1) TSTNO1,TSTNO2
0005 0103: 1 FORMAT(2A4)
0006 0104: WRITE(5,2) TSTNO1,TSTNO2
0007 0105: 2 FORMAT(1H1,'TEST NUMBER=',2A4)
0008 C TINTV IS EQUAL TO TOTAL INITIAL VOLUME IN MM CUBED
0009 0106: TINTV=3.142*(75.0**2)*20/4
0010 0107: PRINT 201,TINTV
0011 0110: 201 FORMAT (1H 'INITIAL VOLUME=',F10.3)
0012 C TH=MASS OF SOLIDS
0013 C GS=SPECIFIC GRAVITY
0014 C THIN=INITIAL MASS OF SAMPLE
0015 C THWC=INITIAL MOISTURE CONTENT
0016 C TFIN=FINAL TOTAL MASS OF THE SAMPLE
0017 0111: READ 101,TH,GS,THIN,TFIN
0018 0112: 101 FORMAT (1)
0019 0113: VSOLID=(1000*TH)/GS
0020 0114: VVOIDS=TINTV-VSOLID
0021 0115: EO=VVOIDS/VSOLID
0022 0116: THWC=(THIN-TH)/TH
0023 0117: PRINT 202,VSOLID
0024 0120: 202 FORMAT (1H/'VOLUME OF SOLIDS=',F10.3)
0025 0121: PRINT 203,EO
0026 0122: 203 FORMAT (1H 'INITIAL VOID RATIO=',F10.3)
0027 0123: PRINT 204,THWC
0028 0124: 204 FORMAT (1H 'INITIAL MOISTURE CONTENT=',F10.3)
0029 0125: READ 110,M
0030 0126: 110 FORMAT (1)
0031 0127: PRINT 401
0032 0130: 401 FORMAT(11111111,'ALL THE VOLUMES OUTPUT ARE IN MILLIMETERS CUBED')
0033 0131: PRINT 402
0034 0132: 402 FORMAT(1H,'THE VERTICAL STRESS IS IN KILONEWTONS PER SQUARE METER
0035 ')
0036 0133: PRINT 403
0037 0134: 403 FORMAT(1H,'THE DEFLECTION READINGS ARE IN TEN THOUSANDTHS OF AN
0038 INCH')
0039 0135: PRINT 205
0040 0136: 205 FORMAT(11111111,'DEFLECTION MOISTURE STRESS VOID
0041 , DELTA DEGREE')
0042 0137: PRINT 400
0043 0140: 400 FORMAT(1H,' READINGS CONTENT VERTICAL RATIO
0044 ,W SATURATION')
0045 C H IS THE NUMBER OF TEST CYCLES
0046 C S IS THE INITIAL DEFLECTION READING
0047 C Y IS THE INITIAL READING AT THE BEGINNING OF WC VARIATION
0048 C X IS THE FINAL READING AT THE END OF WC VARIATION
0049 0141: READ 111,S,Y,X
0050 0142: 111 FORMAT(1)
0051 0143: I=1
0052 0144: K=1
0053 0145: II=1
0054 0146: 12 READ 102,W11,TLOAD(K),DEFL(11)
0055 0147: 102 FORMAT(1)
C TLOAD IS THE LOAD APPLIED TO THE SAMPLE IN THE CONSOLIDOMETER

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B/24

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0056      0150:      I=I+1
0057      0151:      KK=KK+1
0058      0152:      II=II+1
0059      0153:      IF (I-N) 12,12,10
0060      0154:      -10 K=1
0061      0155:      I=1
0062      0156:      WAT(K)=(THIN-TM)+W(I)
0063      C      WAT(K) IS EQUAL TO THE MASS OF WATER IN THE SAMPLE
0064      0157:      -13 K=K+1
0065      0160:      I=I+1
0066      0161:      WAT(K)=(THIN-TM)+W(I)
0067      0162:      IF (I-N) 13,13,14
0068      0163:      -14 WATAC=TFIN-TM
0069      0164:      Z=WAT(K)/WATAC
0070      0165:      L=1
0071      0166:      I=1
0072      0167:      N=1
0073      0170:      LL=1
0074      0171:      KY=1
0075      0172:      JJ=1
0076      0173:      II=1
0077      0174:      MM=1
0078      0175:      NN=1
0079      0176:      DW=S-X
0080      C      WATA IS EQUAL TO THE ACTUAL AMOUNT OF WATER ADDED TO THE SAMPLE
0081      0177:      -18 WATA(L)=(TMIN-TM)+(1-Z)*W(I)
0082      0200:      WCA(L)=WATA(L)/TM
0083      C      DEGSAT IS THE DEGREE OF SATURATION OF THE SAMPLE
0084      C      WCA IS THE ACTUAL WATER CONTENT OF THE SAMPLE
0085      C      E IS THE VOID RATIO OF THE SAMPLE
0086      0201:      E(JJ)=(3.142*(75*21*(20-(15-DEFL(II)))*0.0001*25.4)/4
0087      ,-(1000*TM/GS))/(1000*TM/GS)
0088      0202:      DEGSAT(NN)=WCA(L)*GS/E(JJ)
0089      0203:      STRESS(LL)=(TLOAD(KK)*11.0*4.0/(3.142*75*21)*4.448*1000
0090      C      LEVER ARM RATIO IS 11 TO 1
0091      0204:      IF (N-1) 60,60,121
0092      0205:      -121 IF (WCA(N)-WCA(N-1)) 60,60,62
0093      0206:      60 DELTAW(MM)=0
0094      0207:      GO TO 63
0095      0210:      62 DELTAW(MM)=(DEFL(II)-X)/DW
0096      0211:      63 PRINT 206,DEFL(II),WCA(N),STRESS(LL),E(JJ),DELTAW(MM),DEGSAT(NN)
0097      0212:      206 FORMAT (1H ,F10.2,2X,F10.3,2X,F10.2,2X,F10.3,2X,F10.3,2X,F10.3)
0098      0213:      I=I+1
0099      0214:      N=N+1
0100      0215:      L=L+1
0101      0216:      II=II+1
0102      0217:      JJ=JJ+1
0103      0220:      KK=KK+1
0104      0221:      LL=LL+1
0105      0222:      MM=MM+1
0106      0223:      IF (I-N) 18,18,19
0107      0224:      19 N=1
0108      0225:      92 IF (WCA(N)-WCA(N-1)) 90,90,91
0109      0226:      90 N=N+1
0110      0227:      GO TO 93
0111      0230:      91 WCA(N)=WCA(N)
0112      0231:      MM=MM

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C113      0232:      DELTA(MM)=DELTA*(MM)
C114      0233:      N=N+1
C115      0234:      93 IF (N-N1) 92,92,74
C116      0235:      94 CALL PLOTS(IRUF,1000,17)
C117      0236:      CALL PLOT(3,0,10,0,-3)
C118      0237:      CALL AXIS(0,0, 0,0,19HDEFLECTION READINGS,-19,8,0,-90,0,2000,0,
C119      , -200,0)
C120      0240:      CALL AXIS(0,0, 0,0,16HMOISTURE CONTENT,+16,8,0,0,0,0,0,1)
C121      0241:      DEFL(M+1)=2000
C122      0242:      DEFL(M+2)=200
C123      0243:      WCAI(M+1)=0,0
C124      0244:      WCAI(M+2)=0,1
C125      0245:      CALL LINE(WCAI,DEFL,M,1,-1,2)
C126      0246:      CALL SYMBOL(0,0,1,0,0,21,
C127      , 40HDEFLECTIONS OBTAINED UNDER CONSTANT LOAD,0,0,+40)
C128      0247:      CALL PLOT(0,0,14,0,-3)
C129      0250:      CALL AXIS(0,0,-0,0,10HVOID RAT,10,-10,8,0,-90,0,1,0,-0,1)
C130      0251:      CALL AXIS(0,0, 0,0,6HSTRESS,+6,10,0,0,0,0,0,30,0)
C131      0252:      STRESS(M+2)=30,0
C132      0253:      STRESS(M+1)=0,0
C133      0254:      E(M+1)=1,0
C134      0255:      E(M+2)=0,1
C135      0256:      CALL LINE(STRESS,E,M,1,-1,2)
C136      0257:      CALL SYMBOL(0,5, 1,5,0,21,36HSTRESS WITH VARYING MOISTURE CONTENT,
C137      , 0,0,+36)
C138      0260:      CALL PLOT(12,0,-8,0,-3)
C139      0261:      CALL AXIS( 0,0,0,0,16HMOISTURE CONTENT,-16,8,0,0,0,0,0,1)
C140      0262:      CALL AXIS( 0,0,0,0,11HDELTA WATER,+11,5,0,+90,0,0,0,0,1)
C141      0263:      DELTA(M+1)=0,0
C142      0264:      DELTA(M+2)=0,2
C143      0265:      WCAI(M+2)=0,1
C144      0266:      WCAI(M+1)=0,0
C145      0267:      CALL LINE(WCAI,DELTA,M,1,-1,2)
C146      0270:      CALL SYMBOL(0,5,9,5,0,21,
C147      , 40HExtra SETTLEMENT VERSUS MOISTURE CONTENT,0,0,+40)
C148      0271:      CALL PLOT(12,0,2,5,999)
C149      0272:      STOP
C150      0273:      END

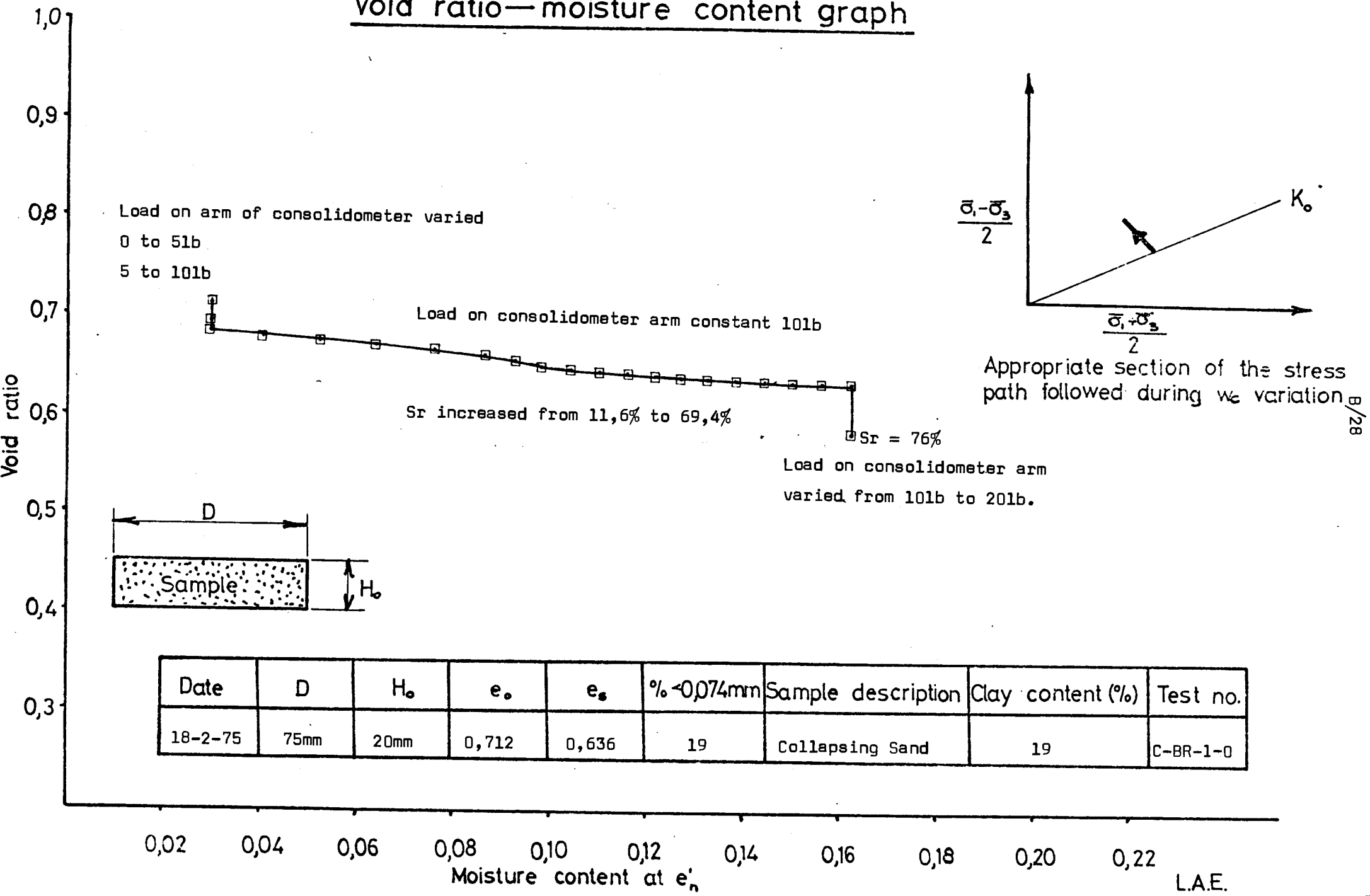
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TEST NUMBER=C-RR-1-0
INITIAL VOLUME= 88368.749
VOLUME OF SOLIDS= 51604.477
INITIAL VOID RATIO= .712
INITIAL MOISTURE CONTENT= .030

ALL THE VOLUMES OUTPUT ARE IN MILLIMETERS CUBED
THE VERTICAL STRESS IS IN KILONEWTONS PER SQUARE METER
THE DEFLECTION READINGS ARE IN TEN THOUSANDTHS OF AN INCH

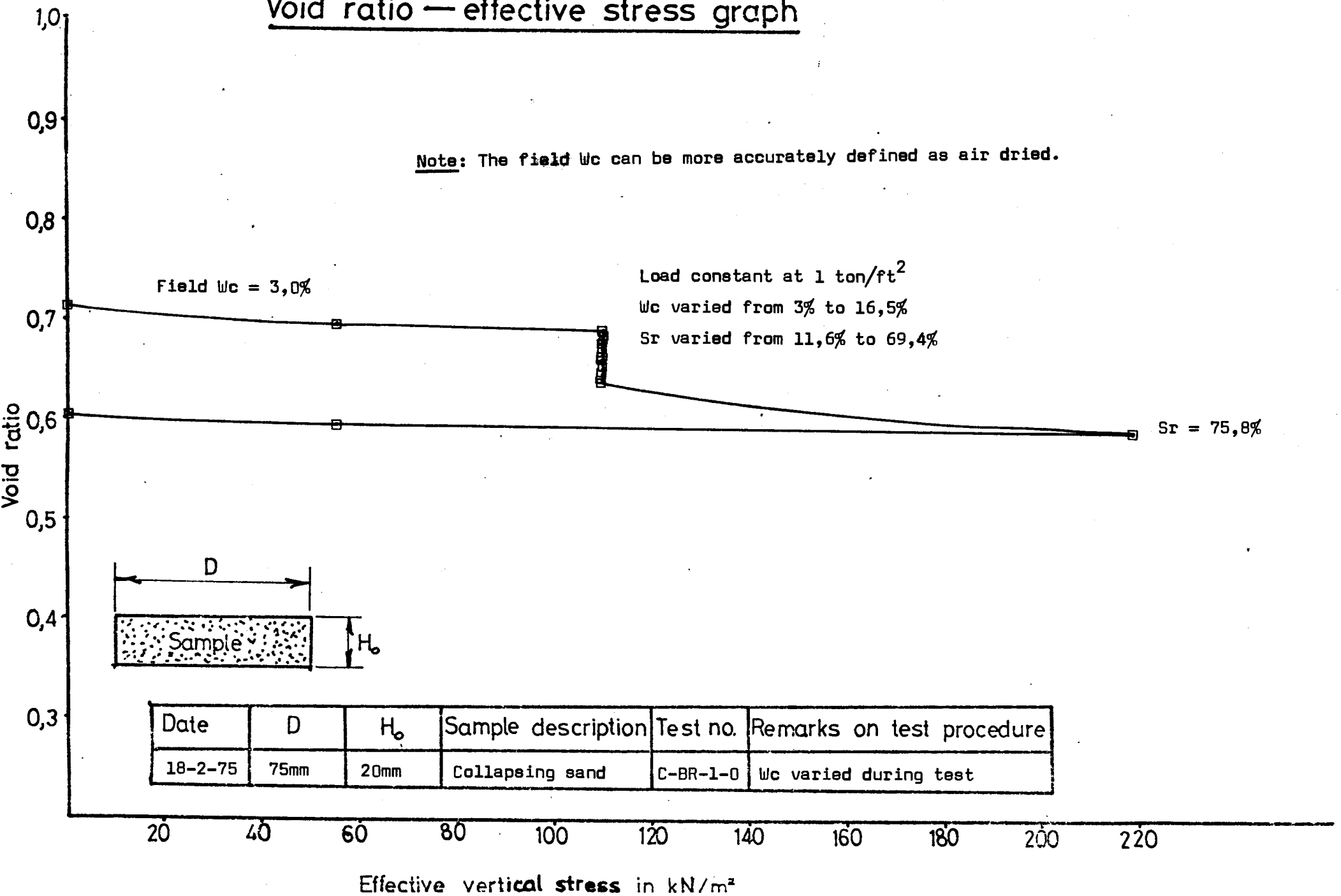
DEFLECTION READINGS	MOISTURE CONTENT	STRESS VERTICAL	VOID RATIO	DELTA W	DEGREE SATURATION
2010.00	.030	55.37	.693	.000	.115
1972.50	.030	110.74	.685	.000	.116
1947.00	.041	110.74	.679	.567	.163
1928.00	.053	110.74	.675	.513	.211
1908.00	.065	110.74	.671	.456	.259
1869.50	.077	110.74	.667	.404	.308
1865.50	.088	110.74	.661	.336	.358
1835.00	.094	110.74	.655	.249	.386
1808.00	.100	110.74	.649	.173	.413
1810.00	.106	110.74	.647	.150	.439
1790.50	.112	110.74	.645	.123	.465
1780.00	.118	110.74	.643	.093	.491
1773.00	.124	110.74	.641	.074	.516
1760.50	.129	110.74	.640	.061	.542
1742.50	.135	110.74	.639	.044	.568
1759.00	.141	110.74	.638	.034	.593
1756.00	.147	110.74	.638	.025	.618
1752.00	.153	110.74	.637	.014	.644
1750.00	.159	110.74	.636	.008	.669
1747.00	.165	110.74	.636	.000	.694
1501.00	.165	221.47	.582	.000	.758
1525.50	.165	55.37	.587	.000	.751
1570.00	.165	.00	.597	.000	.739

Void ratio—moisture content graph



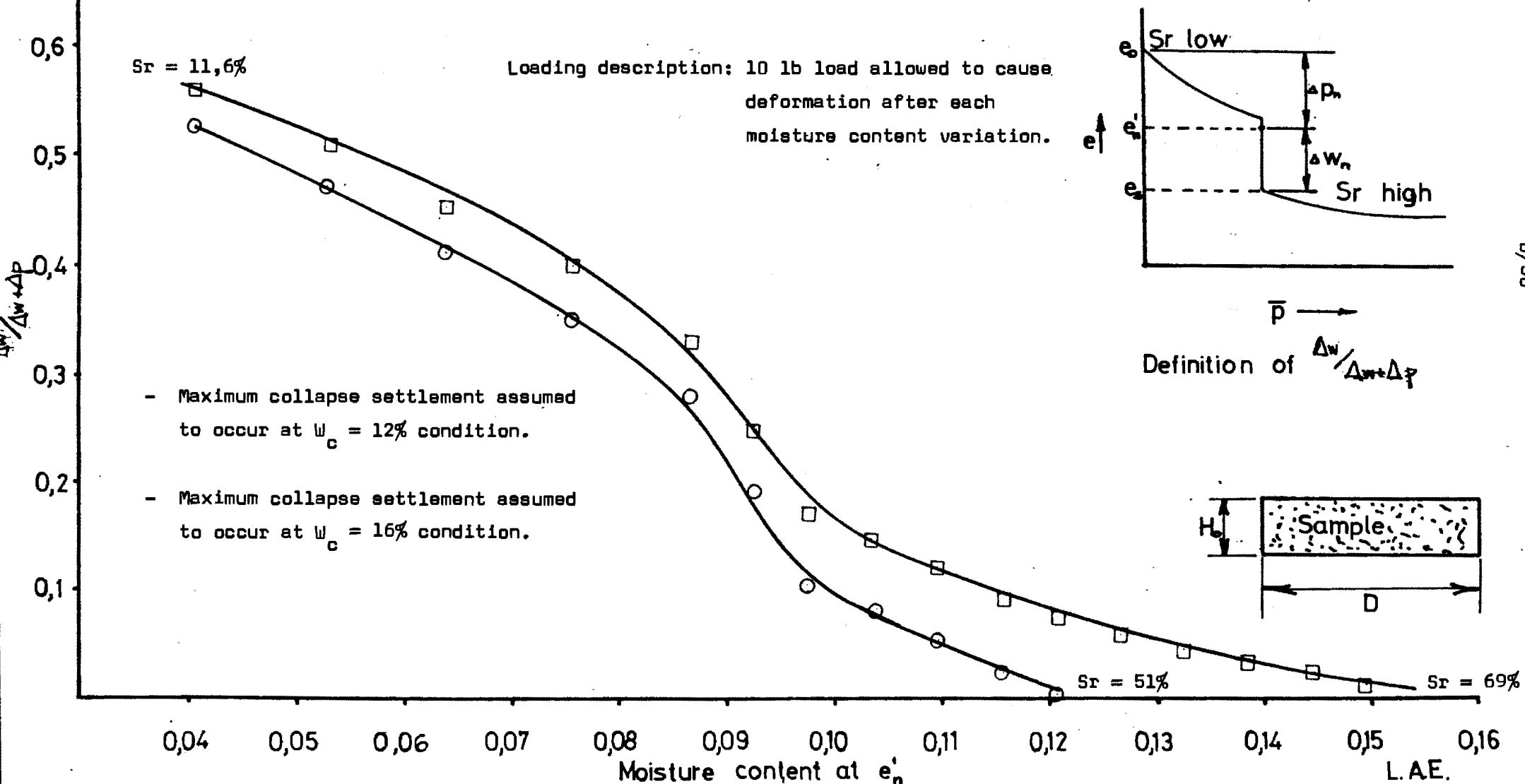
Void ratio — effective stress graph

Note: The field w_c can be more accurately defined as air dried.



$\frac{\Delta w}{\Delta w + \Delta p}$ - moisture content graph

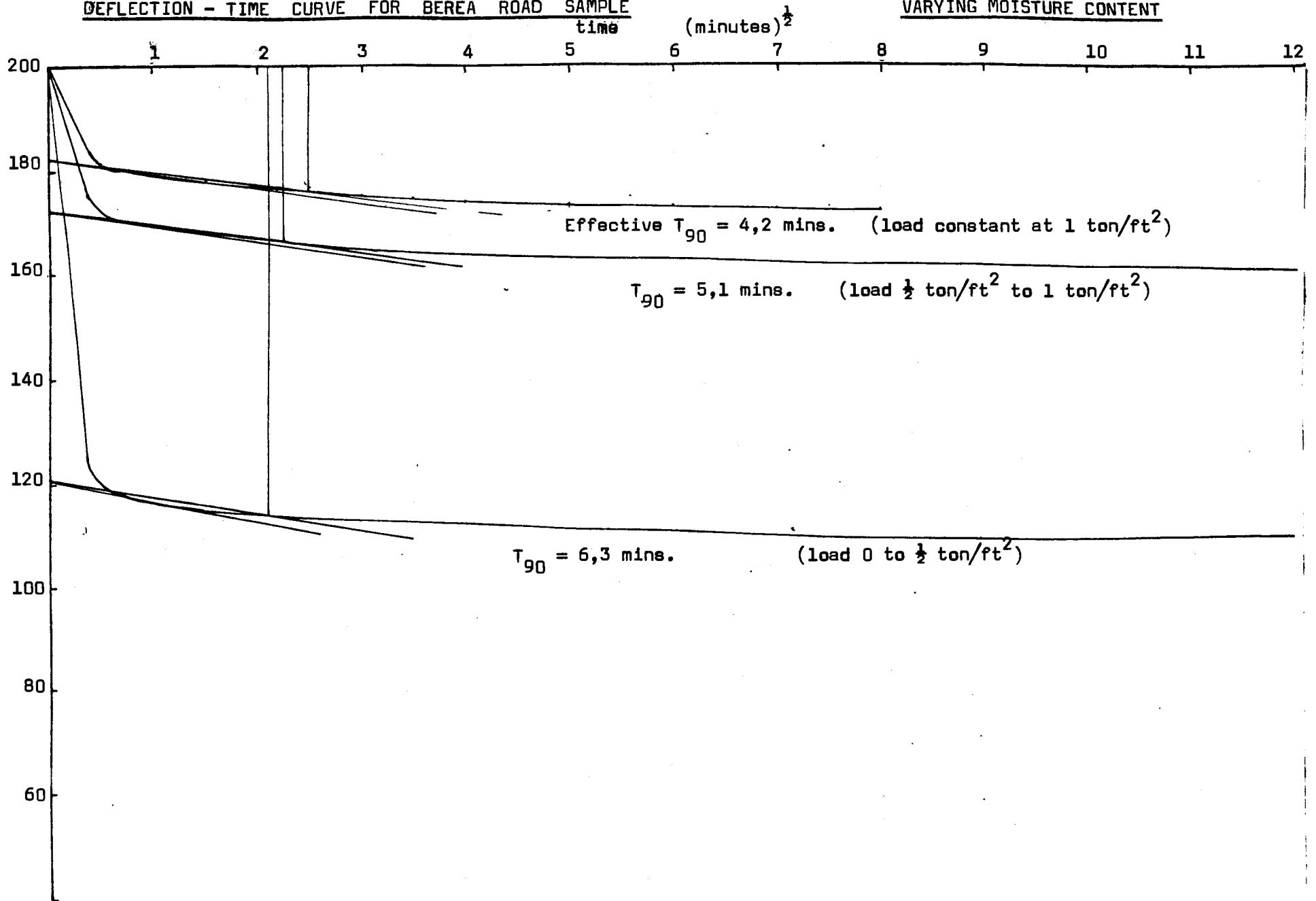
Date	D	H ₀	e ₀	e _s	% < 0,075 mm	Sample description	Clay content (%)	Test no.
18/2/75	75 mm	20 mm	0,712	0,636	19	collapsing sand	19	C-BR-1-0



DEFLECTION - TIME CURVE FOR BEREA ROAD SAMPLE

VARYING MOISTURE CONTENT

Dial gauge readings referred to a common origin



507L SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample
taken from "Feathers"

SPECIFIC GRAVITY 2.68

WEIGHT SOIL SAMPLE

TEST NO. H-FS-1

Mass container + dry soil (g) 130,0

DATE 29/4/75

Mass container (g) 80,0

TESTED BY L.A.E.

Mass dry soil (g) 50,0

HYDROMETER NO. 9843 A.S.T.M. 151-H

DISPERSING AGENTS 10 ml Sodium Oxalate Solution

10 ml Sodium Silicate Solution

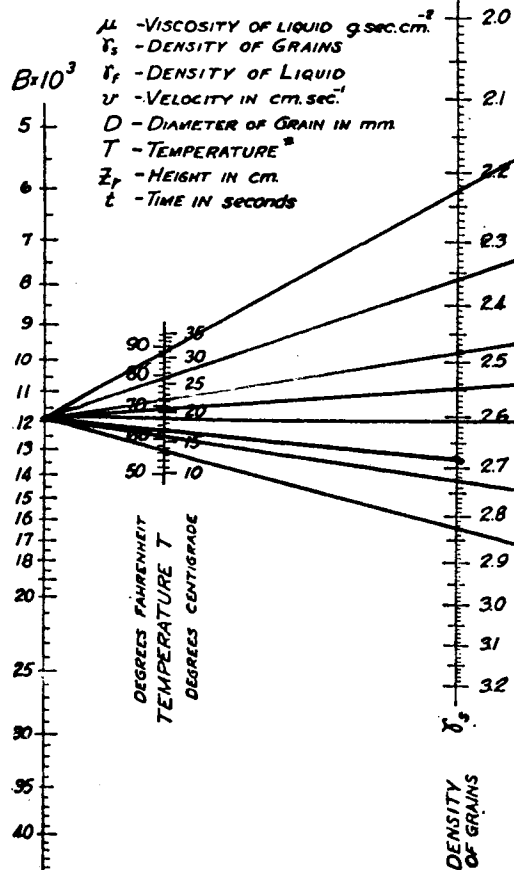
[illegible]

REMARKS:

Sample soaked for 23 hours.

For the 2 and 5 minute readings Z_{u} uncorrected is used.

NOMOGRAPHIC CHART FOR SOLUTION OF STOKES' LAW



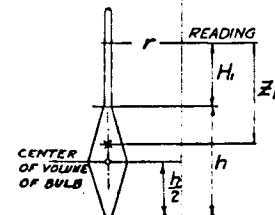
ESTIMATED TIME-AVERAGE OVER THE PERIOD FROM THE START OF THE TEST TO THE TIME WHEN HYDROMETER READING IS MADE.

STOKES' LAW:

$$D = \sqrt{B \cdot v}$$

$$B = \frac{1800\mu}{\gamma_s - \gamma_l}$$

$$v = \frac{Z_f}{t}$$



HEIGHT H WHICH CORRESPONDS TO READING r DETERMINED FROM

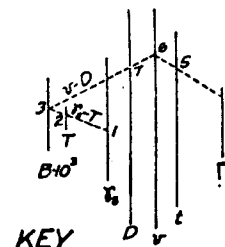
$$Z_f = H + \frac{1}{2} \left(h \cdot \frac{\text{VOLUME OF HYDR. BULB}}{\text{AREA OF GRADUATE}} \right) \text{ CONSTANT}$$

Z_f TO BE DETERMINED FOR DIFFERENT VALUES OF r. CORRESPONDING VALUES OF r TO BE PLOTTED ON RIGHT SIDE OF (Z_f , r) SCALE AND CONVENIENT SUBDIVISIONS MADE.

FOR SOIL SUSPENSIONS IN WATER ANY HYDROMETER MEASURING DENSITIES BETWEEN 0.995 AND 1.040 WITH AN ACCURACY OF 0.0002 MAY BE USED.

SUGGESTED: CALIBRATION AT 20°C. IN DENSITIES, STREAM LINE BULB. MAX. H_1 = 14 TO 16 CM. h = 15 TO 17 CM.

FOR LIQUIDS OTHER THAN WATER THE (B) VALUES MUST BE COMPUTED THE (γ_s) AND (T) SCALES APPLY ONLY TO SUSPENSIONS IN WATER.



KEY

HYDROMETER ANALYSTS

501. SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample
taken from "Feathers"

SPECIFIC GRAVITY 2.68

WEIGHT SOIL SAMPLE

TEST NO. H-F9-2

Mass container + dry soil (g) 155.1

DATE 29/4/75

Mass container (g) 105,1

TESTED BY

Mass dry soil (g) 50.0

HYDROMETER NO. 9843 A.S.T.M. 151 H

DISPERSING AGENTS 10 ml Sodium Oxalate Solution

10 ml Sodium Silicate Solution

[illegible]

REMARKS:

Sample soaked for 23 hours.

For the 2 and 5 minute readings Z_{∞} uncorrected is used.

NOMOGRAPHIC CHART FOR SOLUTION OF STOKES' LAW

μ - VISCOSITY OF LIQUID g.sec.cm.⁻²
 δ_s - DENSITY OF GRAINS
 δ_f - DENSITY OF LIQUID
 v - VELOCITY IN cm.sec.⁻¹
 D - DIAMETER OF GRAIN IN mm.
 T - TEMPERATURE °
 Z_r - HEIGHT IN cm.
 t - TIME IN SECONDS

$B \times 10^3$

5
6
7
8
9
10
11
12
13
14
15
16
17
18
20
25
30
35
40

90
80
70
60
50
 DEGREES FAHRENHEIT
TEMPERATURE T
DEGREES CENTIGRADE

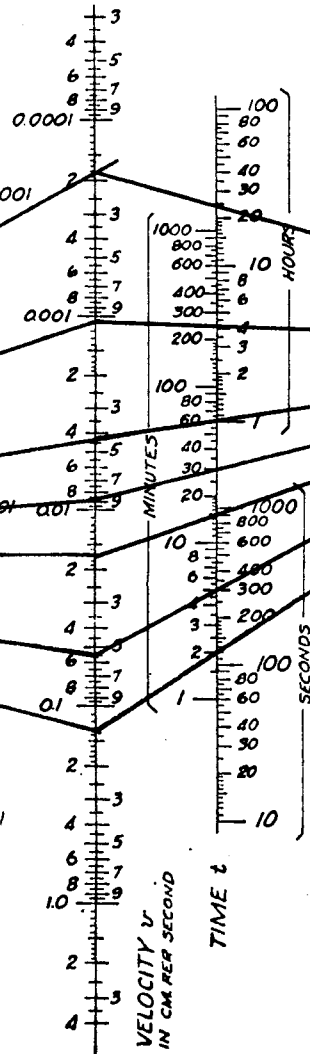
DENSITY OF GRAINS

δ_s

DIAMETER D IN MM

VELOCITY v IN CM PER SECOND

TIME t



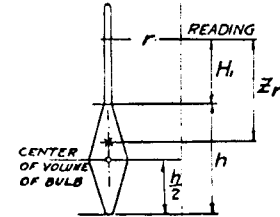
STOKES' LAW:

$$D = \sqrt{Bv}$$

$$B = \frac{1800\mu}{\delta_s - \delta_f}$$

$$v = \frac{Z_r}{t}$$

30
25
20
18
16
14
12
10
9
8
7
6
5
 HEIGHT IN CM
 Z_r



HEIGHT H WHICH CORRESPONDS TO READING r DETERMINED FROM

$$Z_r = H + \frac{1}{2} \left(\frac{\text{VOLUME OF HYDR. BULB}}{\text{AREA OF GRADUATE}} \right) \text{ CONSTANT}$$

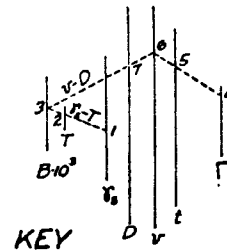
HYDROMETER READING

Z_r TO BE DETERMINED FOR DIFFERENT VALUES OF r . CORRESPONDING VALUES OF r TO BE PLOTTED ON RIGHT SIDE OF (Z_r, r) SCALE AND CONVENIENT SUBDIVISIONS MADE.

FOR SOIL SUSPENSIONS IN WATER ANY HYDROMETER MEASURING DENSITIES BETWEEN 0.995 AND 1.040 WITH AN ACCURACY OF 0.0002 MAY BE USED.

SUGGESTED: CALIBRATION AT 20°C. IN DENSITIES. STREAM LINE BULB. MAX. $H_1 = 14$ TO 16 CM. $h = 15$ TO 17 CM.

FOR LIQUIDS OTHER THAN WATER THE (B) VALUES MUST BE COMPUTED THE (δ_s) AND (T) SCALES APPLY ONLY TO SUSPENSIONS IN WATER.



KEY

ESTIMATED TIME-AVERAGE OVER THE PERIOD FROM THE START OF THE TEST TO THE TIME WHEN HYDROMETER READING IS MADE.

SIEVE ANALYSIS

SPECIFIC GRAVITY 2,68

MASS SOIL SAMPLE

TEST NO. SA - FS - 1

Mass container + dry soil (g) 1856,4

DATE 25-4-75

Mass container (g) 129,5

TESTED BY

Mass dry soil (g) 1726,9

[illegible]

REMARKS: Sample dry - sieved.

SIEVE ANALYSIS

SOIL SAMPLE DESCRIPTION	Decomposed granitic residual soil - Undisturbed sample taken from "Feathers".
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SPECIFIC GRAVITY 2,68

MASS SOIL SAMPLE

TEST NO. SA - FS - 2

Mass container + dry soil (g)

DATE 25-4-75

Mass container (g)

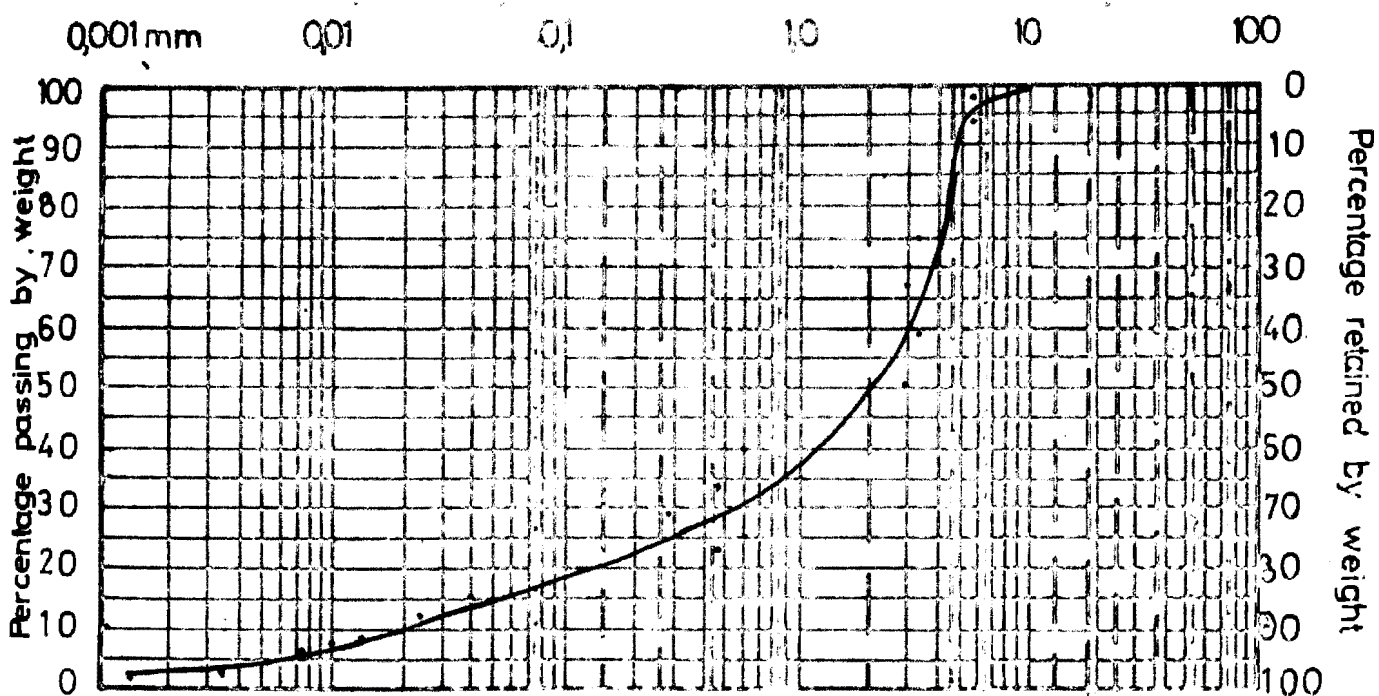
TESTED BY

mass dry soil (g) 1310,0

[illegible]

REMARKS: Sample Wet sieved and then oven dried.

Sample description	Decomposed granite
Sample source	Feathers
Test number	H-FS-1, H-FS-2, SA-FS-2
Dispersing agent	



U.S. Sieve	200	100	50	40	20	10	4	1/4	1/2	3/4	1	1 1/2	2	3	4
B.S. Sieve	200	100	52	36	25	14	7	3/8	1/2	3/4	1	1 1/2	2	3	4

CONSOLIDOMETER TEST

SAMPLE DESCRIPTION Decomposed granitic residual soil - Undisturbed sample taken from "Feathers"

SPECIFIC GRAVITY 2,68

TEST NO. C - FS - 1

TESTED BY _____

DATE 29-4-75

CONSOLIDOMETER NO. B

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (INITIAL) 880,8 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (INITIAL) 653,6 g

MASS SOIL + RING (INITIAL) 227,2 g

MASS RING 97,5 g

MASS SOIL (INITIAL) 130,7 g

DRY MASS SOIL 123,5 g

MASS WATER INITIAL 7,2 g

FIELD MOISTURE CONTENT % 5,8%

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (FINAL) 895,6 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (FINAL) 657,2 g

MASS SOIL + RING (FINAL) 238,4 g

MASS RING 97,5 g

MASS SOIL (FINAL) 140,9 g

DRY MASS SOIL 123,5 g

MASS WATER (FINAL) 17,4 g

FINAL MOISTURE CONTENT 14,0%

REMARKS: Irregularities were observed in the void ratio moisture content curves.

This could be for the following reasons.

(a) Thixotropy

(b) The breaking of the cementing between the particles and allowing the water to enter and then allowing free movement of all particles.

(c) Sample compressing in layers due to side friction.

Reasons (b) and (c) seem the most probable.

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0	3:3000	Tuesday	Field Wc	Load on arm	2000,0
0,25	3:3025	29/4/75		varied from	1916,0
0,50	3:3050			0 to 5 lb's	1913,5
1,00	3:3100				1911,0
2,25	3:3225				1908,0
4,00	3:3400				1905,5
6,25	3:3625				1904,0
9,00	3:3900				1902,5
12,25	3:4225				1901,5
16,00	3:4600				1900,0
25,00	3:5500				1897,5
36,00	4:0600				1896,0
49,00	4:1900				1895,0
64,00	4:3400				1894,0
81,00	4:3100				1893,0
0	9:0000	Wednesday	Field Wc	Load on arm	1893,0
0,25	9:0025	30/4/75		varied from	1827,0
0,50	9:0050			5 to 10 lb's	1823,0
1,00	9:0100				1820,0
2,25	9:0225				1815,0
4,00	9:0400				1812,0
6,25	9:0625				1810,5
9,00	9:0900				1809,0
12,25	9:1225				1802,0
16,00	9:1600				1805,0
25,00	9:2500				1804,0
36,00	9:3600				1803,0
49,00	9:4900				1801,0
64,00	10:0400				1800,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
81,00	10:2100	30/4/75	Field Wc	5 to 10 lbs	1799,0
0	II:0000	Thursday	Field Wc	10lb reapplied	1799,0
0,25	II:0025	1/5/75	+ 2 ml of water	after strain	1727,5
0,50	II:0050			being kept	1722,0
1,00	II:0100			constant	1719,0
2,25	II:0225				1715,5
4,00	II:0400				1713,0
6,25	II:0625				1711,5
9,00	II:0900				1710,0
12,25	II:1225				1709,0
16,00	II:1600				1708,0
25,00	II:2500				1707,0
36,00	II:3600				1705,5
49,00	II:4900				1704,5
64,00	12:0400				1703,5
81,00	12:2100				1703,0
0	9:3000	Friday	Field Wc	10lb reapplied	1703,0
0,25	9:3025	2/5/75	+ 4 ml of water	after strain	1520,0
0,50	9:3050			being kept	1510,0
1,00	9:3100			constant	1502,5
2,25	9:3225				1494,5
4,00	9:3400				1490,0
6,25	9:3625				1488,0
9,00	9:3900				1485,0
12,25	9:4225				1483,0
16,00	9:4600				1481,0
25,00	9:5500				1479,0
36,00	10:0600				1477,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
49,00	10:1900	Friday	Field Wc + 4ml	I01b reapplied	I475,0
64,00	10:3400				I474,0
81,00	10:5100				I473,0
0	9:0000	Monday	Field Wc	I01b reapplied	I473,0
0,25	9:0025	5/5/75	+ 5 ml water	after strain	I469,0
0,50	9:0050			being kept	I468,5
1,00	9:0100			constant	I468,0
2,25	9:0225				I467,0
4,00	9:0400				I466,0
6,25	9:0625				I465,0
9,00	9:0900				I464,5
12,25	9:1225				I464,0
16,00	9:1600				I463,5
25,00	9:2500				I462,5
36,00	9:3600				I462,0
49,00	9:4900				I461,0
64,00	10:0400				I460,5
81,00	10:2100				I460,0
0,00	9:4500	Tuesday	Field Wc	I01b reapplied	I460,0
0,25	9:4525	6/5/75	+ 6 ml water	after strain	I456,0
0,50	9:4550			being kept	I454,0
1,00	9:4600			constant	I444,0
2,25	9:4725				I434,0
4,00	9:4900				I424,0
6,25	9:5125				I417,0
9,00	9:5400				I412,5
12,25	9:5725				I409,5
16,00	10:0100				I407,5
25,00	10:1000				I404,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
36,00	10:2100	Tuesday	Field Wc	I01b reapplied	I402,5
49,00	10:3400	6/5/75	+ 6 ml water	after strain	I400,5
64,00	10:4900			being kept	I399,5
81,00	11:0600				I398,5
0,00	9:1500	Wednesday	Field Wc	I01b reapplied	I398,5
0,25	9:1525	7/5/75	+ 7 ml water	after strain	I395,5
0,50	9:1550			being kept	I394,0
1,00	9:1600			constant	I392,0
2,25	9:1725				I388,5
4,00	9:1900				I379,0
6,25	9:2125				I375,0
9,00	9:2400				I371,0
12,25	9:2725				I366,0
16,00	9:3100				I363,0
25,00	9:4000				I358,5
36,00	9:5100				I355,5
49,00	10:0400				I353,0
64,00	10:1900				I351,0
81,00	10:3600				I350,0
100,00	10:5500				I349,0
0,00	9:4500	Friday	Field Wc	I01b reapplied	I349,0
0,25	9:4525	9/5/75	+ 8 ml water	after strain	I348,0
0,50	9:4550			being kept	I342,0
1,00	9:4600			constant	I347,5
2,25	9:4725				I347,0
4,00	9:4900				I346,0
6,25	9:5125				I346,0
9,00	9:5400				I344,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
12,25	9:5725	Friday	Field Wc	10 lb reapplied	I344,5
16,00	10:0100	9/5/75	+ 8 ml water	after strain	I343,0
25,00	10:1000			being kept	I342,0
36,00	10:2100			constant	I339,5
49,00	10:3400				I337,5
64,00	10:4900				I336,0
81,00	11:0600				I335,0
100,00	11:2500				I334,0
0,00	8:4500	Monday	Field Wc	10lb reapplied	I334,0
0,25	8:4525	12/5/75	+ 9 ml water	after strain	I331,5
0,50	8:4550			being kept	I331,0
1,00	8:4600			constant	I330,5
2,25	8:4725				I330,5
4,00	8:4900				I330,0
6,25	8:5125				I329,5
9,00	8:5400				I329,0
12,25	8:5725				I328,5
16,00	9:0100				I328,0
25,00	9:1000				I327,0
36,00	9:2100				I325,0
49,00	9:3400				I322,0
64,00	9:4900				I319,0
81,00	10:0600				I317,0
100,00	10:2500				I315,0
121,00	10:4600				I313,0
144,00	11:0900				I311,0
169,00	11:3400				I310,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	8:4500	Tuesday	Field Wc	I01b reapplied	I310,0
0,25	8:4525	13/5/75	+ 10 ml water	after strain	I309,0
0,50	8:4550			being kept	I308,5
1,00	8:4600			constant	I308,0
2,25	8:4725				I307,5
4,00	8:4900				I304,5
6,25	8:5125				I301,5
9,00	8:5400				I289,0
12,25	8:5725				I280,0
16,00	9:0100				I270,5
25,00	9:1000				I258,0
36,00	9:2100				I250,0
49,00	9:3400				I246,0
64,00	9:4900				I243,0
81,00	10:0600				I241,0
100,00	10:2500				I239,5
121,00	10:4600				I239,0
144,00	11:0900				I238,0
169,00	11:3400				I237,0
0,00	8:4500	Wednesday	Field Wc	I01b reapplied	I237,0
0,25	8:4525	14/5/75	+ 11 ml water	after strain	I236,5
0,50	8:4550			being kept	I236,5
1,00	8:4600			constant	I236,0
2,25	8:4725				I236,0
4,00	8:4900				I235,5
6,25	8:5125				I235,5
9,00	8:5400				I235,0
12,25	8:5725				I234,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
16,00	9:0100	Wednesday	Field Wc	I01b reapplied	I234,0
25,00	9:1000	19/5/75	+ 11 ml water	after strain	I233,0
36,00	9:2100			being kept	I231,5
49,00	9:3400			constant	I228,0
64,00	9:4900				I224,0
81,00	10:0600				I220,0
100,00	10:2500				I217,0
121,00	10:4600				I213,0
144,00	11:0900				I210,0
169,00	11:3400				I208,0
196,00	12:0100				I204,0
0,00	8:4500	Thursday	Field Wc	I01b reapplied	I207,0
0,25	8:4525	15/5/75	+ 12 ml water	after strain	I206,5
0,50	8:4550			being kept	I206,0
1,00	8:4600			constant	I206,0
2,25	8:4725				I205,5
4,00	8:4900				I205,0
6,25	8:5125				I204,5
9,00	8:5400				I204,0
12,25	8:5725				I203,5
16,00	9:0100				I203,0
25,00	9:1000				I202,0
36,00	9:2100				1199,5
49,00	9:3400				1197,0
64,00	9:4900				1193,0
81,00	10:0600				1189,0
100,00	10:2500				1186,0
121,00	10:4600				1182,0
144,00	11:0900				1179,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
I69,00	II:3400	Thursday	Field Wc	I01b reapplied	II76,5
I96,00	I2:0100	I5/5/75	+ I2 ml water	after strain	II75,0
225,00	I2:3000			being kept	II74,0
				constant	
0,00	8:4500	Friday	Field Wc	I01b reapplied	II74,0
0,25	8:4525	I6/5/75	+ I3 ml water	after strain	II73,5
0,50	8:4550			being kept	II73,5
I,00	8:4600			constant	II73,0
2,25	8:4725				II72,5
4,00	8:4900				II72,0
6,25	8:5125				II71,5
9,00	8:5400				II70,5
I2,25	8:5725				II69,0
I6,00	9:0100				II67,5
25,00	9:1000				II60,0
36,00	9:2100				II46,0
49,00	9:3400				II32,0
64,00	9:4900				II25,0
81,00	10:0600				II20,0
I00,00	10:2500				III7,5
I21,00	10:4600				III5,0
I44,00	II:0900				III3,5
I69,00	II:3400				III2,5
I96,00	I2:0100				III1,5
225,00	I2:3000				III0,5
0,00	8:4500	Monday	Field Wc	I01b reapplied	III0,5
0,25	8:4525	I9/5/75	+ I4 ml water	after strain	III0,0
0,50	8:4550			being kept	III0,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
1,00	8:4600	Monday	Field Wc	I01b reapplied	II10,0
2,25	8:4725	19/5/75	+ 14 ml water	after strain	II10,0
4,00	8:4900			being kept	II10,0
6,25	8:5125			constant	II09,5
9,00	8:5400				II09,5
12,25	8:5725				II09,5
16,00	9:0100				II09,5
25,00	9:1000				II09,0
36,00	9:2100				II09,0
49,00	9:3400				II09,0
64,00	9:4900				II08,5
81,00	10:0600				II08,5
100,00	10:2500				II08,5
121,00	10:4600				II08,5
144,00	11:0900				II08,0
169,00	11:3400				II08,0
196,00	12:0100				II08,0
225,00	12:3000				II08,0
0,00	8:4500	Tuesday	Field Wc	I01b reapplied	II08,0
0,25	8:4525	20/5/75	+ 15 ml Water	after strain	II08,0
0,50	8:4550			being kept	II08,0
1,00	8:4600			constant	II08,0
2,25	8:4725				II08,0
4,00	8:4900				II08,0
6,25	8:5125				II08,0
9,00	8:5400				II08,0
12,25	8:5725				II08,0
16,00	9:0100				II07,5
25,00	9:1000				II07,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
36,00	9:2100	Tuesday	Field Wc	I01b reapplied	1107,5
49,00	9:3400	20/5/75	+ 15 ml water	after strain	1107,5
64,00	9:4900			being kept	1107,0
81,00	10:0600			constant	1107,0
100,00	10:2500				1107,0
121,00	10:4600				1107,0
144,00	11:0900				1106,5
169,00	11:3400				1106,5
196,00	12:0100				1106,5
225,00	12:3000				1106,0
0,00	2:3000	Wednesday	Field Wc	I01b reapplied	1106,0
0,25	2:3025	21/5/75	+ 15 ml water	after strain	94,0
0,50	2:3050			being kept	82,0
1,00	2:3100			constant	66,0
2,25	2:3225				52,5
4,00	2:3400				48,0
6,25	2:3625				45,5
9,00	2:3900				43,5
12,25	2:4225				42,5
16,00	2:4600				41,5
25,00	2:5500				39,5
36,00	3:0600				38,5
49,00	3:1900				37,5
64,00	3:3400				36,5
81,00	3:5100				35,5
100,00	4:1000				35,0
121,00	4:3100				34,0

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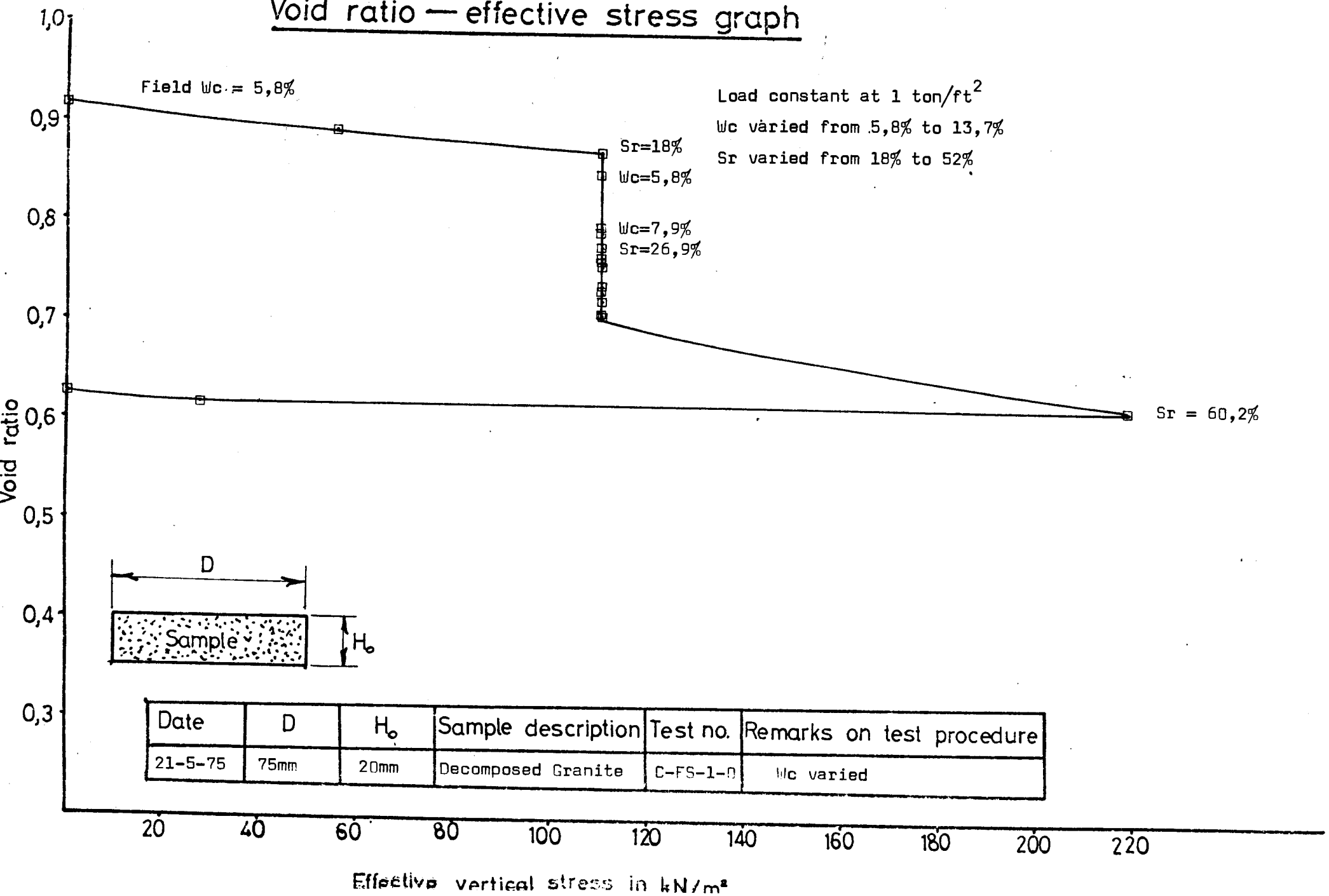
TEST NUMBER=C-F5-1-0
 INITIAL VOLUME= 88368.749
 VOLUME OF SOLIDS= 46082.089
 INITIAL VOID RATIO= .918
 INITIAL MOISTURE CONTENT= .058

ALL THE VOLUMES OUTPUT ARE IN MILLIMETERS CUBED
 THE VERTICAL STRESS IS IN KILONEWTONS PER SQUARE METER
 THE DEFLECTION READINGS ARE IN TEN THOUSANDTHS OF AN INCH

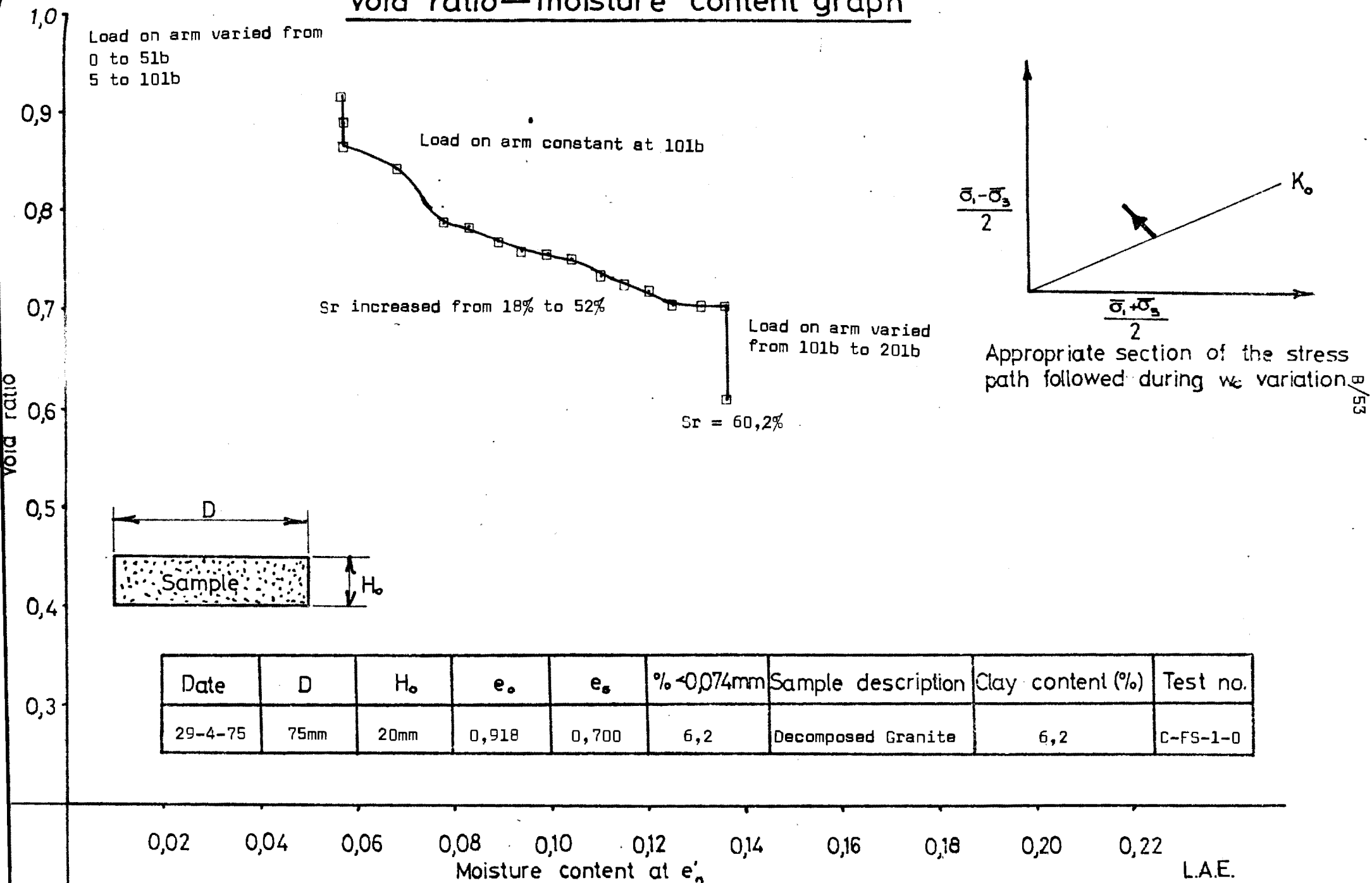
DEFLECTION READINGS	MOISTURE CONTENT	STRESS VERTICAL	VOID RATIO	DELTA W	DEGREE SATURATION
1893.00	.058	55.37	.892	.000	.175
1799.00	.058	110.74	.869	.000	.180
1703.00	.069	110.74	.845	.668	.218
1473.00	.079	110.74	.789	.411	.269
1460.00	.084	110.74	.786	.396	.288
1398.50	.090	110.74	.771	.327	.312
1349.00	.095	110.74	.759	.272	.335
1334.00	.100	110.74	.755	.255	.356
1310.00	.105	110.74	.750	.228	.377
1237.00	.111	110.74	.732	.147	.405
1208.00	.116	110.74	.725	.114	.429
1174.00	.121	110.74	.716	.076	.453
1110.50	.126	110.74	.701	.005	.483
1108.00	.132	110.74	.700	.002	.504
1106.00	.137	110.74	.700	.000	.524
734.00	.137	221.47	.609	.000	.602
759.00	.137	27.68	.615	.000	.596
796.00	.137	.00	.624	.000	.588

B/51

Void ratio — effective stress graph

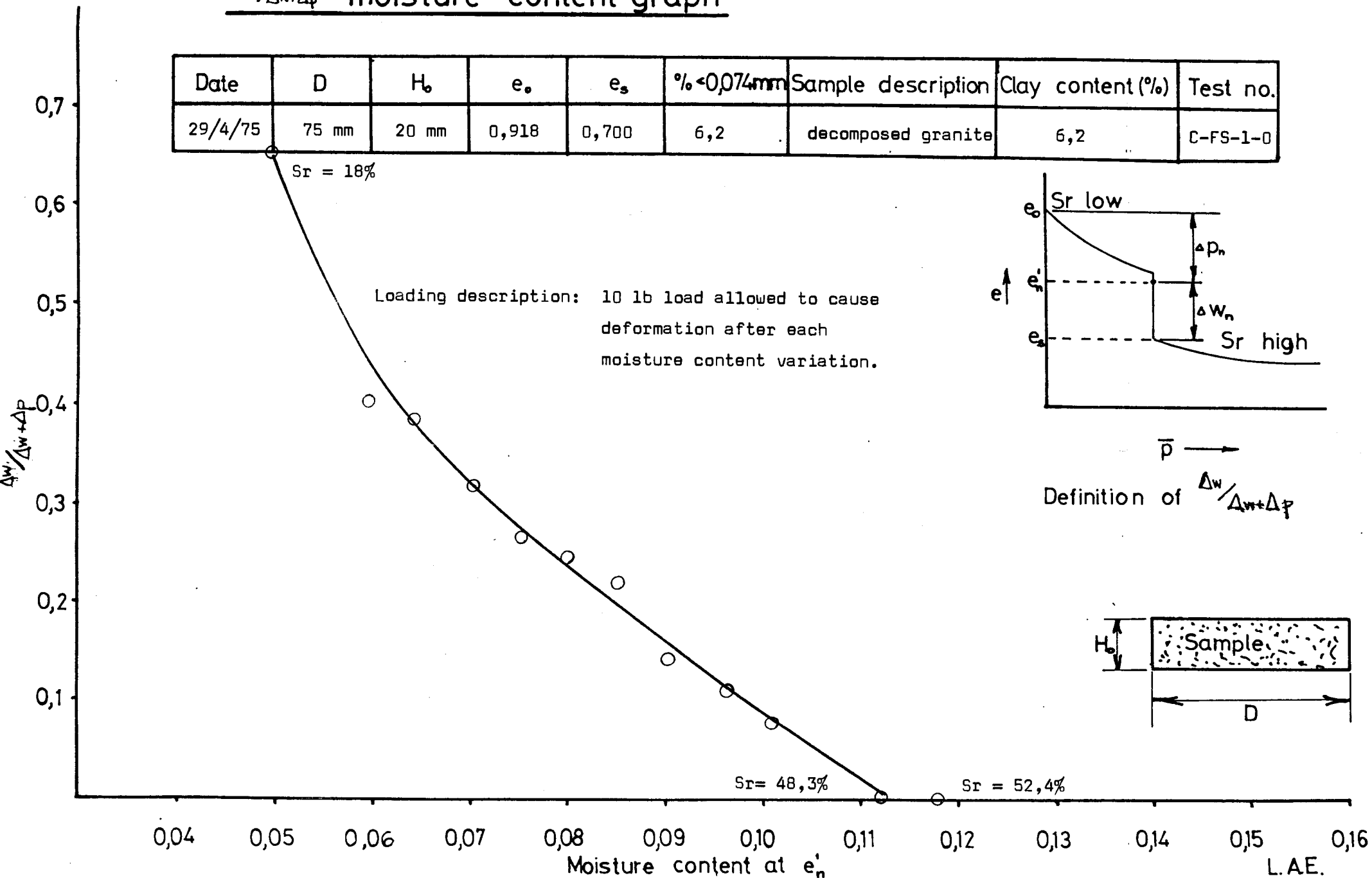


Void ratio—moisture content graph

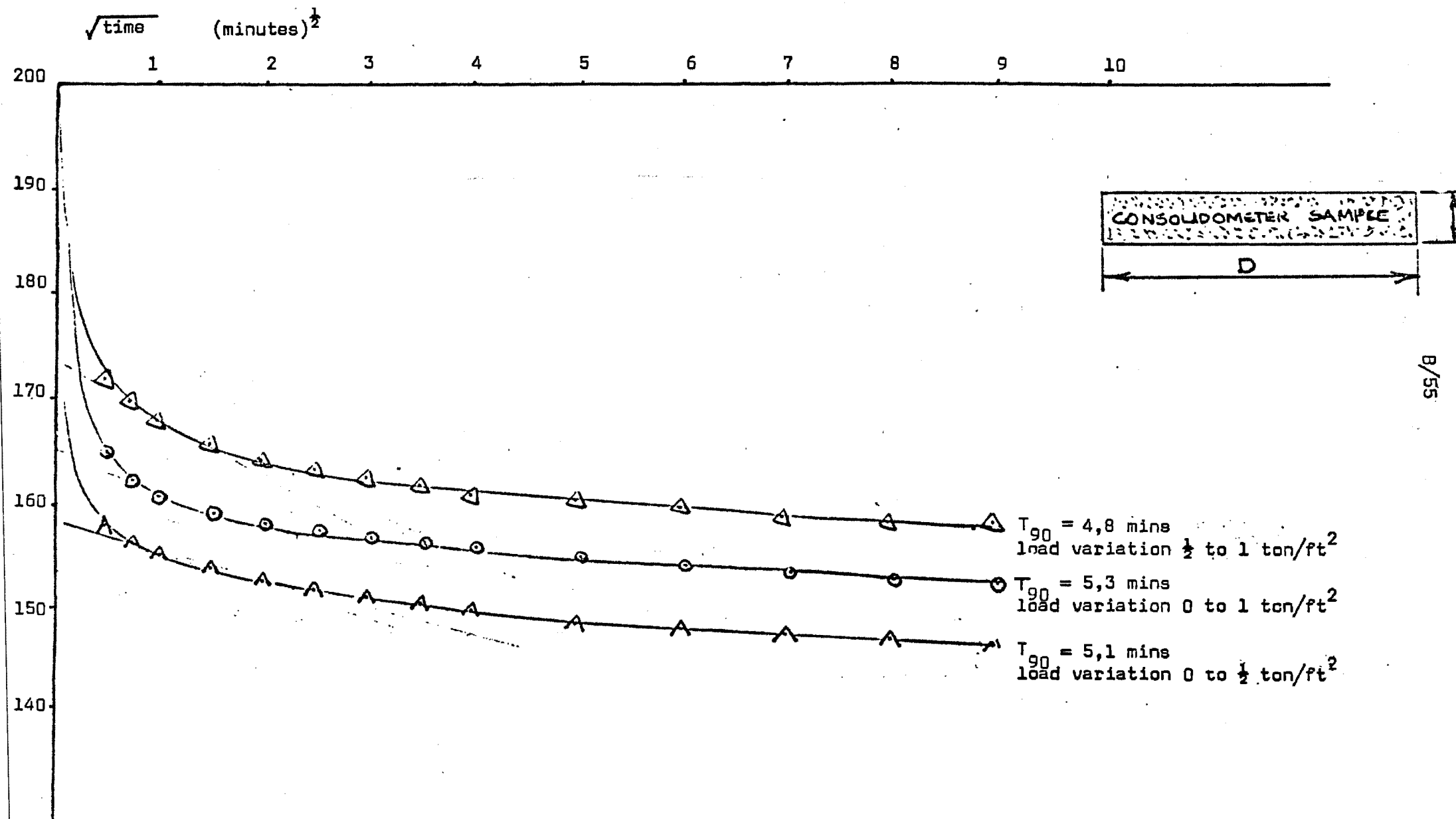


$\frac{\Delta w}{\Delta w + \Delta p}$ - moisture content graph

Date	D	H ₀	e ₀	e _s	% < 0,075 mm	Sample description	Clay content (%)	Test no.
29/4/75	75 mm	20 mm	0,918	0,700	6,2	decomposed granite	6,2	C-FS-1-0



DEFLECTION - TIME CURVES FOR SAMPLE EX FEATHERS



CONSOLIDOMETER TEST

SAMPLE DESCRIPTION Decomposed granitic residual soil - Undisturbed sample taken
from "Feathers"

SPECIFIC GRAVITY 2,68

TEST NO. C-FS-2 TESTED BY _____

DATE 30-4-75 CONSOLIDOMETER NO. A

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (INITIAL) 873,4 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (INITIAL) 651,2 g

MASS SOIL + RING (INITIAL) 222,2 g

MASS RING 94,4 g

MASS SOIL (INITIAL) 127,8 g

DRY MASS SOIL 120,8 g

MASS WATER INITIAL 7,0 g

FIELD MOISTURE CONTENT % 5,8%

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (FINAL) _____

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (FINAL) _____

MASS SOIL + RING (FINAL) _____

MASS RING _____

MASS SOIL (FINAL) _____

DRY MASS SOIL _____

MASS WATER (FINAL) _____

FINAL MOISTURE CONTENT _____

REMARKS: No moisture content variation.

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:3000	Wednesday	Field Wc	Load on arm	2000,0
0,25	9:3025	30-4-75		varied from	1921,0
0,50	9:3050			0 to 5lbs	1915,0
1,00	9:3100				1912,5
2,25	9:3225				1910,5
4,00	9:3400				1908,0
6,25	9:3625				1907,0
9,00	9:3900				1905,0
12,25	9:4225				1904,0
16,00	9:4600				1902,0
25,00	9:5500				1901,0
36,00	10:0600				1900,0
49,00	10:1900				1899,0
64,00	10:3400				1898,0
81,00	10:5100				1897,0
0,00	11:0000	Wednesday	Field Wc	Load on arm	1897,0
0,25	11:0025	30-4-75		varied from	1836,0
0,50	11:0050			5 to 10lbs	1832,0
1,00	11:0100				1829,0
2,25	11:0225				1825,0
4,00	11:0400				1822,0
6,25	11:0625				1820,0
9,00	11:0900				1819,0
12,25	11:1225				1818,0
16,00	11:1600				1817,0
25,00	11:2500				1816,0
36,00	11:3600				1814,0
49,00	11:4900				1812,0
64,00	12:0400				1811,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
81,00	12:2100				1810,0
0,00	12:2500	Wednesday	Field Wc	Load on arm	1810,0
0,25	12:2525	30-4-75		varied from	1718,0
0,50	12:2550			10 to 20lbs	1714,0
1,00	12:2600				1711,0
2,25	12:2725				1707,5
4,00	12:2900				1703,0
6,25	12:3125				1701,0
9,00	12:3400				1700,0
12,25	12:3725				1699,0
16,00	12:4100				1697,0
25,00	12:5000				1696,0
36,00	1:0100				1694,0
49,00	1:1400				1693,0
64,00	1:2900				1692,0
81,00	1:4600				1691,0
0,00	2:4500	Wednesday	Field Wc	Load on arm	1691,0
0,25	2:4525	30-4-75		varied from	1710,5
0,50	2:4550			20 to 2½lbs	1710,5
1,00	2:4600				1711,0
2,25	2:4725				1711,5
4,00	2:4900				1712,0
6,25	2:5125				1712,0
9,00	2:5400				1712,0
12,25	2:5725				1712,0
16,00	3:0100				1712,0
25,00	3:1000				1712,0
36,00	3:2100				1712,0

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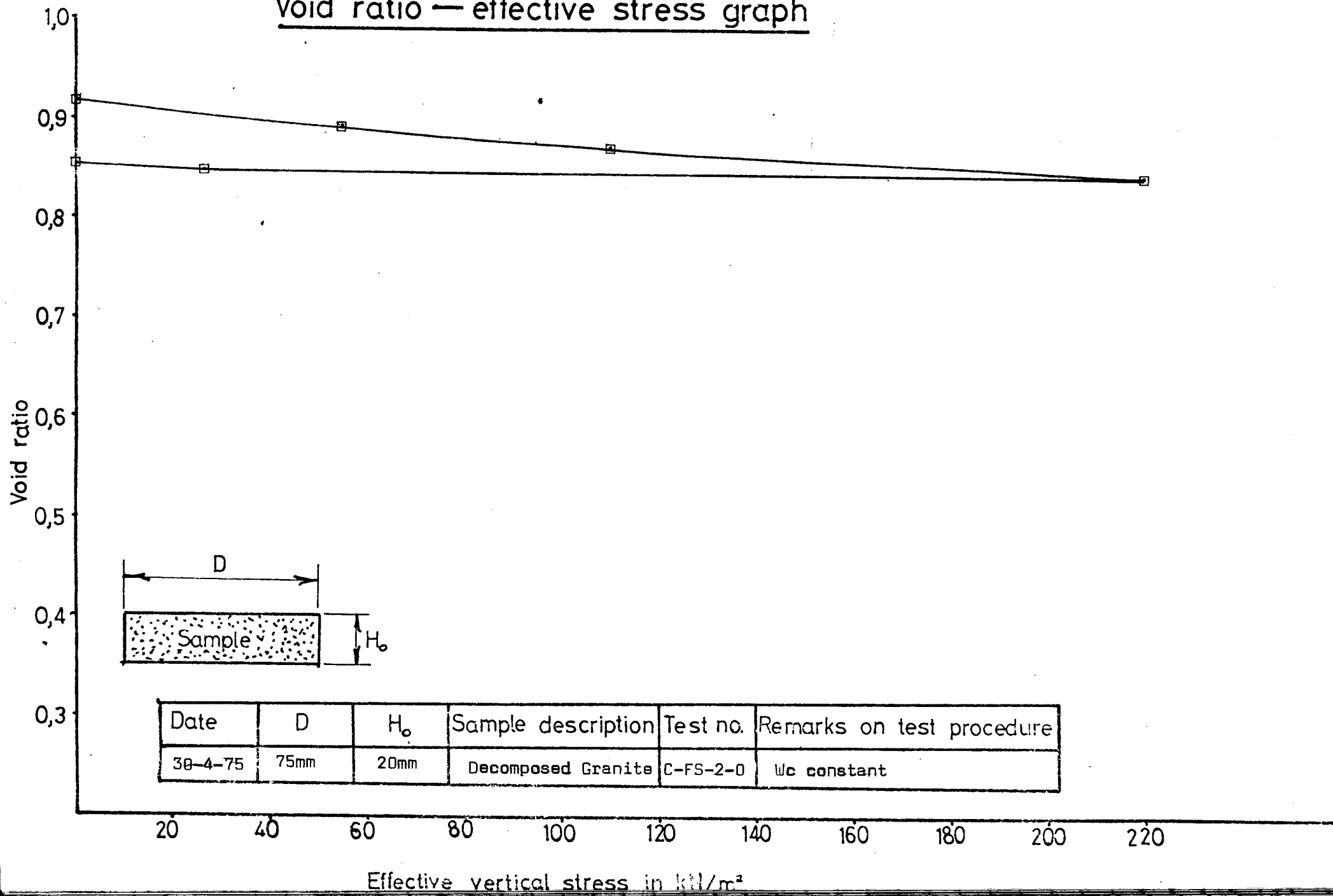
TEST NUMBER=C-F5-2-C
 INITIAL VOLUME= 58369.749
 VOLUME OF SOLIDS= 45022.089
 INITIAL VOID RATIO= .918
 INITIAL MOISTURE CONTENT= .058

ALL THE VOLUMES OUTPUT ARE IN MILLIMETERS CUBED
 THE VERTICAL STRESS IS IN KILONEWTONS PER SQUARE METER
 THE DEFLECTION READINGS ARE IN TEN THOUSANDTHS OF AN INCH

DEFLECTION READINGS	MOISTURE CONTENT	STRESS VERTICAL	VOID RATIO	DELTA W	DEGREE SATURATION
1998.00	.058	55.37	.893	.000	.175
1910.00	.058	110.74	.871	.000	.179
1691.00	.058	221.47	.842	.000	.185
1712.00	.058	27.68	.847	.000	.184
1729.00	.058	.00	.852	.000	.183

B/68

Void ratio — effective stress graph



SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample
taken from "Feathers"

SPECIFIC GRAVITY 2,68

TEST NO. C-FS-1

TESTED BY

DATE 9-7-75

TRIAXIAL CELL

MASS SOIL INITIAL

MASS DRY SOIL

MASS WATER INITIAL

WATER CONTENT

MASS SOIL FINAL 166,4 g

MASS DRY SOIL 136,6 g

MASS WATER FINAL 29,8 g

FINAL MOISTURE CONTENT 22%

MASS OF CONTAINER 99,0 g

REMARKS:

Sample height = 78mm

Sample diameter = 37mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	3	220,0
35	21	3	223,5
36	22	3½	228,5
40	24	3½	330,5
41	25	4	335,5
42	25	4	335,5
44	26	4	338,5
47	28	4	344,5
51	31	4	402,5
52	31	4	402,5
54	32	4	406,5
60	36	4½	426,0
61	37	4½	430,5
64	38	4½	434,5
65	39	5	437,5
67	40	5	443,5
69	41	5	455,0
71	43	5½	467,0
73	44	5½	479,5
74	44	6	485,5
76	46	6	497,0
77	46	6½	503,0
81	49	6½	523,0
83	50	7	531,0
85	51	7	539,0
87	52	7½	547,0
88	53	8	551,0
91	55	8	563,0
94	56	8½	576,0
103	62	8½	612,5
104	62	8½	615,5
106	64	9	621,0
109	65	9½	630,0
118	71	9½	651,0
121	73	10	657,0
123	74	10	665,0
134	80	10	702,0
137	82	10	705,5

SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample taken
from "Feathers"

SPECIFIC GRAVITY 2,68

TEST NO. T-FS-3

TESTED BY _____

DATE 11-7-77

TRIAXIAL CELL _____

MASS SOIL INITIAL 124,6 g

MASS DRY SOIL 118,4 g

MASS WATER INITIAL 6,2 g

FIELD MOISTURE CONTENT 5,2%

MASS SOIL FINAL _____

MASS DRY SOIL _____

MASS WATER FINAL _____

FINAL MOISTURE CONTENT _____

MASS OF CONTAINER _____

REMARKS:

Initial height of sample = 76mm

Initial diameter of sample = 39mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	2½	0,135
35	21	2½	0,145
36	22	3	0,150
40	24	3	0,170
41	25	3	0,190
42	25	3½	0,190
44	26	3½	0,215
47	28	3½	0,235
51	31	4	0,295
52	31	4	0,295
54	32	4½	0,310
60	36	4½	0,325
61	37	5	0,335
64	38	5	0,340
65	39	5	0,345
67	40	5	0,355
69	41	5½	0,360
71	43	5½	0,365
73	44	5½	0,370
74	44	5½	0,370
76	46	6	0,380
77	46	6	0,380
81	49	6	0,390
83	50	6	0,395
85	51	6	0,405
97	52	6	0,415
88	53	6½	0,420
91	55	6½	0,435
94	56	6½	0,440
103	62	7	0,470
104	62	7	0,470
106	64	7	0,475
109	65	7	0,480
118	71	7½	1,015
121	73	7½	1,020
123	74	7½	1,025
134	80	8	1,070
137	82	8½	1,075

B/66

TRIAxIAL

SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample
taken from "Feathers"

SPECIFIC GRAVITY 2.68

TEST NO. T-FS-4

TESTED BY _____

DATE 12-7-77

TRIAxIAL CELL _____

MASS SOIL INITIAL _____

MASS DRY SOIL _____

MASS WATER INITIAL _____

FIELD MOISTURE CONTENT _____

MASS SOIL FINAL 158,5 g

MASS DRY SOIL 133,7 g

MASS WATER FINAL 24,8 g

FINAL MOISTURE CONTENT 18,5%

MASS OF CONTAINER 94,5 g

REMARKS:

Initial height of sample = 81mm

Initial diameter of sample = 39mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	3	1,225
35	21	3½	1,250
36	22	3½	1,275
40	24	3½	1,310
41	25	3½	1,335
42	25	3½	1,335
44	26	4	1,360
47	28	4	1,405
51	31	4½	2,090
52	31	4½	2,090
54	32	4½	2,140
60	36	5	2,240
61	37	5	2,270
64	38	5	2,300
65	39	5½	2,330
67	40	5½	2,360
69	41	5½	2,400
71	43	6	3,020
73	44	6	3,060
74	44	6	3,060
76	46	6	3,130
77	46	6	3,130
81	49	6½	3,270
83	50	6½	3,295
85	51	6½	3,330
87	52	6½	3,360
88	53	7	3,390
91	55	7	3,445
94	56	7	3,480
103	62	7½	4,180
104	62	7½	4,190
106	64	7½	4,180
109	65	7½	4,240
118	71	8	5,020
121	73	8	5,095
123	74	8½	5,130
134	80	9	5,310
137	82	9	5,370

B/68

TRIAXIAL TEST

SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample
taken from "Feathers"

SPECIFIC GRAVITY 2.68

TEST NO. T-FS-5

TESTED BY _____

DATE 13-7-75

TRIAXIAL CELL _____

MASS SOIL INITIAL _____

MASS DRY SOIL _____

MASS WATER INITIAL _____

FIELD MOISTURE CONTENT _____

MASS SOIL FINAL 231.5 g

MASS DRY SOIL 219.9 g

MASS WATER FINAL 11.6 g

FINAL MOISTURE CONTENT 8.2%

MASS OF CONTAINER 78.6 g

REMARKS

Initial height of sample = 81mm

Initial diameter of sample = 39mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	2½	0,185
35	21	2½	0,200
36	22	3	0,215
40	24	3	0,235
41	25	3	0,245
42	25	3	0,245
44	26	3½	0,255
47	28	3½	0,255
51	31	3½	0,275
52	31	3½	0,275
54	32	4	0,290
60	36	4	0,330
61	37	4	0,340
64	38	4½	0,350
65	39	4½	0,360
67	40	4½	0,365
69	41	5	0,370
71	43	5	0,375
73	44	5	0,380
74	44	5	0,380
76	46	5½	0,395
77	46	5½	0,395
81	49	5½	0,415
83	50	6	0,420
85	51	6	0,420
87	52	6	0,425
88	53	6	0,430
91	55	6½	0,440
94	56	6½	0,445
103	62	7	0,485
104	62	7	0,485
106	64	7½	0,495
109	65	7½	1,000
118	71	8	1,040
121	73	8	1,060
123	74	8	1,065
134	80	8½	1,090
137	82	8½	1,100

8/70

TRIAXIAL TEST

SAMPLE DESCRIPTION Decomposed granitic residual soil - undisturbed sample
taken from "Feathers"

SPECIFIC GRAVITY 2.68

TEST NO. T-F8-6

TESTED BY _____

DATE 13-7-75

TRIAXIAL CELL _____

MASS SOIL INITIAL _____

MASS DRY SOIL _____

MASS WATER INITIAL _____

FIELD MOISTURE CONTENT _____

MASS SOIL FINAL 125.7 g

MASS DRY SOIL 111.0 g

MASS WATER FINAL 14.7 g

FINAL MOISTURE CONTENT 13.2%

MASS OF CONTAINER 94.5 g

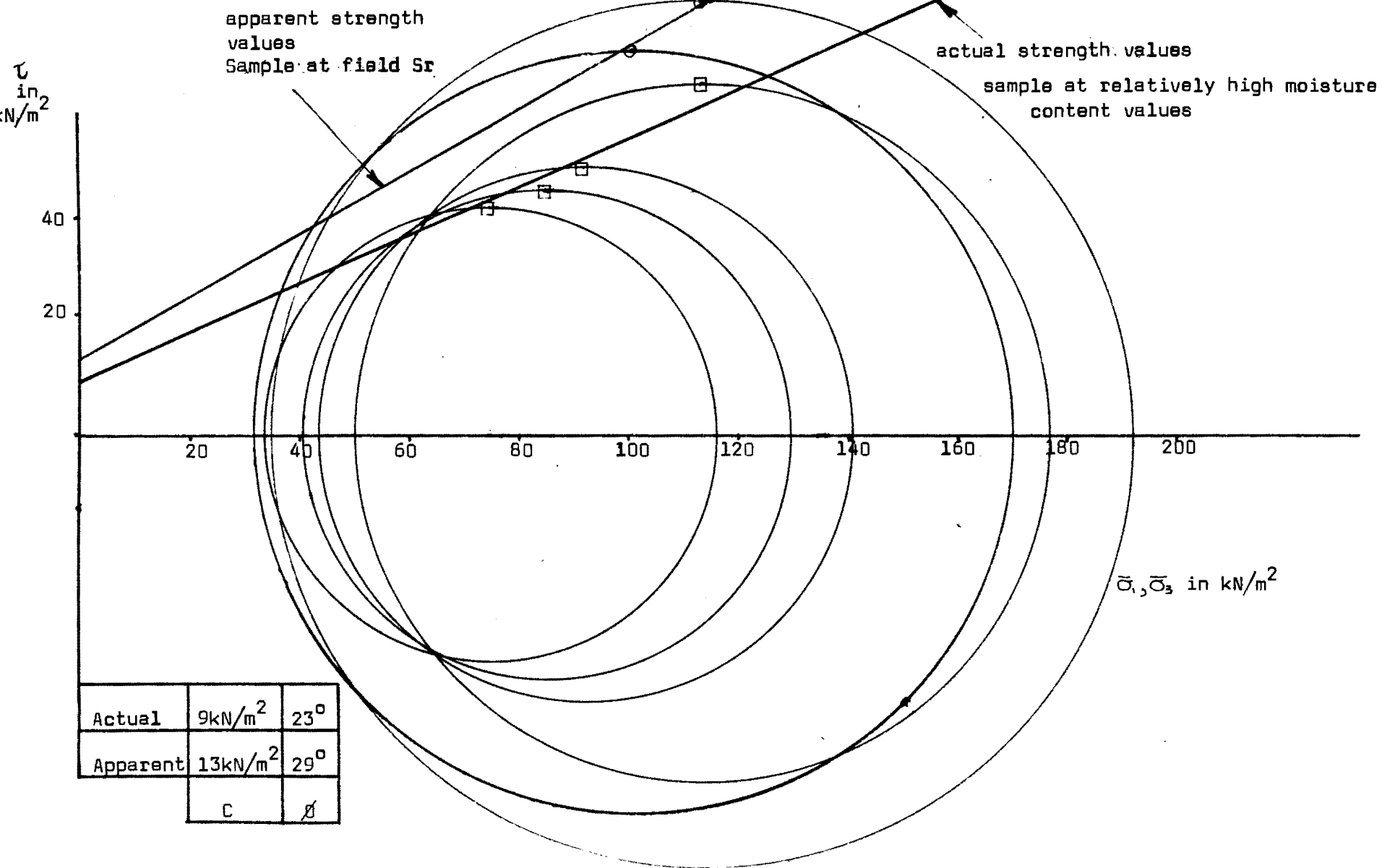
REMARKS:

Initial height of sample = 71mm

Initial diameter of sample = 39mm

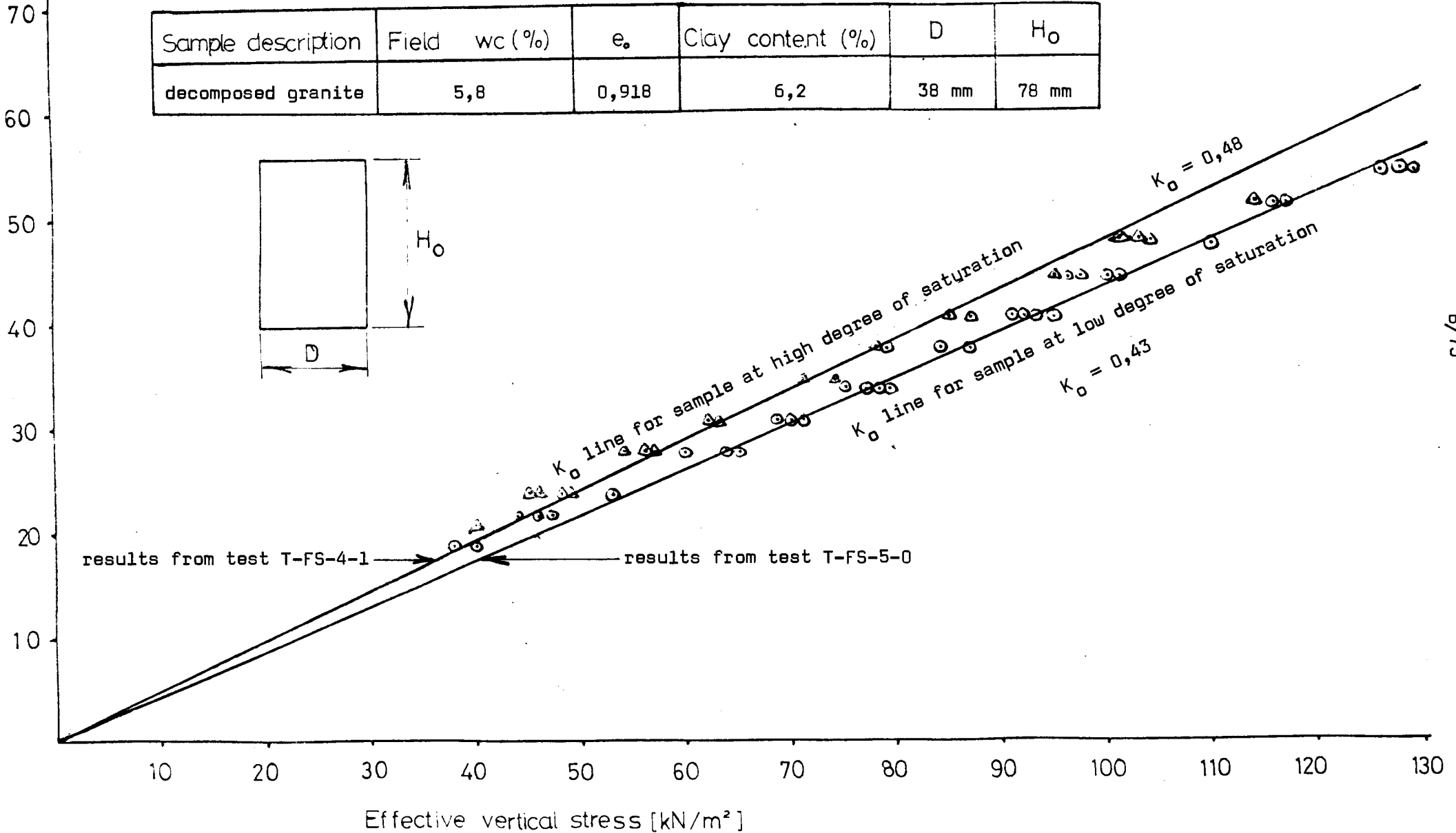
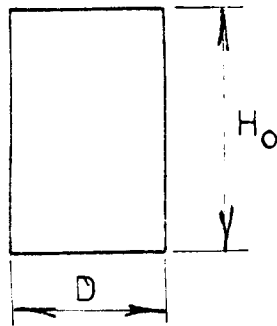
VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	3	0,325
35	21	3	0,370
36	22	3	0,425
40	24	3½	0,460
41	25	3½	0,480
42	25	3½	0,480
44	26	4	1,000
47	28	4	1,045
51	31	4½	1,115
52	31	4½	1,115
54	32	4½	1,140
60	36	5	1,225
61	37	5	1,250
64	38	5	1,280
65	39	5½	1,310
67	40	5½	1,335
69	41	5½	1,355
71	43	6	1,390
73	44	6	1,410
74	44	6	1,410
76	46	6½	1,435
77	46	6½	1,435
81	49	6½	1,495
83	50	6½	2,035
85	51	6½	2,055
87	52	7	2,080
88	53	7	2,105
91	55	7	2,125
94	56	7	2,145
103	62	7½	2,225
104	62	7½	2,225
106	64	7½	2,290
109	65	7½	2,320
118	71	8	2,415
121	73	8	2,440
123	74	8	2,460
134	80	8½	3,060
137	82	8½	3,100

TRIAXIAL STRENGTH TESTS - SAMPLE EX FEATHERS



K_0 Lines - Triaxial K_0 tests

Sample description	Field	wc (%)	e_0	Clay content (%)	D	H_0
decomposed granite		5,8	0,918	6,2	38 mm	78 mm



HYDROMETER ANALYSTS

SPECIFIC GRAVITY 2.68

TEST NO. H - SH - 1

DATE 8-8-75

TESTED BY

HYDROMETER NO. 9843 A.S.T.M. 151 H

10 ml. Sodium silicate solution

[illegible]

REMARKS:

Sample soaked for 24 hrs.

For the 2 and 5 minute readings Z_r uncorrected is used.

HYDROMETER ANALYSTS

SOIL SAMPLE DESCRIPTION **Brown Fine Grained Collapsing Sand - Undisturbed sample**
from **Sisahn**

SPEED IN GRAVITY 2,68

WEIGHT SOL SAMPLE

TEST NO. H-SH-2

Mass container + dry soil (g) 140,0

DATE 11/8/75

Mass container (g)	90,0
--------------------	------

TESTED BY

Mass dry soil (g)	50,0
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HYDROMETER NO. 9843 A.S.T.M. 151 H.

DISPERSING AGENTS 10 ml. Sodium oxalate solution

10 ml. Sodium silicate solution

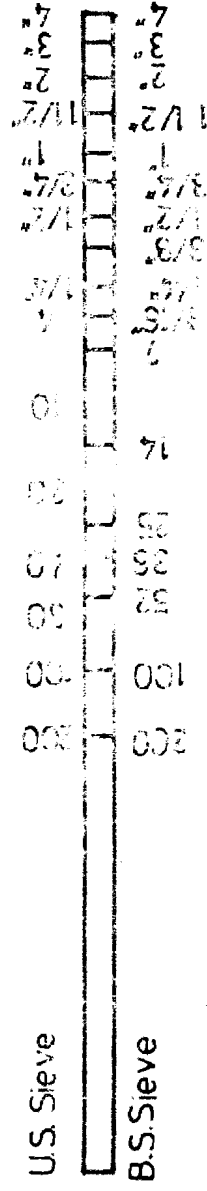
[illegible]

REMARKS:

Sample soaked for 24 hrs.

For the 2 and 5 minute readings Z_r uncorrected is used.

Sample description	collapsing sand	B/77
Sample source	Siahen	
Test number	H-SH-1, H-SH-2, SA-SH-1	
Dispersing agent		



LA
E

B/78

CONSOLIDOMETER TEST

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample from
Sishen.

SPECIFIC GRAVITY 2,68

TEST NO. C - SH - 1

TESTED BY _____

DATE 5-8-75

CONSOLIDOMETER NO. A.

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (INITIAL) 892,4 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (INITIAL) 667,2 g

MASS SOIL + RING (INITIAL) 225,2 g

MASS RING 85,7 g

MASS SOIL (INITIAL) 139,5 g

DRY MASS SOIL 136,4 g

MASS WATER INITIAL 3,1 g

FIELD MOISTURE CONTENT % 2,3%

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (FINAL) _____

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (FINAL) _____

MASS SOIL + RING (FINAL) _____

MASS RING _____

MASS SOIL (FINAL) _____

DRY MASS SOIL _____

MASS WATER (FINAL) _____

FINAL MOISTURE CONTENT _____

REMARKS: No moisture content variation.

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	11:5000	Tuesday	Field Wc	Load on arm	2000,00
0,25	11:5025	5/8/75	+	varied from	1903,0
0,50	11:5050			0 to 2½lbs	1900,0
1,00	11:5100				1896,5
2,25	11:5225				1893,5
4,00	11:5400				1888,0
6,25	11:5625				1883,0
9,00	11:5900				1881,0
12,25	12:0225				1879,0
16,00	12:0600				1878,0
25,00	12:1500				1876,0
36,00	12:2600				1872,0
49,00	12:3900				1870,0
64,00	12:5400				1869,0
0,00	2:0500	Tuesday	Field Wc	Load on arm	1869,0
0,25	2:0525	5/8/75	+	varied from	1816,0
0,50	2:0550			2½lbs to 5lbs	1812,0
1,00	2:0600				1808,5
2,25	2:0725				1804,5
4,00	2:0900				1801,0
6,25	2:1125				1798,0
9,00	2:1400				1796,0
12,25	2:1725				1794,5
16,00	2:2100				1793,0
25,00	2:3000				1791,0
36,00	2:4100				1789,5
49,00	2:5400				1788,0
64,00	3:0900				1786,5
81,00	3:2600				1785,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	3:3000	Tuesday	Field Wc	Load on arm	1705,5
0,25	3:3025	5/8/75		varied from	1709,0
0,50	3:3050			5lbs to 10lbs	1703,0
1,00	3:3100				1697,0
2,25	3:3225				1693,0
4,00	3:3400				1689,0
6,25	3:3625				1686,0
9,00	3:3900				1683,5
12,25	3:4225				1681,5
16,00	3:4600				1680,0
25,00	3:5500				1678,5
36,00	4:0600				1676,0
49,00	4:1900				1674,0
64,00	4:3400				1672,5
81,00	4:5100				1671,0
100,00	5:1000				1670,0
0,00	9:3000	Wednesday	Field Wc	Load on arm	1670,0
0,25	9:3025	6/8/75		varied from	1610,0
0,50	9:3050			10 to 20lbs	1605,0
1,00	9:3100				1600,0
2,25	9:3225				1595,5
4,00	9:3400				1593,0
6,25	9:3625				1590,5
9,00	9:3900				1588,5
12,25	9:4225				1586,5
16,00	9:4600				1585,0
25,00	9:5500				1583,5
36,00	10:0600				1582,0
49,00	10:1900				1580,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
64,00	10:3400	Wednesday	Field Wc	Load on arm	1579,5
81,00	10:5100	6-8-75		Varied from	1578,0
100,00	11:1000			10 to 20 lbs.	1577,0
0	11:25	Wednesday	Field Wc	Load on arm	1577,0
0,25	11:2525	6-8-75		Varied from	1592,0
0,50	11:2550			20 to 5 lbs.	1593,0
1,00	11:2600				1593,0
2,25	11:2725				1593,5
4,00	11:2900				1593,5
6,25	11:3125				1594,0
9,00	11:3400				1594,0
12,25	11:3700				1594,5
16,00	11:4100				1594,5
0	12:0000	Wednesday	Field Wc	Load on arm	1594,5
0,25	12:0025	6-8-75		Varied from	1600,0
0,50	12:0050			5 to 2½ lbs.	1600,5
1,00	12:0100				1601,0
2,25	12:0225				1601,0
4,00	12:0400				1601,5
6,25	12:0625				1601,5
9,00	12:0900				1602,0
12,25	12:1225				1602,5
16,00	12:1600				1602,5
0	12:2000	Wednesday	Field Wc	Load on arm	1602,5
0,25	12:2025	6-8-75		Varied from	1620,0
0,50	12:2050			2½ to 0 lbs.	1621,0
1,00	12:2100				1621,5

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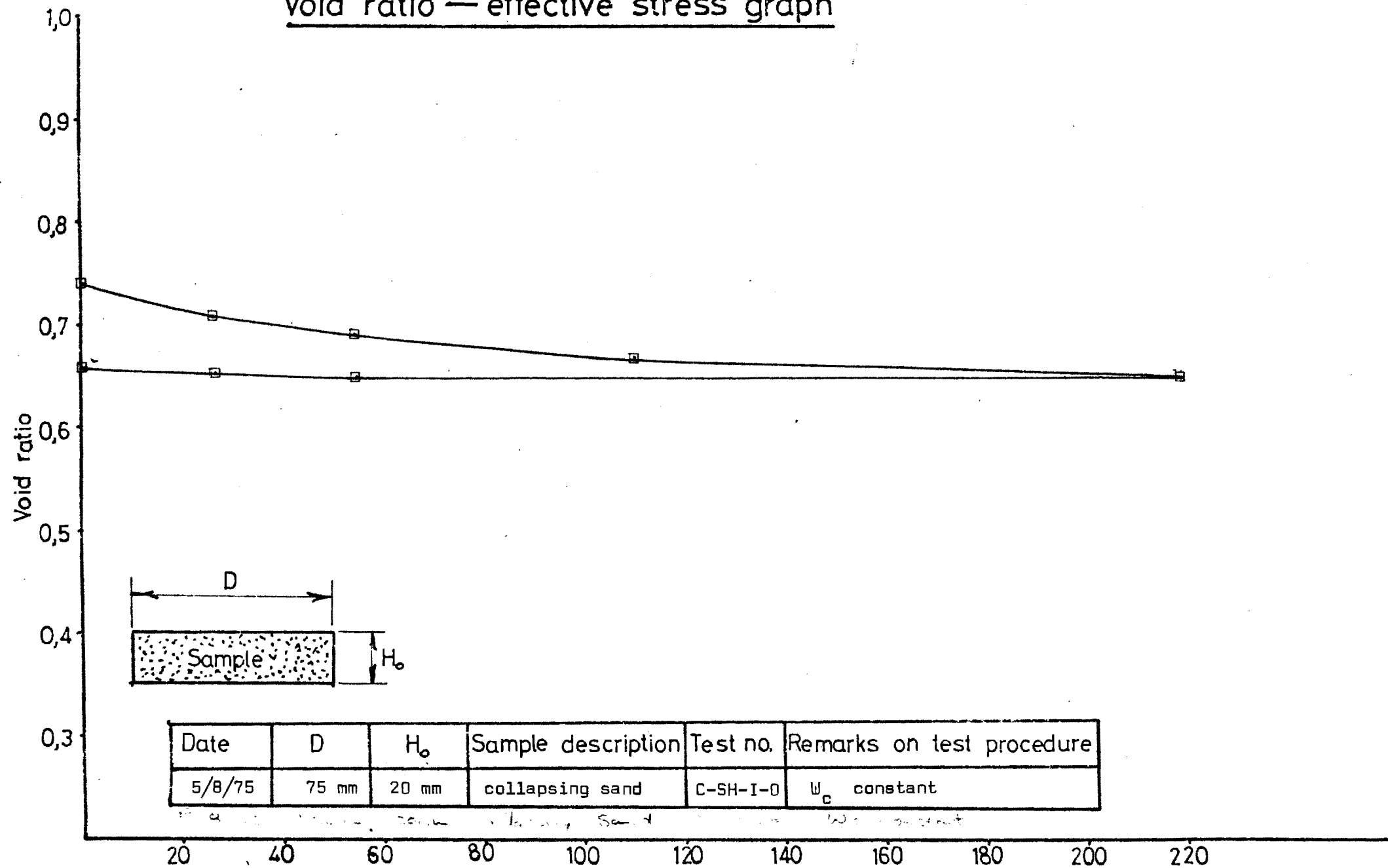
TEST NUMBER=C-54-1-0
 INITIAL VOLUME= 30168.749
 VOLUME OF SOLIDS= 50875.521
 INITIAL VOID RATIO= .736
 INITIAL MOISTURE CONTENT= .023

ALL THE VOLUMES OUTPUT ARE IN MILLIMETERS CUBED
 THE VERTICAL STRESS IS IN KILONEWTONS PER SQUARE METER
 THE DEFLECTION READINGS ARE IN TEN THOUSANDTHS OF AN INCH

DEFLECTION READINGS	MOISTURE CONTENT	STRESS VERTICAL	VOID RATIO	DELTA #	DEGREE SATURATION
1569.00	.023	27.69	.707	.000	.086
1745.50	.023	55.37	.689	.000	.088
1670.00	.023	110.74	.664	.000	.092
1577.00	.023	221.47	.643	.000	.095
1594.50	.023	55.37	.647	.000	.094
1592.50	.023	27.69	.649	.000	.094
1624.50	.023	.00	.653	.000	.093

B/83

Void ratio — effective stress graph



B/85

CONSOLIDOMETER TEST

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample
from Sishen

SPECIFIC GRAVITY 2,68

TEST NO. C-SH-2 TESTED BY _____

DATE 4/8/75 CONSOLIDOMETER NO. _____

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (INITIAL) 883,7 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (INITIAL) 653,8 g

MASS SOIL + RING (INITIAL) 229,9g

MASS RING 97,4 g

MASS SOIL (INITIAL) 132,5 g

DRY MASS SOIL 131,4 g

MASS WATER INITIAL 1,1 g

FIELD MOISTURE CONTENT % 1,0%

MASS FILTER PAPERS + POROUS PLATES + PLASTIC + SOIL + RING (FINAL) 892,3 g

MASS FILTER PAPERS + POROUS PLATES + PLASTIC (FINAL) 656,2 g

MASS SOIL + RING (FINAL) 236,1 g

MASS RING 97,4g

MASS SOIL (FINAL) 138,7 g

DRY MASS SOIL 131,4 g

MASS WATER (FINAL) 7,3 g

FINAL MOISTURE CONTENT 5,6%

REMARKS:

LEONARDO A. ERRERA

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	10:4000	Tuesday	Field Wc	Load on arm	2000,0
0,25	10:4025	19-8-75		Varied from	1928,0
0,50	10:4050			0 to 2½ lb.	1925,0
1,00	10:4100				1922,0
2,25	10:4225				1918,0
4,00	10:4400				1916,0
6,25	10:4625				1914,0
9,00	10:4900				1912,0
12,25	10:5225				1911,0
16,00	10:5600				1910,5
25,00	11:050				1908,5
36,00	11:1600				1906,5
49,00	11:2900				1905,0
64,00	11:4400				1904,0
0,00	11:4500	Tuesday	Field Wc	Load on arm	1904,0
0,25	11:4525	19-8-75		Varied from	1874,0
0,50	11:4550			2½ to 5 lb.	1872,0
1,00	11:4600				1870,0
2,25	11:4725				1867,5
4,00	11:4900				1865,5
6,25	11:5125				1864,5
9,00	11:5400				1863,5
12,25	11:5725				1862,5
16,00	12:0100				1861,5
25,00	12:1000				1859,5
36,00	12:2100				1857,5
49,00	12:3400				1856,5
64,00	12:4900				1855,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	2:3000	Tuesday	Field Wc	Load on arm	1855,5
0,25	2:3025	19-8-75		Varied from	1800,0
0,50	2:3050			5 to 10 lb.	1797,5
1,00	2:3100				1794,5
2,25	2:3225				1791,5
4,00	2:3400				1789,0
6,25	2:3625				1787,5
9,00	2:3900				1786,0
12,25	2:4225				1785,0
16,00	2:4600				1784,0
25,00	2:5500				1782,5
36,00	3:0600				1781,0
49,00	3:1900				1779,5
64,00	3:3400				1778,5
0,00	2:2000	Wednesday	Field Wc	10lb reapplied	1778,5
0,25	2:2025	20-8-75	+ 2 ml of water	after strain	1585,0
0,50	2:2050			being kept	1575,0
1,00	2:2100			constant	1562,0
2,25	2:2225				1555,0
4,00	2:2400				1550,5
6,25	2:2625				1547,5
9,00	2:2900				1545,0
12,25	2:3225				1543,0
16,00	2:3600				1541,0
25,00	2:4500				1538,5
36,00	2:5600				1536,5
49,00	2:0900				1534,5
64,00	2:2400				1533,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	2:2000	Friday	Field Wc	101b reapplied	1533,0
0,25	2:2025	22-8-75	+ 3ml of water	after strain	1499,0
0,50	2:2050			being kept	1497,0
1,00	2:2100			constant	1494,5
2,25	2:2225				1491,0
4,00	2:2400				1487,0
6,25	2:2625				1485,5
9,00	2:2900				1484,5
12,25	2:3225				1483,5
16,00	2:3600				1482,5
25,00	2:4500				1482,0
36,00	2:5600				1481,0
49,00	3:0900				1480,0
64,00	3:2400				1479,0
0,00	9:5800	Saturday	Field Wc	101b reapplied	1479,0
0,25	9:5825	23-8-75	+ 4ml of water	after strain	1473,5
0,50	9:5850			being kept	1473,0
1,00	9:5900			constant	1472,0
2,25	10:0025				1471,0
4,00	10:0200				1469,5
6,25	10:0425				1467,5
9,00	10:0700				1466,0
12,25	10:1025				1464,5
16,00	10:1400				1463,0
25,00	10:2300				1461,5
36,00	10:3400				1460,0
49,00	10:4700				1458,5
64,00	11:0200				1457,5

B/89

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	8:5000	Monday	Field Wc	101b reapplied	1457,5
0,25	8:5025	25-8-75	+ 5ml of water	after strain	1454,0
0,50	8:5050			being kept	1453,5
1,00	8:5100			constant	1453,5
2,25	8:5225				1453,0
4,00	8:5400				1453,0
6,25	8:5625				1452,0
9,00	8:5900				1452,0
12,25	9:0225				1452,0
16,00	9:0600				1452,0
25,00	9:1500				1451,5
36,00	9:2600				1451,0
49,00	9:3900				1451,0
64,00	9:5400				1450,5
0,00	10:2000	Tuesday	Field Wc	101b reapplied	1450,5
0,25	10:2025	26-8-75	+ 6ml of water	after strain	1450,0
0,50	10:2050			being kept	1449,5
1,00	10:2100			constant	1449,5
2,25	10:2225				1449,0
4,00	10:2400				1448,5
6,25	10:2625				1448,5
9,00	10:2900				1448,0
12,25	10:3225				1448,0
16,00	10:3600				1447,5
25,00	10:4500				1447,0
36,00	10:5600				1446,5
49,00	11:0900				1446,0
64,00	11:2400				1445,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	10:2000	Wednesday	Field Wc	101b reapplied	1445,5
0,25	10:2025	27-8-75	+ 7ml of water	after strain	1444,0
0,50	10:2050			being kept	1443,5
1,00	10:2100			constant	1443,5
2,25	10:2225				1443,0
4,00	10:2400				1443,0
6,25	10:2625				1443,0
9,00	10:2900				1442,5
12,25	10:3225				1442,5
16,00	10:3600				1442,5
25,00	10:4500				1442,0
36,00	10:5600				1441,5
49,00	11:0900				1441,0
64:00	11:2400				1441,0
0,00	11:3000	Thursday	Field Wc	Load on arm	1440,5
0,25	11:3025	28-8-75	+ 7ml of water	varied from	1434,0
0,50	11:3050			10 to 12½lb	1433,0
1,00	11:3100				1431,5
2,25	11:3225				1429,5
4,00	11:3400				1426,5
6,25	11:3625				1424,0
9,00	11:3900				1422,5
12,25	11:4225				1420,5
16,00	11:4600				1419,0
25,00	11:5500				1417,0
36,00	12:0600				1414,0
49,00	12:1900				1412,0
64,00	12:3400				1411,0

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
0,00	9:3000	Tuesday	Field Wc	Load on arm	1411,0
0,25	9:3025	2-9-75	+ 7ml of water	varied from	1400,0
0,50	9:3050			12½ to 15lb	1399,0
1,00	9:3100				1397,0
2,25	9:3225				1395,0
4,00	9:3400				1393,0
6,25	9:3625				1391,5
9,00	9:3900				1390,0
12,25	9:4225				1388,5
16,00	9:4600				1387,0
25,00	9:5500				1385,0
36,00	10:0600				1384,5
49,00	10:1900				1382,0
64,00	10:3400				1380,5
81,00	10:5100				1379,0
0,00	11:000	Tuesday	Field Wc	Load on arm	1379,0
0,25	11:0025	2-9-75	+ 7ml of water	varied from	1374,0
0,50	11:0050			15 to 17½lb	1373,0
1,00	11:0100				1372,0
2,25	11:0225				1369,0
4,00	11:0400				1366,0
6,25	11:0625				1364,0
9,00	11:0900				1362,5
12,25	11:1225				1361,0
16,00	11:1600				1359,5
25,00	11:2500				1357,5
36,00	11:3600				1355,5
49,00	11:4900				1353,5
64,00	12:0400				1351,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
81,00	12:2100	Tuesday	Field Wc	Load on arm	1350,0
100,00	12:4000	2-9-75	+ 7ml of water	varied from	1349,0
				15 to 17½lb	
0,00	11:2000	Friday	Field Wc	Load on arm	1349,0
0,25	11:2025	5-9-75	+ 7ml of water	varied from	1338,5
0,50	11:2050			17½ to 20lb	1337,5
1,00	11:2100				1336,0
2,25	11:2225				1334,5
4,00	11:2400				1333,5
6,25	11:2625				1332,0
9,00	11:2900				1331,0
12,25	11:3225				1330,0
16,00	11:3600				1328,0
25,00	11:4500				1326,0
36,00	11:5600				1325,0
49,00	12:0900				1324,0
64,00	12:2400				1323,0
81,00	12:4100				1322,0
100,00	1:0000				1321,0
121,00	1:2100				1320,0
144,00	1:4400				1319,0
169,00	2:0900				1318,0
0,00	2:3300	Friday	Field Wc	Load on arm	1318,0
0,25	2:3325	5-9-75	+ 7ml of water	varied from	1333,0
0,50	2:3350			20 to 51b	1334,0
1,00	2:3400				1334,0
2,25	2:3525				1334,5

TIME INTERVAL	TIME	DAY/DATE	MOISTURE CONTENT DESCRIPTION	LOADING DESCRIPTION	READINGS
4,00	2:3700	Friday	Field Wc	Load on arm	1335,0
6,25	2:3925	5-9-75	+ 7ml of water	varied from	1335,0
9,00	2:4200			20 to 51b	1335,0
12,25	2:4525				1335,0
0,00	2:5000	Friday	Field Wc	Load on arm	1335,5
0,25	2:5025	5-9-75	+ 7ml of water	varied from	1341,0
0,50	2:5050			5 to 2½lb	1342,0
1,00	2:5100				1342,0
2,25	2:5225				1342,5
4,00	2:5400				1343,0
6,25	2:5625				1343,0
9,00	2:5900				1343,5
12,25	3:0225				1343,5
16,00	3:0600				1344,0
25,00	3:1500				1344,0
0,00	3:2500	Friday	Field Wc	Load on arm	1344,0
0,25	3:2525	5-9-75	+ 7ml of water	varied from	1363,5
0,50	3:2550			2½ to 01b	1364,0
1,00	3:2600				1365,0
2,25	3:2725				1366,0
4,00	3:2900				1368,0
6,25	3:3125				1369,0
9,00	3:3400				1370,0
12,25	3:3725				1371,0
16,00	3:4100				1371,5
25,00	3:5000				1372,0

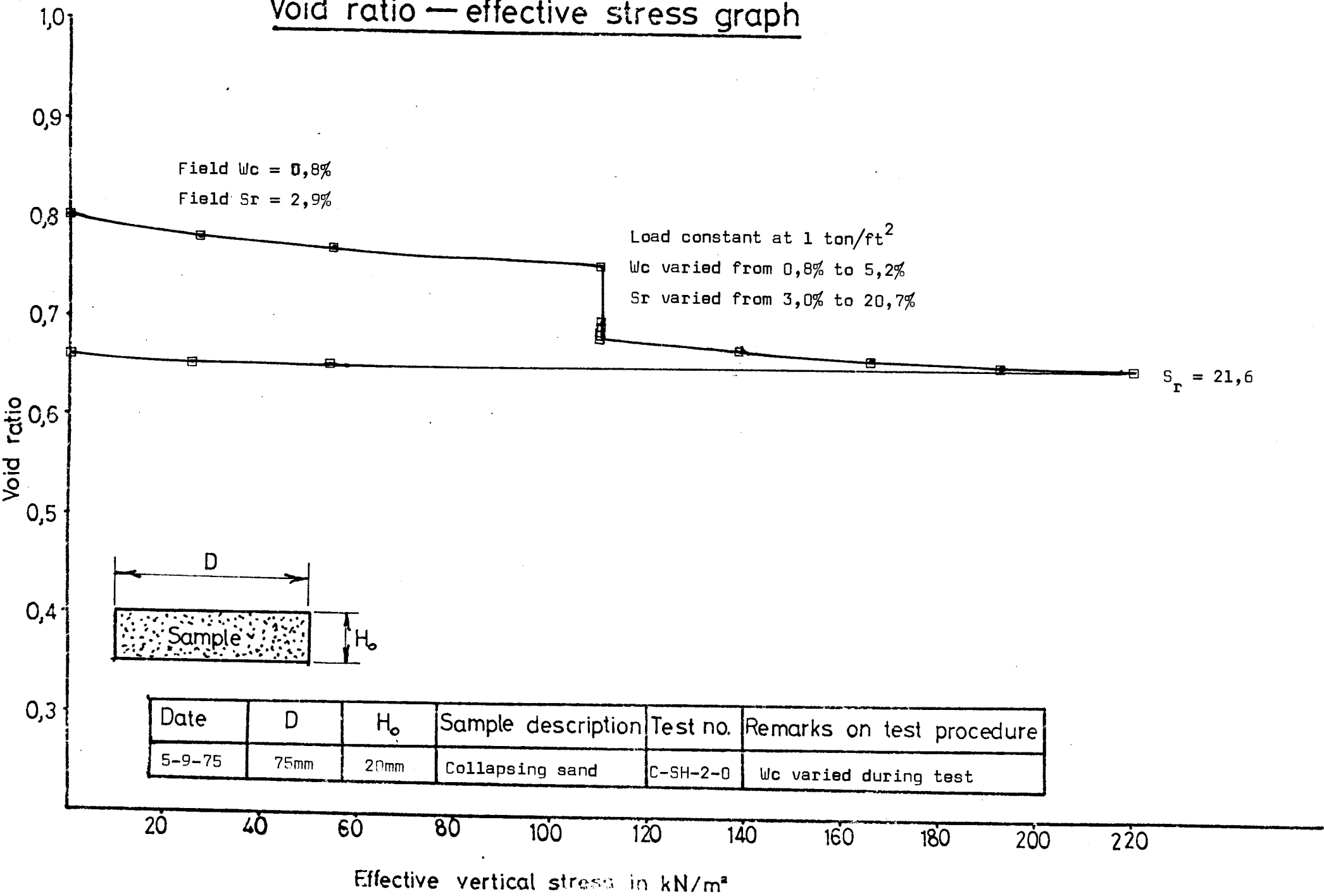
TEST NUMBER=C-5H-2-0
 INITIAL VOLUME= 88368.749
 VOLUME OF SOLIDS= 49029.950
 INITIAL VOID RATIO= .802
 INITIAL MOISTURE CONTENT= .008

ALL THE VOLUMES OUTPUT ARE IN MILLIMETERS CUBED
 THE VERTICAL STRESS IS IN KILONEWTONS PER SQUARE METER
 THE DEFLECTION READINGS ARE IN TEN THOUSANDTHS OF AN INCH

DEFLECTION READINGS	MOISTURE CONTENT	STRESS VERTICAL	VOID RATIO	DELTA W	DEGREE SATURATION
1904.00	.008	27.68	.780	.000	.029
1855.50	.008	55.37	.769	.000	.029
1778.50	.008	110.74	.752	.000	.030
1533.00	.021	110.74	.695	.165	.080
1479.00	.027	110.74	.603	.069	.106
1457.50	.033	110.74	.678	.030	.132
1450.50	.040	110.74	.677	.018	.157
1445.50	.016	110.74	.675	.009	.182
1440.50	.052	110.74	.674	.000	.207
1411.00	.052	138.42	.668	.000	.209
1379.00	.052	166.10	.660	.000	.211
1349.00	.052	193.79	.653	.000	.213
1318.00	.052	221.47	.646	.000	.216
1335.50	.052	55.37	.650	.000	.214
1344.00	.052	27.68	.652	.000	.214
1372.00	.052	.00	.659	.000	.212

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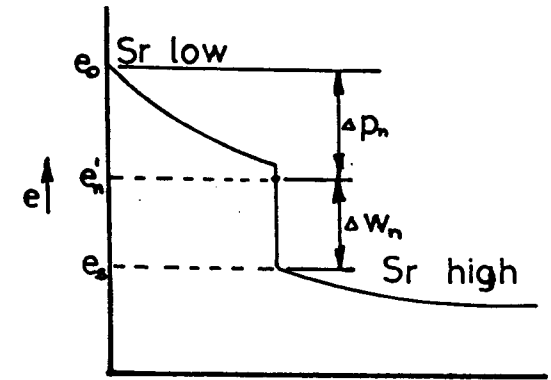
Void ratio — effective stress graph



$\frac{\Delta w}{\Delta w + \Delta p}$ —moisture content graph

Date	D	H ₀	e _s	e _s	% < 0,074 mm	Sample description	Clay content (%)	Test no.
5/9/75	75 mm	20 mm	0,802	0,674	10	collapsing sand	10	C-SH-2-0

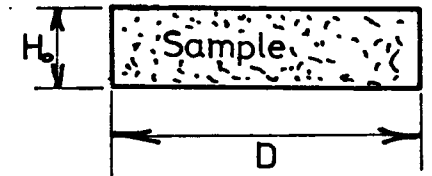
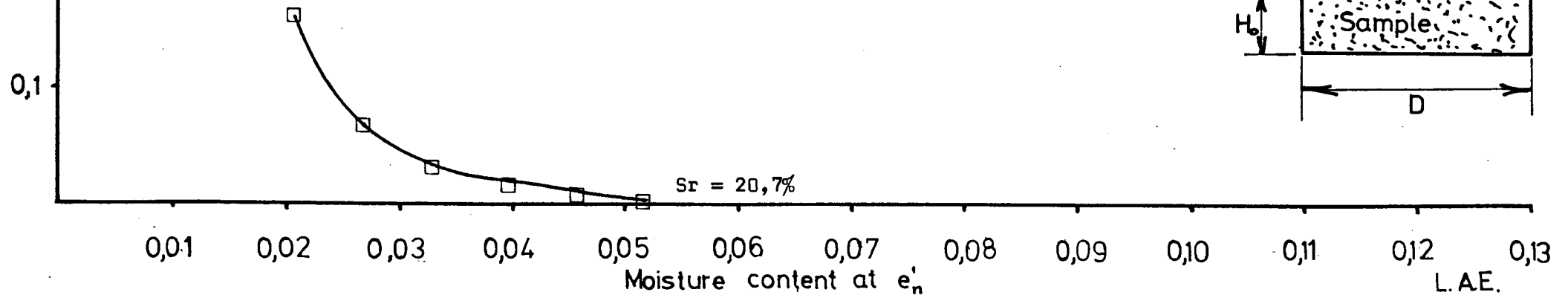
Loading description : 10 lb load allowed to cause deformation after each moisture content variation.



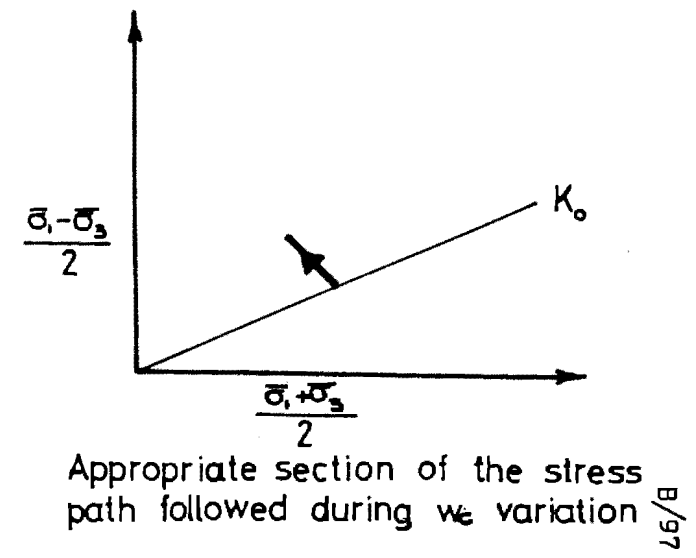
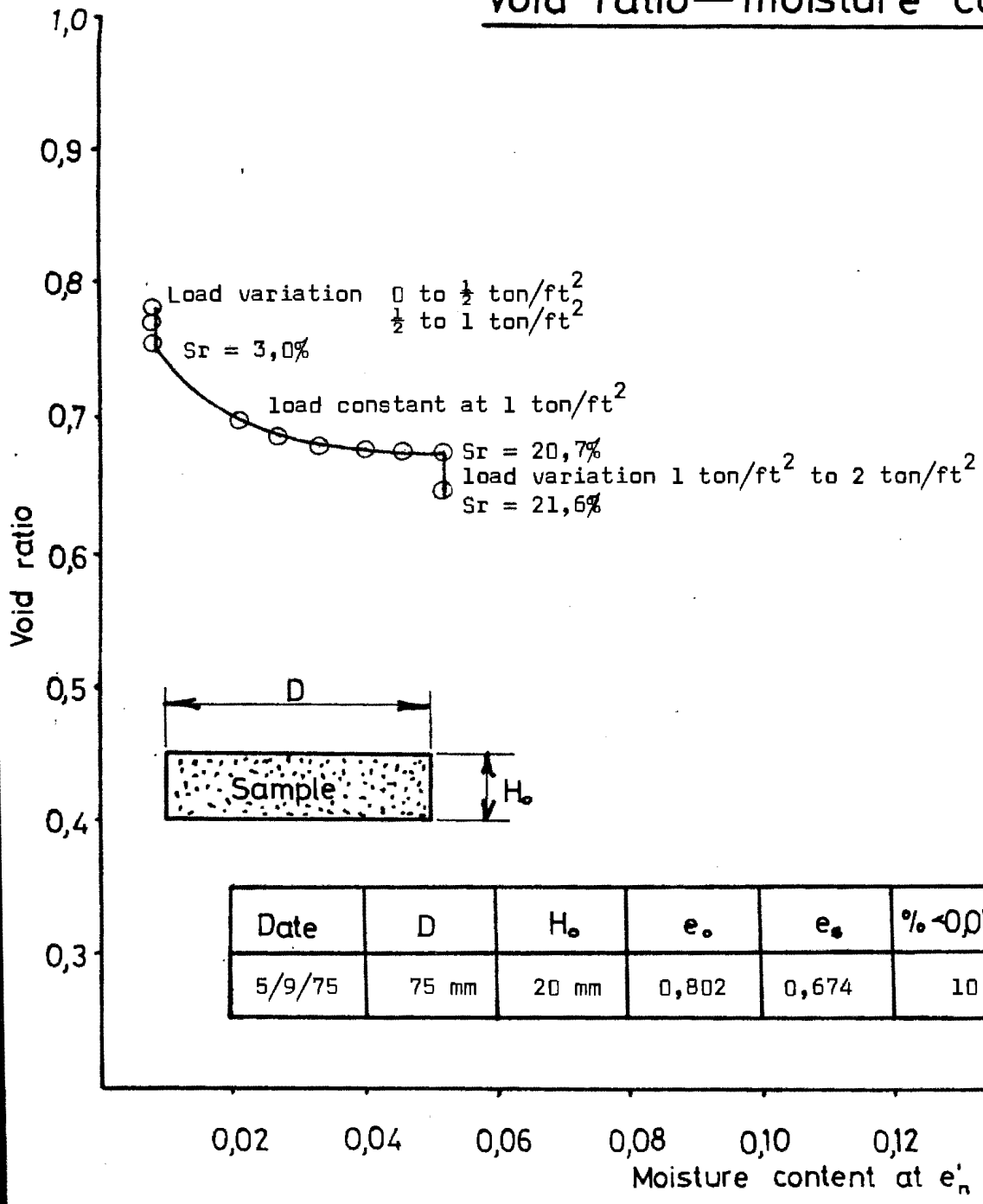
$\bar{p} \rightarrow$
Definition of $\frac{\Delta w}{\Delta w + \Delta p}$

$\frac{\Delta w}{\Delta w + \Delta p}$

Sr = 3%



Void ratio—moisture content graph

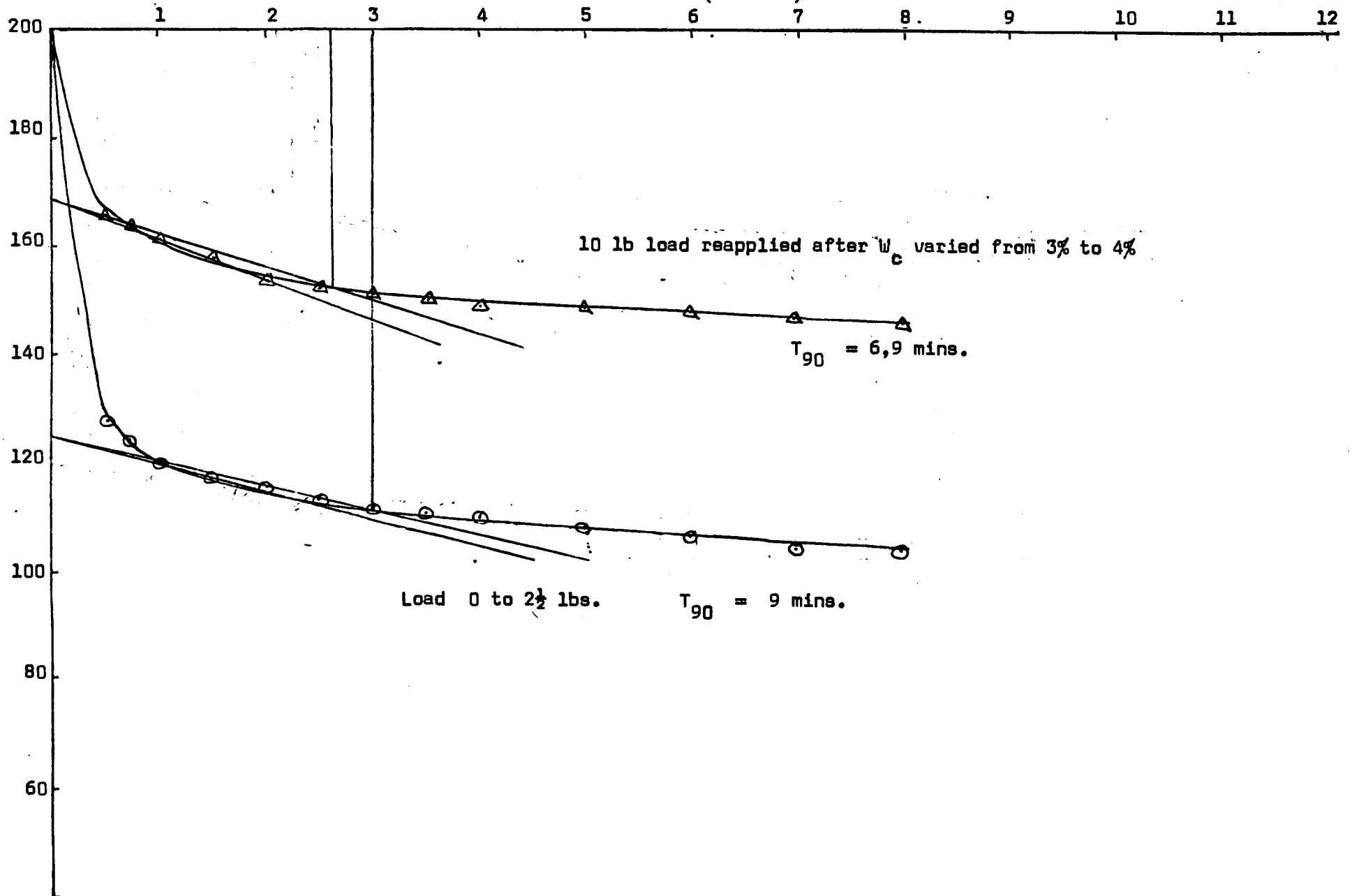


DEFLECTION - TIME CURVE FOR SISHEN SAMPLE

VARYING MOISTURE CONTENT

Dial gauge readings referred to a common origin

time (minutes)^{1/2}



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IRIAXIAL

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample
from Sishen

SPECIFIC GRAVITY 2,68

TEST NO. T-SH-1

TESTED BY

DATE 20-8-75

IRIAXIAL CELL

MASS SOIL INITIAL 136,3 g

MASS DRY SOIL 134,3 g

MASS WATER INITIAL 2,0 g

FIELD MOISTURE CONTENT 1,5%

MASS SOIL FINAL

MASS DRY SOIL

MASS WATER FINAL

FINAL MOISTURE CONTENT

MASS OF CONTAINER

REMARKS.

Initial sample height = 89mm

Initial sample diameter = 39mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	2,5	8,5
35	21	2,5	9,5
36	22	2,5	10,0
40	24	3,0	11,5
41	25	3,0	12,5
42	25	3,0	12,5
44	26	3,5	14,5
47	28	3,5	16,0
51	31	4,0	17,5
52	31	4,0	17,5
54	32	4,0	18,0
60	36	4,5	20,0
61	37	4,5	20,5
64	38	4,5	21,5
65	39	4,5	22,5
67	40	5,0	23,5
69	41	5,0	24,5
71	43	5,0	26,0
73	44	5,0	27,0
74	44	5,0	27,0
76	46	5½	29,0
77	46	5½	29,0
81	49	6	31,0
83	50	6	32,5
85	51	6	33,5
87	52	6	34,5
88	53	6	35,5
91	55	6½	38,0
94	56	6½	39,0
103	62	7	44,0
104	62	7	44,0
106	64	7½	46,5
109	65	7½	47,5
118	71	8	1 06,0
121	73	8	1 10,5
123	74	8	1 11,5
134	80	8½	1 20,0
137	82	8½	1 22,0

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample
from Sishen

SPECIFIC GRAVITY 2.68

TEST NO. T-SH-2

TESTED BY _____

DATE 22-8-75

TRIAXIAL CELL _____

MASS SOIL INITIAL 128.4 g

MASS DRY SOIL 126.1 g

MASS WATER INITIAL 2.3 g

FIELD MOISTURE CONTENT 1.8%

MASS SOIL FINAL _____

MASS DRY SOIL _____

MASS WATER FINAL _____

FINAL MOISTURE CONTENT _____

MASS OF CONTAINER _____

REMARKS:

Initial sample height = 79mm

Initial sample diameter = 38mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	2½	7,5
35	21	2½	8,5
36	22	2½	9,5
40	24	3	11,0
41	25	3	12,0
42	25	3	12,0
44	26	3½	13,0
47	28	3½	14,0
51	31	4	15,5
52	31	4	15,5
54	32	4½	16,5
60	36	4½	18,5
61	37	4½	19,0
64	38	5	19,5
65	39	5	20,5
67	40	5	21,5
69	4	5	22,0
71	43	5½	23,0
73	44	5½	23,5
74	44	5½	23,5
76	46	5½	24,5
77	46	5½	24,5
81	49	6	26,5
83	50	6	27,0
85	51	6	27,5
87	52	6	28,0
88	53	6	28,5
91	55	6½	30,0
94	56	6½	30,5
103	62	7	33,5
104	62	7	33,5
106	64	7	34,5
109	65	7	35,0
118	71	7½	37,5
121	73	7½	38,5
123	74	7½	39,0
134	80	8	42,5
137	82	8	43,0

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample
from Siahon

SPECIFIC GRAVITY 2,68

TEST NO. T-SH-3

TESTED BY _____

DATE 2-9-75

TRIAXIAL CELL _____

MASS SOIL INITIAL _____

MASS DRY SOIL _____

MASS WATER INITIAL _____

FIELD MOISTURE CONTENT _____

MASS SOIL FINAL 230,2 g

MASS DRY SOIL 217,6 g

MASS WATER FINAL 12,6 g

FINAL MOISTURE CONTENT 10,6%

MASS OF CONTAINER 98,1 g

REMARKS:

Initial height of sample = 75mm

Initial diameter of sample = 38mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	2½	16,0
35	21	2½	20,5
36	22	3	23,0
40	24	3	29,0
41	25	3½	31,0
42	25	3½	31,0
44	26	3½	32,0
47	28	3½	33,5
51	31	4	37,0
52	31	4	37,0
54	32	4	38,0
60	36	4½	42,0
61	37	4½	43,0
64	38	4½	44,0
65	39	5	45,5
67	40	5	46,5
69	41	5	47,5
71	43	5½	49,5
73	44	5½	1 01,0
74	44	5½	1 01,0
76	46	6	1 03,0
77	46	6	1 05,0
81	49	6	1 06,0
83	50	6½	1 06,0
85	51	6½	1 06,5
87	52	6½	1 07,0
88	53	6½	1 07,5
91	55	7	1 08,5
94	56	7	1 09,0
103	62	7½	1 12,5
104	62	7½	1 12,5
106	64	7½	1 14,0
109	65	8	1 14,5
118	71	8½	1 18,5
121	73	8½	1 20,0
123	74	8½	1 20,5
134	80	9	1 24,0
137	82	9	1 25,0

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample from
Sishen

SPECIFIC GRAVITY 2.68

TEST NO. T-SH-5

TESTED BY _____

DATE 8-9-75

TRIAXIAL CELL _____

MASS SOIL INITIAL _____

MASS DRY SOIL _____

MASS WATER INITIAL _____

FIELD MOISTURE CONTENT _____

MASS SOIL FINAL 230.3 g

MASS DRY SOIL 225.0 g

MASS WATER FINAL 5.3 g

FINAL MOISTURE CONTENT 3.8%

MASS OF CONTAINER 85.5 g

REMARKS:

Initial sample height = 81mm

Initial diameter of sample = 38mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	2½	29,0
35	21	2½	30,0
36	22	2½	31,0
40	24	3	33,5
41	25	3	36,0
42	25	3	36,0
44	26	3½	37,0
47	28	3½	39,0
51	31	4	44,5
52	31	4	44,5
54	32	4	45,5
60	36	4½	46,0
61	37	4½	47,0
64	38	4½	48,0
65	39	4½	49,0
67	40	5	1 00,0
69	41	5	1 01,0
71	43	5½	1 03,0
73	44	5½	1 04,5
74	44	5½	1 04,5
76	46	5½	1 07,5
77	46	5½	1 07,5
81	49	6	1 10,0
83	50	6	1 11,5
85	51	6	1 12,5
87	52	6	1 13,0
88	53	6½	1 14,0
91	55	6½	1 14,5
94	56	6½	1 15,5
103	62	7	1 20,0
104	62	7	1 20,0
106	64	7	1 21,0
109	65	7½	1 22,0
118	71	8	1 28,5
121	73	8	1 29,5
123	74	8	1 30,5
134	80	8½	1 35,5
137	82	8½	1 38,0

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample
from Siehen

SPECIFIC GRAVITY 2.68

TEST NO. T-SH-6

TESTED BY

DATE 10-9-75

TRIAXIAL CELL

MASS SOIL INITIAL

MASS DRY SOIL

MASS WATER INITIAL

FIELD MOISTURE CONTENT

MASS SOIL FINAL 243.2 g

MASS DRY SOIL 231.5 g

MASS WATER FINAL 11.7 g

FINAL MOISTURE CONTENT 8.8%

MASS OF CONTAINER 98.0 g

REMARKS:

Initial sample height = 80mm

Initial sample diameter = 38mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	3	1 10,5
35	21	3	1 15,0
36	22	3	1 17,5
40	24	3	1 22,0
41	25	3½	1 24,0
42	25	3½	1 24,0
44	26	3½	1 25,5
47	28	4	1 30,0
51	31	4	1 37,0
52	31	4	1 37,0
54	32	4	1 39,0
60	36	4½	1 46,0
61	37	4½	1 48,0
64	38	4½	2 00,0
65	39	4½	2 02,0
67	40	5	2 04,0
69	41	5	2 05,5
71	43	5½	2 08,5
73	44	5½	2 10,0
74	44	5½	2 10,0
76	46	5½	2 12,5
77	46	5½	2 12,5
81	49	6	2 23,5
83	50	6	2 26,0
85	51	6	2 27,5
87	52	6	2 28,5
88	53	6½	2 30,5
91	55	6½	2 34,5
94	56	6½	2 36,0
103	62	7	2 43,0
104	62	7	2 43,0
106	64	7½	2 44,5
109	65	7½	2 45,0
118	71	8	3 01,5
121	73	8	3 03,5
123	74	85	3 05,0
134	80	8½	3 18,0
137	82	8½	3 12,0

SAMPLE DESCRIPTION Brown fine grained collapsing sand - undisturbed sample
from Siahon

SPECIFIC GRAVITY 2.68

TEST NO. T-SH-7

TESTED BY

DATE 11-9-75

TRIAXIAL CELL

MASS SOIL INITIAL

MASS DRY SOIL

MASS WATER INITIAL

FIELD MOISTURE CONTENT

MASS SOIL FINAL 235.9 g

MASS DRY SOIL 222.8 g

MASS WATER FINAL 13.1 g

FINAL MOISTURE CONTENT 10.3%

MASS OF CONTAINER 95.1 g

REMARKS:

Initial sample height = 77mm

Initial sample diameter = 39mm

VERTICAL STRESS kN/m ²	DEVIATOR STRESS kN/m ²	CELL PRESSURE lb/in ²	DIAL GAUGE READINGS
31	19	3	1 03,0
35	21	3	1 06,0
36	22	3	1 09,0
40	24	3	1 12,5
41	25	3½	1 14,0
42	25	3½	1 14,0
44	26	3½	1 20,0
47	28	4	1 26,0
51	31	4	1 34,0
52	31	4	1 34,0
54	32	4	1 35,0
60	36	4½	1 39,5
61	37	4½	1 40,5
64	38	4½	1 41,5
65	39	4½	1 42,5
67	40	5	1 43,5
69	41	5	1 44,5
71	43	5½	1 45,5
73	44	5½	1 46,5
74	44	5½	1 46,5
76	46	5½	1 49,5
77	46	5½	1 49,5
81	49	6	2 03,5
83	50	6	2 05,0
85	51	6	2 06,0
87	52	6	2 07,0
88	53	6½	2 08,5
91	55	6½	2 11,0
94	56	6½	2 12,0
103	62	7	2 20,0
104	62	7	2 20,0
106	64	7½	2 22,0
109	65	7½	2 23,0
118	71	8	2 33,0
121	71	8	2 35,0
123	74	8	2 36,0
134	80	8½	2 40,5
137	82	8½	2 41,5

8/111

TRIAXIAL

SAMPLE DESCRIPTION Brown fine grained collapseing sand - undisturbed sample
from Sishen

SPECIFIC GRAVITY 2.68

TEST NO. T-SH-8

TESTED BY _____

DATE 15-9-75

TRIAXIAL CELL _____

MASS SOIL INITIAL _____

MASS DRY SOIL _____

MASS WATER INITIAL _____

INITIAL MOISTURE CONTENT _____

MASS SOIL FINAL 234.6 g

MASS DRY SOIL 223.4 g

MASS WATER FINAL 11.2 g

FINAL MOISTURE CONTENT 8.6%

MASS OF CONTAINER 94.1 g

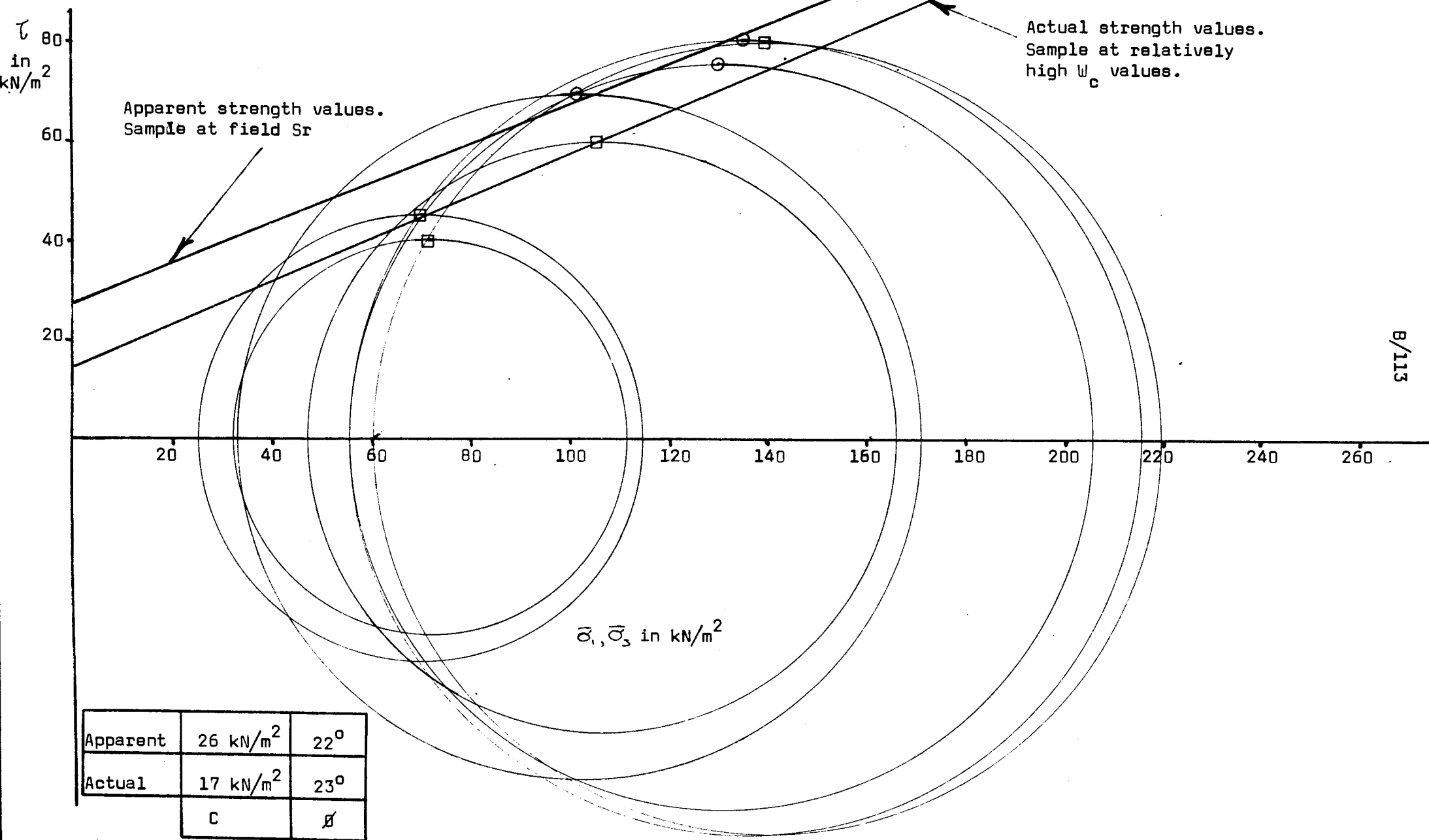
REMARKS:

Initial sample height = 79mm

Initial sample diameter = 39mm

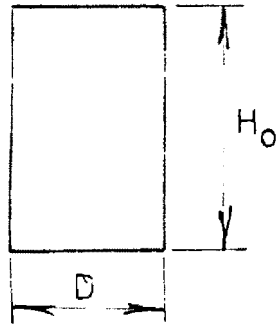
[illegible]

TRIAXIAL STRENGTH RESULTS - SAMPLE EX SISHEN



K₀ Lines - Triaxial K₀ tests

Sample description	Field	wc (%)	e ₀	Clay content (%)	D	H ₀
collapsing sands		0,8	0,802	10	39	78



K₀ = 0,45
 moisture content = 10,6%
 Sr =

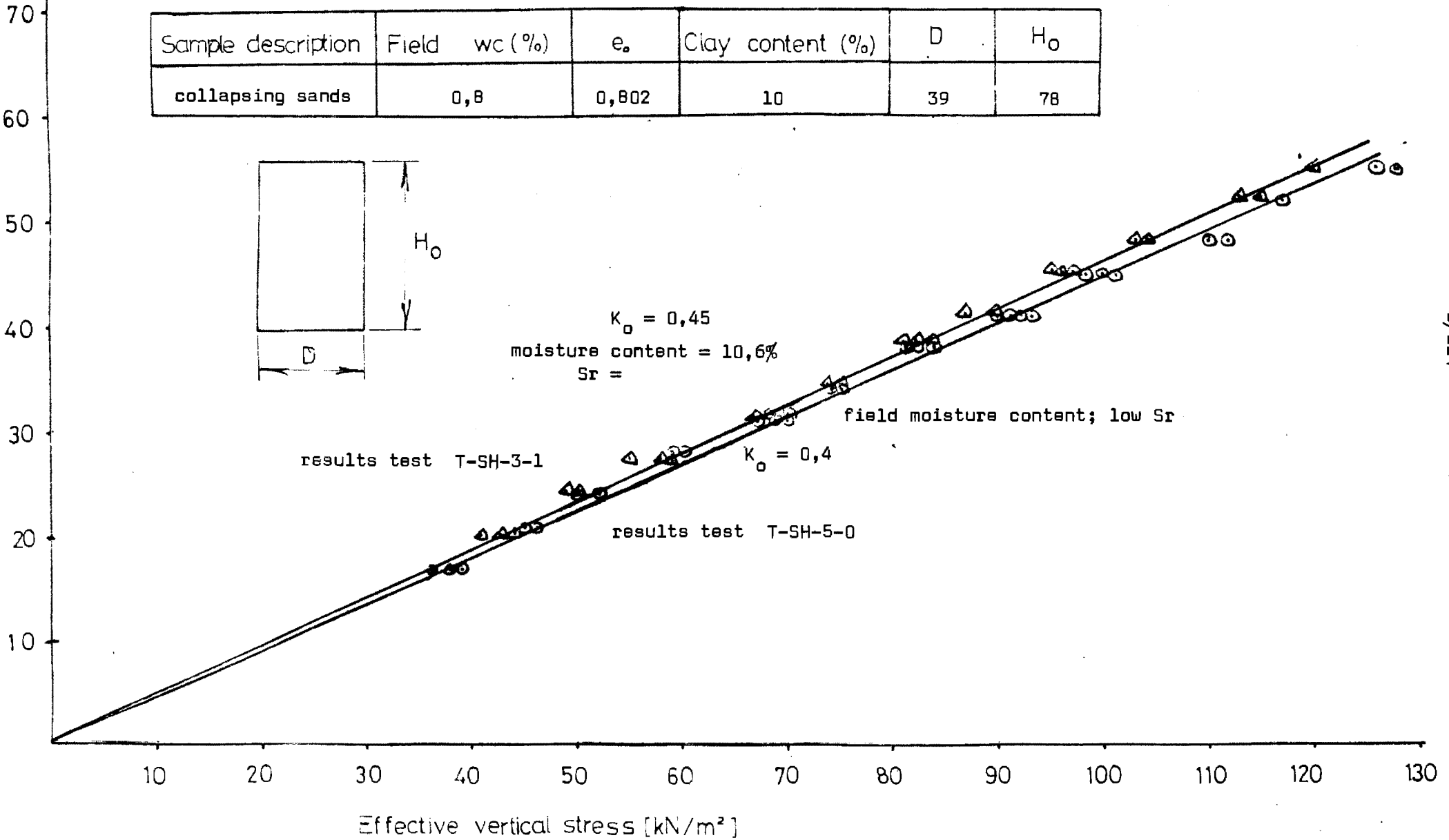
field moisture content; low Sr

results test T-SH-3-1

K₀ = 0,4

results test T-SH-5-0

B/114



Unit weight of the soils:

Berea Road

$$e_o = 0,712$$

$$Sr = 3\%$$

$$\gamma_{Bulk} = \frac{2,68 + eSr_w}{1 + e}$$

$$= 15,78 \text{ kN/m}^2$$

Feathers

$$e_o = 0,918$$

$$sr = 5,8\%$$

$$\gamma_{Bulk} = 14,26 \text{ kN/m}^2$$

Sishen

$$e_o = 0,802$$

$$Sr = 1\%$$

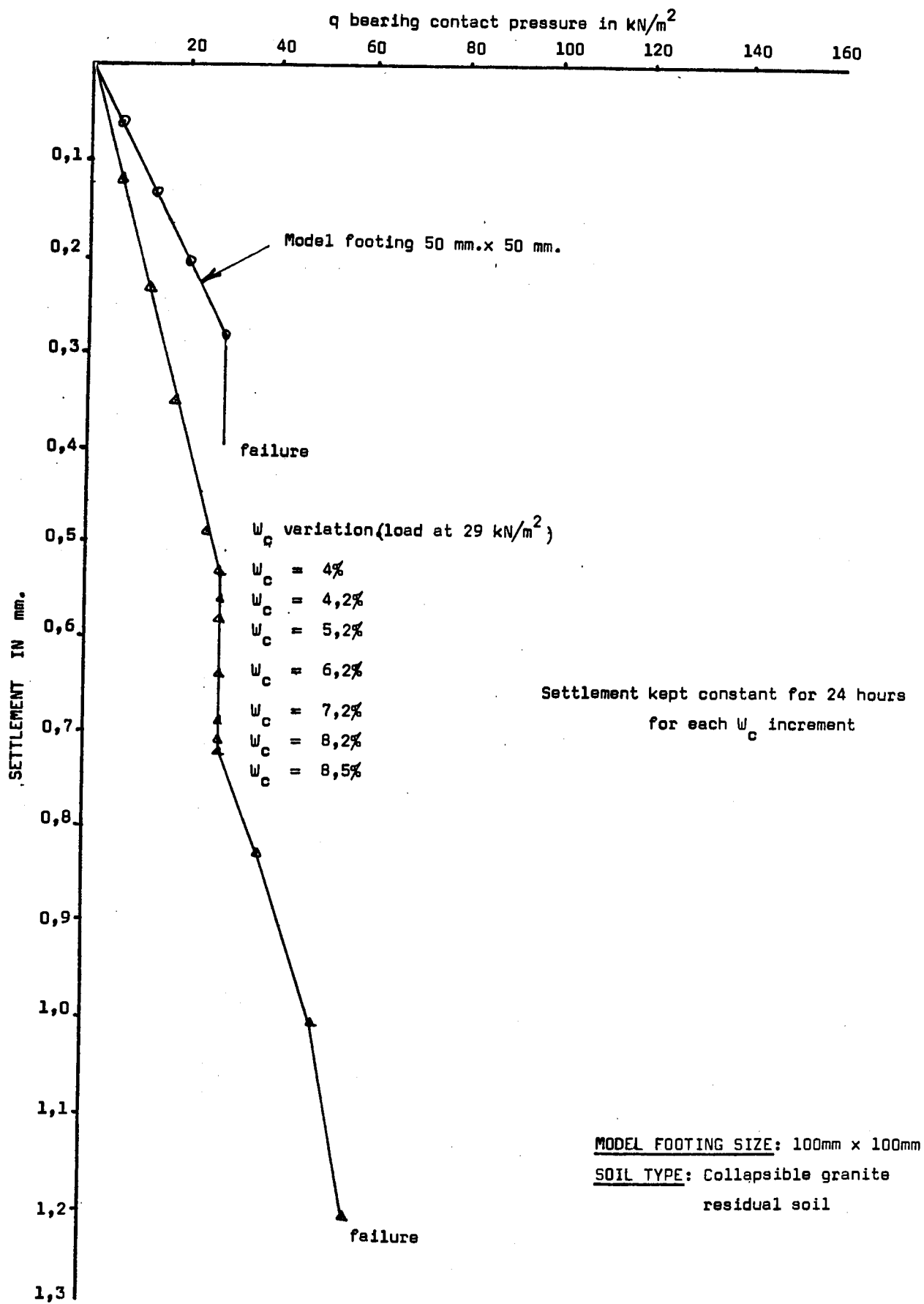
$$\gamma_{Bulk} = 14,92 \text{ kN/m}^2$$

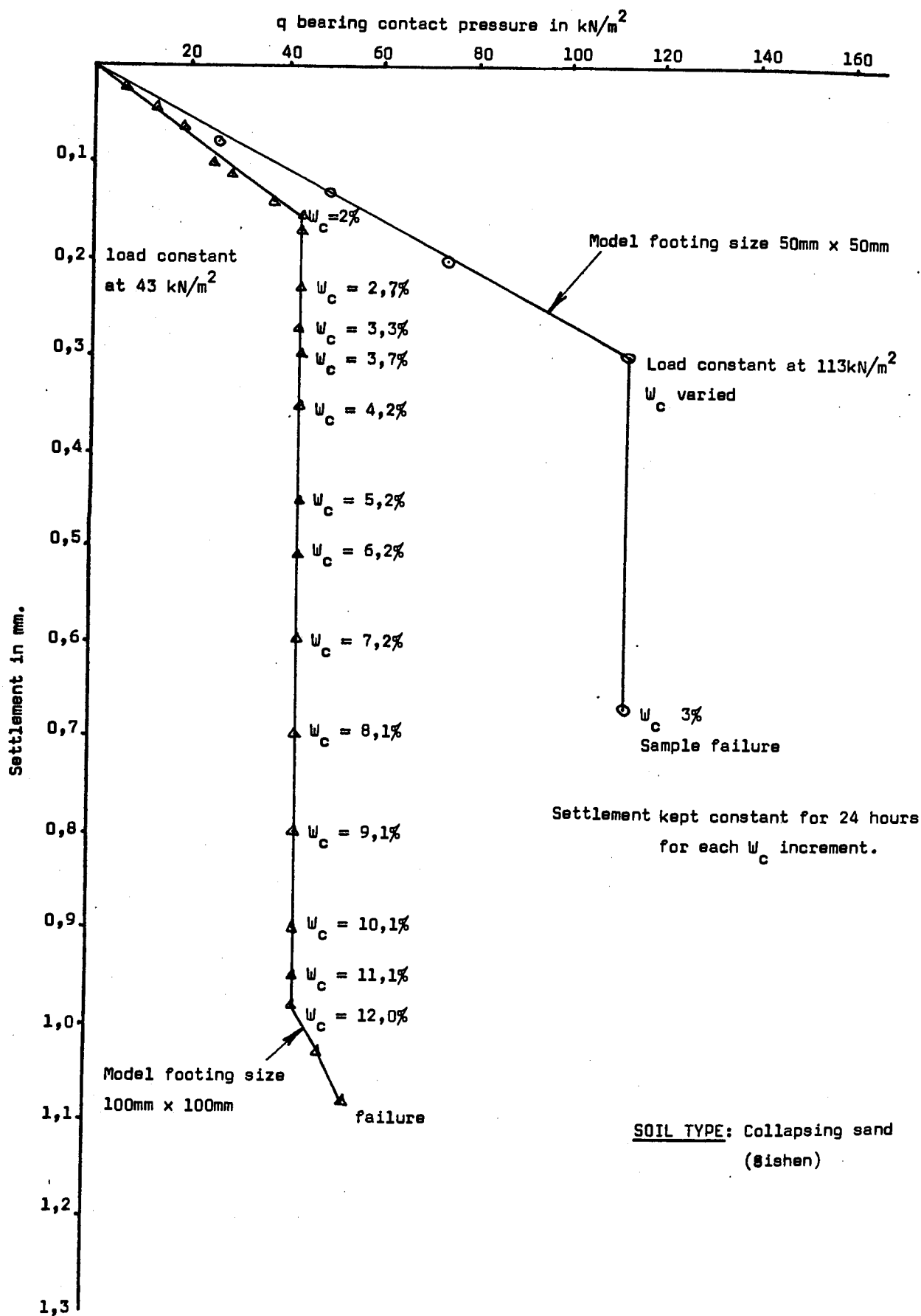
Therefore approximate all to be 15 kN/m^3 . This value is very nearly correct and it will enable the same stress paths to be used throughout the test series.

Footing size	Depth below the centre of the footing. m.	Vertical stress due to self weight. kN/m ²	Vertical stress due to self weight + footing load. kN/m ²
1,0 x 1,0	0,1	16,5	95,7
	0,2	18,0	94,8
	0,3	19,5	90,9
	0,4	21,0	83,4
	0,5	22,5	82,3
	1,0	30,0	57,5
	2,0	45,0	54,2
2,0 x 2,0	0,2	18,0	97,2
	0,4	21,0	97,8
	0,6	24,0	95,4
	1,0	30,0	89,8
	2,0	45,0	72,2
	4,0	75,0	84,2
3,0 x 3,0	0,3	19,5	98,7
	0,6	24,0	100,8
	1,0	30,0	103,1
	2,0	45,0	92,6
	3,0	60,0	87,2
	6,0	105,0	114,2

Footing size	Depth below the centre of the footing	$\frac{\Delta e}{1+e_0}$ Results from Consolidometer Tests	$\frac{\Delta H}{H}$ Results from Stress path Tests	Soil	w _c
1,0 x 1,0	0,1	1,57%	1,15%	Collap- sing granitic residual soil	low
	0,2	1,50%	1,10%		
	0,3	1,31%	0,95%		
	0,4	1,30%	0,90%		
	0,5	1,05%	0,80%		
	1,0	0,53%	0,40%		
	2,0	0,26%	0,20%		
2,0 x 2,0	0,2	1,31%	0,90%	Collap- sing granitic residual soil	low
	0,4	1,29%	0,95%		
	0,6	1,23%	1,00%		
	1,0	1,05%	0,80%		
	2,0	0,53%	0,35%		
	4,0	0,26%	0,10%		
3,0 x 3,0	0,3	1,57%	1,05%	Collap- sing granitic residual soil	low
	0,6	1,41%	1,00%		
	1,0	1,31%	0,85%		
	2,0	0,79%	0,60%		
	3,0	0,53%	0,30%		
	6,0	0,11%	0,10%		
1,0 x 1,0	0,1	7,60%	7,50%	Collap- sing granitic residual soil	high
	0,2	7,49%	7,25%		
	0,3	7,02%	7,15%		
	0,4	6,39%	6,20%		
	0,5	6,05%	6,05%		
	1,0	3,23%	2,90%		
	2,0	0,88%	0,70%		
2,0 x 2,0	0,2	7,49%	7,20%	Collap- sing granitic residual soil	high
	0,4	7,14%	6,90%		
	0,6	6,79%	6,35%		
	1,0	5,75%	5,20%		
	2,0	2,29%	2,30%		
	4,0	0,65%	0,95%		
3,0 x 3,0	0,3	7,30%	7,25%	Collap- sing granitic residual soil	high
	0,6	7,26%	6,65%		
	1,0	6,30%	5,90%		
	2,0	3,91%	3,55%		
	3,0	2,05%	1,95%		
	6,0	0,65%	0,70%		

Footing size	Depth below the centre of the footing	$\frac{\Delta e}{1+e_0}$ Results from Consolidometer Tests	$\frac{\Delta H}{H}$ Results from Stress path Tests	Soil	w_c
1,0 x 1,0	0,1 0,2 0,3 0,4 0,5 1,0 2,0	1,42% 1,12% 0,85% 0,62% 0,53% 0,28% 0,08%	0,85% 0,80% 0,75% 0,70% 0,65% 0,36% 0,15%	Collap- sing sand - Sishen	low
2,0 x 2,0	0,2 0,4 0,6 1,0 2,0 4,0	1,35% 1,35% 0,88% 0,62% 0,22% 0,06%	0,80% 0,85% 0,78% 0,70% 0,30% 0,10%	Collap- sing sand - Sishen	low
3,0 x 3,0	0,3 0,6 1,0 2,0 3,0 6,0	1,35% 1,35% 1,07% 0,87% 0,69% 0,08%	0,88% 0,85% 0,78% 0,55% 0,40% 0,10%	Collap- sing sand - Sishen	low
1,0 x 1,0	0,1 0,2 0,3 0,4 0,5 1,0 2,0		1,75% 1,65% 1,55% 1,40% 1,30% 0,70% 0,35%	Collap- sing sand - Sishen	high
2,0 x 2,0	0,2 0,4 0,6 1,0 2,0 4,0		1,70% 1,60% 1,50% 1,30% 0,65% 0,15%	Collap- sing sand - Sishen	High
3,0 x 3,0	0,3 0,6 1,0 2,0 3,0 6,0		1,65% 1,60% 1,45% 0,95% 0,50% 0,10%	Collap- sing sand - Sishen	High





APPENDIX C

COURSES COMPLETED IN PARTIAL FULFILMENT
OF THE M.Sc. (ENG.) DEGREE AT THE UNIVERSITY OF CAPE TOWN

<u>COURSE</u>	<u>YEAR CREDITED</u>	<u>CREDIT VALUE</u>
Introduction to Management Accounting	1975	5
Coastal Engineering	1975	5
Probability and Engineering Statistics	1975	4
Prestressed Concrete	1975	5
Skeletal Structures	1975	5

Total credit requirements for the M.Sc. (Eng.) Degree: 40

Half Thesis: 20

Course Credits 24

Total: 44

UNIVERSITY OF CAPE TOWN

DEPARTMENT OF CIVIL ENGINEERING

M.Sc. IN CIVIL ENGINEERING

UNIVERSITY EXAMINATION : JULY 1977

CE 525 : Coastal Hydraulics

All Questions may be attempted

Time : 3 hours

Constants

Sea water density = 1025 kg/m^3

Sea water weight = 10 kN/m^3

1. A beach site has an average underwater slope of 1 in 50, and the beach material is a coarse quartz sand of relative density 2,65 and average size 1,35 mm, the shoreline being essentially straight.

Two conditions of wave attack are being considered :-

- (A) swell of 10 second period with a deep water wave height of 1,6 m approaching the beach with wave crests parallel to the shore line.
- (B) as in (A) above, but with a deep water wave incidence of 35° , (angle between wave crest and contour)

For case (A) make the following calculations :-

- (a) the wave length and wave celerity in deep water.
- (b) the water depth at which the wave begins to be affected by the presence of the sea bed.
- (c) the wavelength, celerity and height for water depths at 10 m intervals between $d=80 \text{ m}$ and $d=10 \text{ m}$, and at 1 m intervals between $d=10 \text{ m}$ and $d=1 \text{ m}$.
- (d) the water depth in which the wave breaks, the breaker type, and the wave height at breaking. Ignore the effect of wave set up or down.
- (e) the deep water energy flow.
- (f) the wave height and energy flow in a water depth of 1 m.
- (g) the water depth in which the sand is on the point of moving.
- (h) the water depth in the which the sand is in motion but has no net drift.

For case (B) make the following calculations :-

- (i) the water depths in which the angle of incidence becomes 30° , 20° , 10° and 5° , and the wave heights at these depths.
 - (j) the water depth and wave height under breaking conditions. (assume the depth at breaking is 80 per cent of the value obtained for parallel waves)
 - (k) the thrust on the mass of water in the surf zone, per metre length along the shore. (N)
 - (l) an estimate of the bulk sand volume flow rate in m^3/s in the alongshore direction.
2. A cylindrical pipe is laid on the sea bed across a harbour entrance in 10 m of water, the pipe diameter being 0,3 m, and the axis of the pipe is parallel to the local wave crests. If the local wave length is 50 m, estimate the wave period, and find the peak magnitudes of the velocity and acceleration force components per metre length of pipe. Estimate the peak resultant force in the inshore direction, and the timing of this in relation to the passage of the wave crest. The wave height is 2 m, take $C_D = 1,2$ and $C_M = 2,16$
3. (a) A steady wind of speed 15 m/s blows over a fetch for a period of 8 hours, producing a significant wave height of 1,8 m at the downwind end of the fetch. Estimate the fetch length in km and the wave period. Check whether the wind duration is sufficient for this condition to be stable and also check whether this is the fully arisen sea for this wind speed.
- (b) In a zero damage design calculation for the armour protection of a rubble mound breakwater, 3 tonne and 5 tonne dolosse are specified for the trunk and head respectively, the slope of the breakwater face being $\cot \theta = 2$. Estimate the block masses and block heights if tetrapods had been used in the same design. If the design wave height was 3 m, and a storm causes damage of the order 20-30 per cent to the tetrapod scheme, estimate the storm wave height. (concrete density = 2245 kg/m^3)
- (c) An incoming swell has crests parallel to a straight beach with a deep water wave height of 2 m. Estimate the horizontal force (per metre along the beach) acting on the beach inside the refraction zone, due to the dynamic action of the waves.
- (d) In an area where the sea bed is horizontal, and the water depth is 3 m, a wave has a period of 7 s, a wavelength of 38 m, and a wave height of 1,5 m. Estimate the drift velocity at bed level, and indicate the direction. Compare this velocity with the maximum orbital velocity at the same level, and indicate the influence on bed drift of a strong onshore wind.
- (e) A storm at sea generates waves with a period range of 8 to 16 seconds. The resulting swell travels towards a harbour 500 km away. Estimate the time interval between the arrival of the shortest and longest waves, assuming deep water throughout.

UNIVERSITY OF CAPE TOWN
DEPARTMENT OF CIVIL ENGINEERING
UNIVERSITY EXAMINATION: JUNE, 1975
COURSE CE 508 - SKELETAL STRUCTURES

Time allowed: 4 hours

Notes are allowed

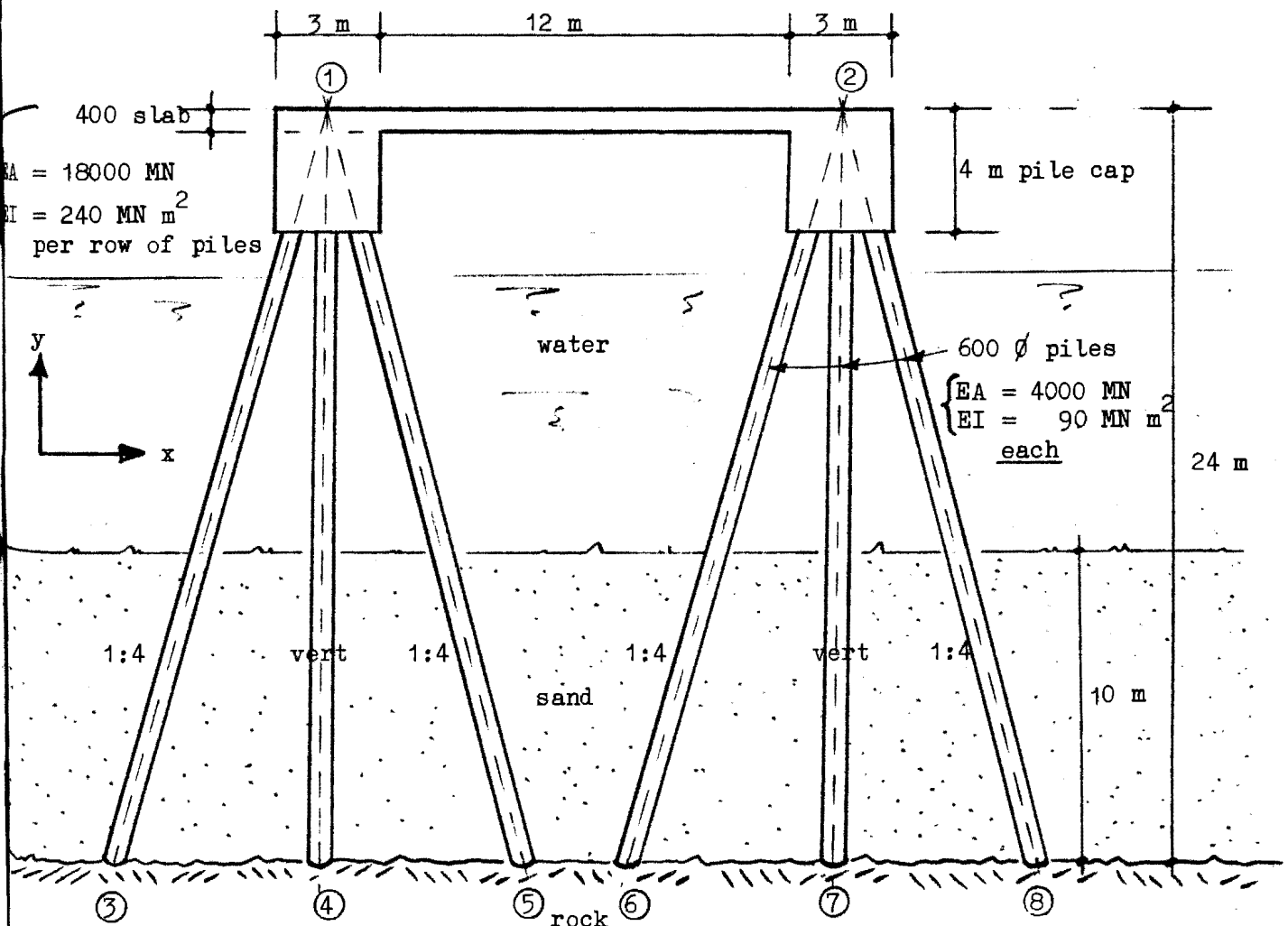
Part A: For each of the five structures shown below determine the degree of static and of effective kinematic indeterminateness, select the most suitable method of analysis, give the order of all the relevant matrices required for solution by the chosen method. State clearly what assumptions are made.

[40 marks]

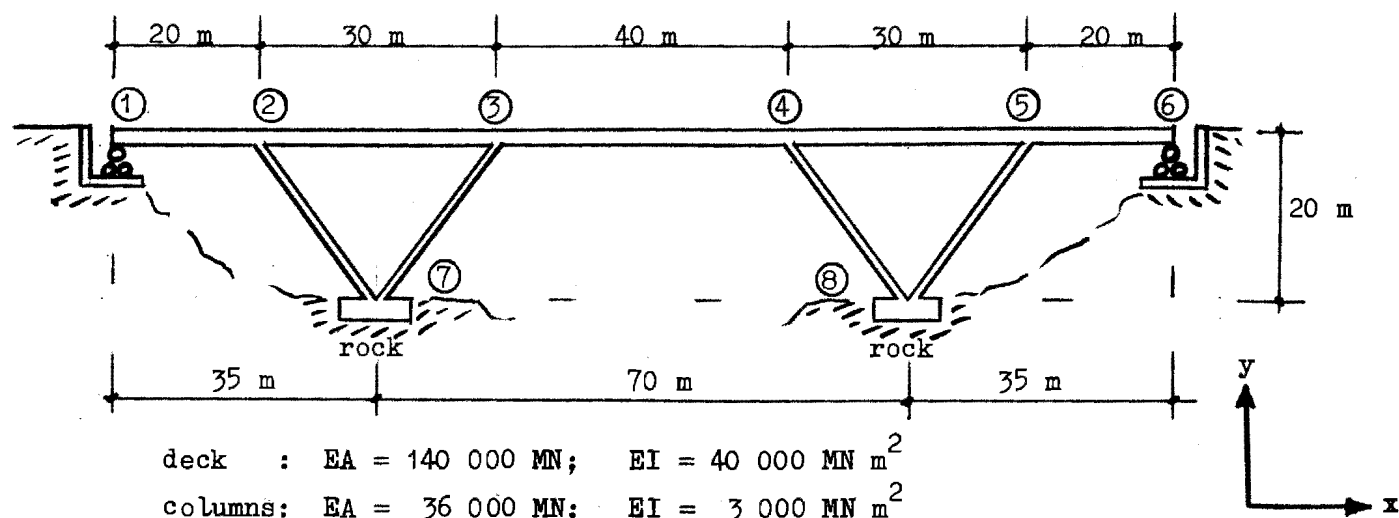
Part B: Compile the matrices for any two of these structures; one analysed by the FORCE method and one analysed by the DISPLACEMENT method. Do not attempt to complete all the arithmetic processes, but give sufficient detail to show clearly the principles and operations involved.

[60 marks]

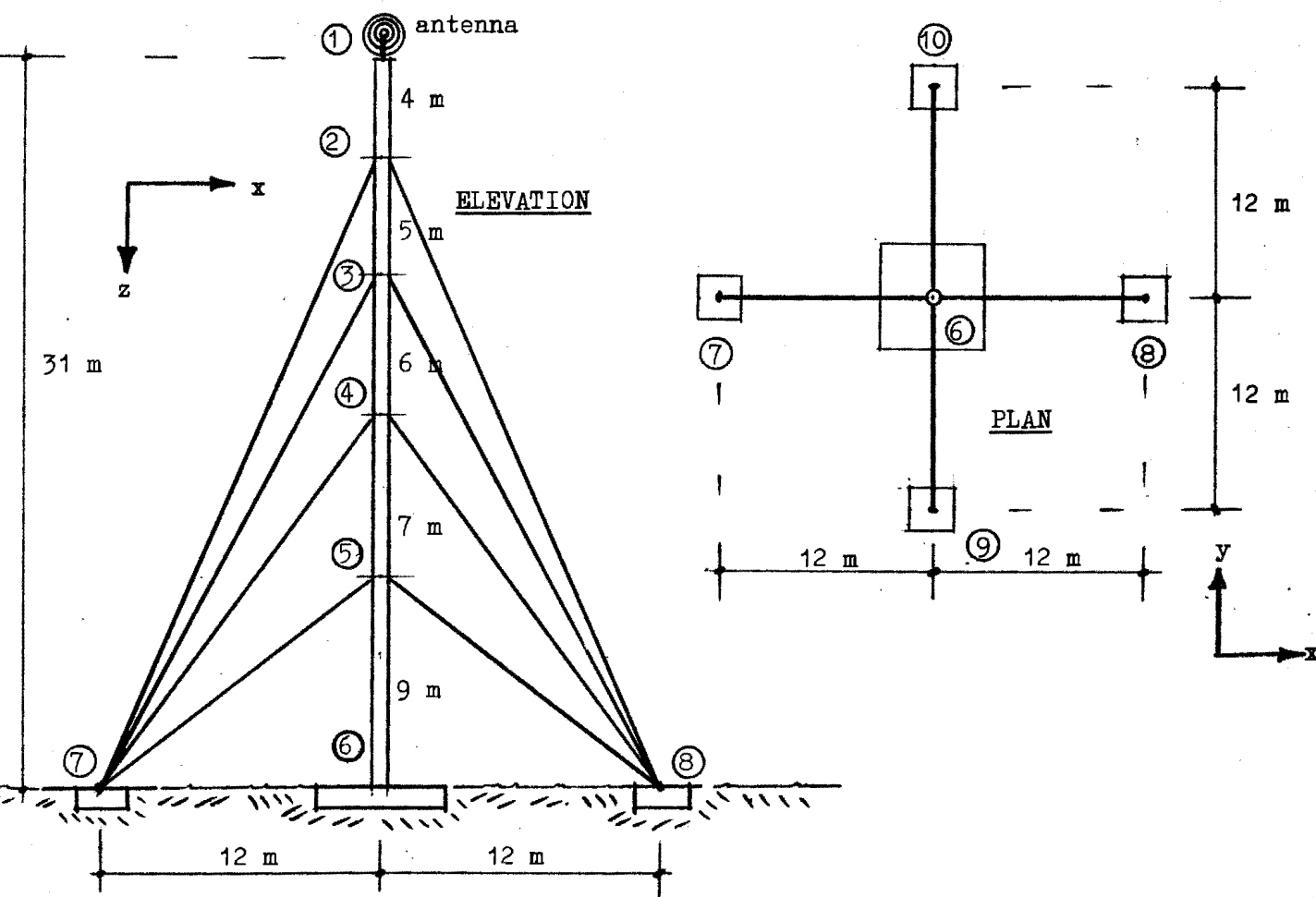
1. Jetty with vertical and horizontal loads applied to the top surface in the xy plane. The pile rows are at 3 m spacing along the jetty.



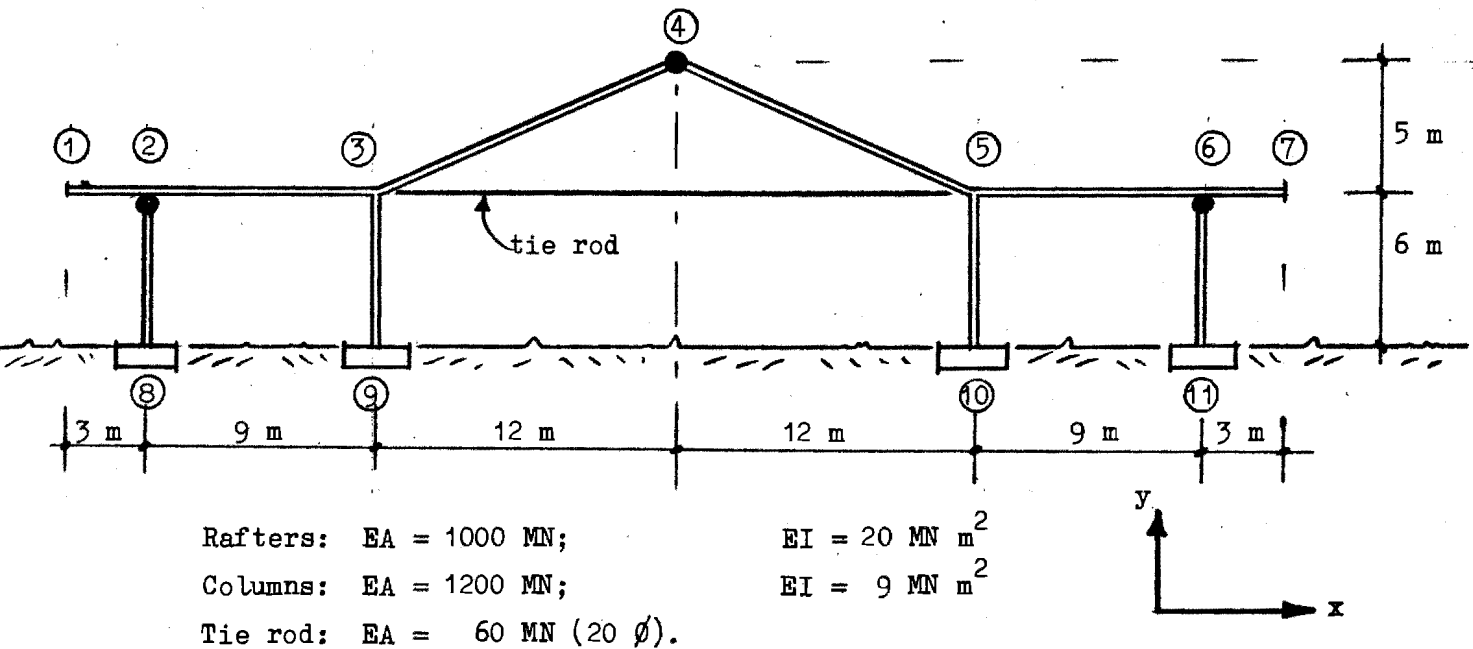
2. Bridge, monolithic concrete beam-slab deck and inclined columns, with vertical and horizontal loading applied to the deck.



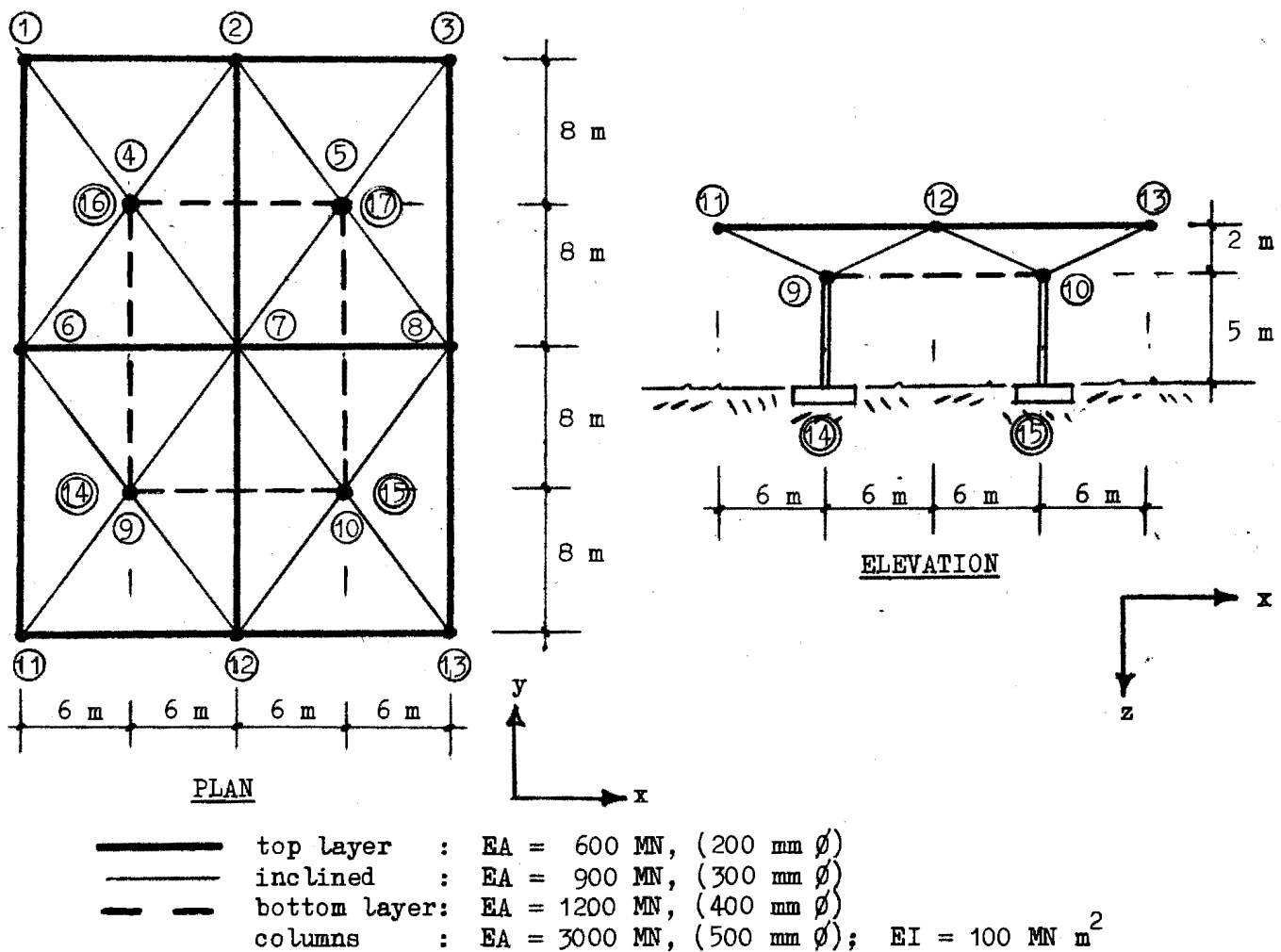
3. Tower, consisting of a single vertical tubular column fixed at the base and stayed at right angles on four levels with steel wire guy ropes, which are sufficiently pretensioned not to go slack. Loading is applied at the top only.



4. Building, tied steel portal frame with two side bays. Wind, dead and imposed roof loading.



5. Roof, ball-jointed, double-layer, three-way grid on four columns fixed at their bases, all of tubular steel construction, with vertical and horizontal loading applied to the top joints.



UNIVERSITY OF CAPE TOWN
DEPARTMENT OF CIVIL ENGINEERING
UNIVERSITY EXAMINATION, NOVEMBER 1974

CE 504: PROBABILITY AND STATISTICS FOR ENGINEERS

Total marks: 100

Time allowed: 3 hours

External Examiner : Professor D.M. Schultz

Internal Examiners: Professor G.v.R. Marais
Mr. M.S. Green

Attempt ALL questions in Section A and FOUR questions from
Section B and C. Use separate answer book for Section C.

Name:

SECTION A

Note: Answer these questions in the spaces provided on this question
paper. Do not show calculations, enter only the final answer.

1. Give formulae for:

(a) the coefficient of variation;

(b) the mean deviation about the mode.

2. Find the standard deviation of the data: 2; 6; 10.

3. In a particular experiment the result of 10 weighings showed 4 values
between 20 and 25 g, 4 values between 25 and 30 g and 2 values between
30 and 35 g. What was the median weight?

4. An engineering firm has 100 electrical components in stock, 25 manufactured by process A and 75 manufactured by process B. Unknown to the firm, 13 of those manufactured by A are defective and 18 of those manufactured by B are defective.

A component is chosen at random from the 100 components. What is the probability that this component is:

(i) manufactured by B and defective?

(ii) either manufactured by A or is a defective component?

5. An item of radar equipment has three critical components A, B, C. The frequency of defect for component A was found to be 5 per 100, for B to be 6 per 100, and for C to be 8 per 100. Estimate the probability that a given item of equipment is defective.

6. A biased coin which has twice the probability of falling heads as falling tails is tossed with two unbiased coins. What is the probability:

(i) of at least two heads occurring?

(ii) of no heads occurring?

7. At a telephone exchange the average number of calls passed per hour in the morning is 96 and the rate can be regarded as constant. Calculate the probability of:

(i) exactly 3 calls in a period of 5 minutes;

(ii) more than 3 calls in a period of 5 minutes.

8. Packets are filled automatically and on the average, 5 per cent are underweight. An inspector takes a batch of twelve collected randomly. What is the probability that he will find 25 per cent or more underweight?
9. The mean diameter of steel rods produced by a process is 2 cm and the standard deviation is 0,05 cm. Assuming the diameters are normally distributed, find the value such that only 5 per cent of the rods will have a diameter exceeding this value.
10. A sample of 11 lengths of plastic were tested and found to have a standard deviation of 35. A second sample of 9 lengths of plastic, treated by a different process, was tested and found to have a standard deviation of 20. Test whether the standard deviations differ significantly.
11. State the assumptions required for the use of the t-test for the difference between the means of two independent samples.
12. If one denotes by y' the values of y which are calculated by means of the equation of the regression line, what is the least squares criterion?

13. Give the formula for the variance of the mean value of y , that is \bar{y} , where y is estimated from a regression line.
14. Give the formula for the correlation coefficient for two variables x and y .

15.

	Defective	Good	Total
Process A	25	15	40
Process B	35	25	60
Total	60	40	100

Test whether there is a difference between process A and process B in the above table.

SECTION BAnswer these questions in the answer books provided

1. A laboratory balance is used to weigh the same object 100 times. The values are given in the table below.

<u>Weight in g</u>	<u>Number of observations</u>
4,55 - 4,65	10
4,65 - 4,75	20
4,75 - 4,85	45
4,85 - 4,95	15
4,95 - 5,05	10
	<hr/> 100

- (a) Using this data calculate:

- (i) the mean,
- (ii) the mode,
- (iii) the median,
- (iv) the variance and standard deviation,
- (v) the coefficient of variation.

- (b) By fitting a normal distribution to the data, find the expected frequencies in the first two class intervals.

2. (a) Derive the binomial distribution from first principles and hence derive the Poisson distribution from the binomial distribution.
- (b) The probability of a light bulb failing during the first twelve hours of service is 0,0049. If 1000 light bulbs are installed, use the Poisson distribution to find the probability of exactly ten bulbs failing within the first twelve hours.
- (c) A machine is known to produce piston rings of which 10 per cent are defective. Find the probability that in a random sample of 400 rings:
- (i) at most 35 rings will be defective;
 - (ii) between 35 and 50 will be defective.
3. (a) Define with diagram a type I error, type II error and the power of a test.
- (b) The outputs from two production plants A and B were measured on each of 5 days. The data was given as follows:

Output (tons)

<u>Plant A</u>	<u>Plant B</u>
2,0	2,2
1,7	2,0
2,6	2,7
1,7	1,7
2,0	1,9

/Test whether

3. (b) (Continued)

Test whether the output of Plant B is significantly higher than that of Plant A at the 5 per cent level of significance if:

- (i) sample A was considered to be independent of sample B:
- (ii) it was believed that the day on which the observation was made was a relevant factor, and the observations were considered to be paired.

4. An experiment was carried out to measure the resistance of wire from three sources by taking five samples from each source.

- (a) Use analysis of variance to determine whether or not there is a significant difference between the resistance of the wire from the three sources.

Source Sample	A	B	C
1	7,2	8,5	8,3
2	7,3	8,6	8,6
3	7,4	9,0	8,6
4	7,9	8,7	8,7
5	7,7	8,7	8,8

- (b) It is believed that the 5 samples for each source were taken on consecutive days and that the resistance increased each day due to an external factor. Explain how you would test this hypothesis for Source A only.

SECTION C

(Answer this question in a separate answer book).

1. (a) In a set of 10 compressive tests on concrete cubes, two of the tests exceeded the capacity of the testing machine (12 MPa). The 8 definite test results were (in MPa):

11,9 8,0 8,8 11,3 10,7 10,7 9,9 9,7.

For the set of 10 cubes, determine graphically the mean compressive stress and its standard deviation.

- (b) On two succeeding days a set of data was obtained on the concentration of bacteria in the effluent from a sewage works. The two sets of ranked data are:

Set 1: 400 700 850 1200 1900

Set 2: 750 1200 1700 1900 2400 3100 3600 5000 6000 11000

The data is expected to be log-normally distributed.

/(i) Determine

1. (b) (Continued)

- (i) Determine (using graphical procedures) the log-mean, geometric-mean of each set of data.
 - (ii) Test if the log-means are significantly different at 96 per cent level of significance.
 - (iii) Briefly explain why you performed the test for significance (in (ii) above), on the differences of the log-means and not on the differences of the geometric and arithmetic-means.
- (c) List the conditions which must prevail for (i) a normal, (ii) a log-normal, distribution to arise.

UNIVERSITY OF CAPE TOWN

DEPARTMENT OF CIVIL ENGINEERING

UNIVERSITY EXAMINATION: DECEMBER, 1975

M.Sc. IN CIVIL ENGINEERING

COURSE CE 516: PRESTRESSED CONCRETE

Time allowed: 3 hours

Attempt ALL questions

Any books and notes may be used

1. (a) State as concisely as possible the reason why it is essential in prestressed concrete design to check both the serviceability and ultimate limit states.

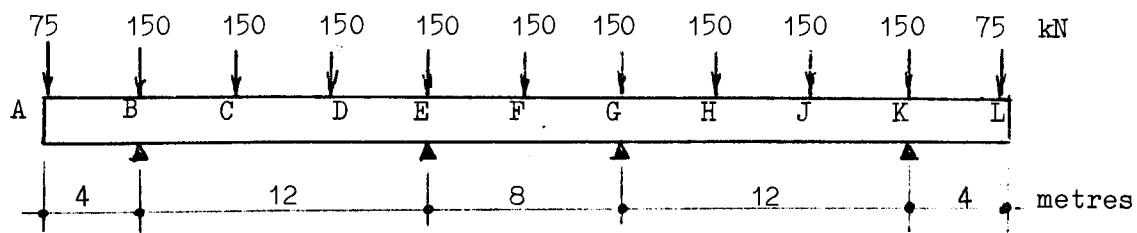
[3 marks]
- (b) In a partially prestressed member a certain amount of untensioned reinforcement is normally required. Show, with the aid of appropriate diagrams, how you would determine, in the design of a particular member according to CP 110, the relative costs of using prestressing steel, high yield reinforcing steel or mild steel to provide the additional reinforcement required. Assume that unit rates for the three types of steel are available.

[12 marks]
2. Write brief notes (about half a page) on each of the following:-
 - (a) The main factors affecting creep in prestressed concrete listed in order of importance with respect to a typical structure such as a highway bridge.
 - (b) The reasons for avoiding either too small or too large a percentage of steel in a prestressed concrete member.
 - (c) Compare and contrast flexural cracking and shear cracking.
 - (d) Linear transformation of a cable profile.
 - (e) The mechanism of failure of a concrete beam in torsion, with comments on the effect of shear and bending moment in combination with torsion.

[25 marks]

/3.

3.



The rectangular, post-tensioned concrete beam shown above is simply supported at B, E, G and K. The beam carries eleven equally spaced columns supporting an upper floor. The sustained loads transmitted by these columns to the beam are as shown (viz. 75 kN at A and L; 150 kN at all the other points). In addition to its self-weight, the beam has to carry a sustained load of 20 kN/m throughout its length.

Use the load balancing method, balancing all sustained loads, to give a suitable preliminary design (i.e. beam size, cable profile and prestress force).

The design should comply with the following constraints:-

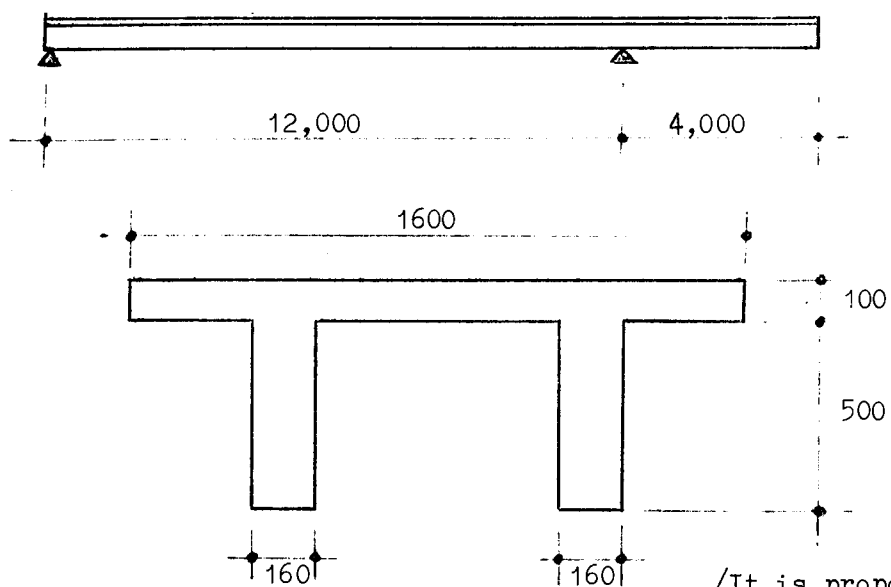
- (a) Minimum width of beam : 250 mm
- (b) Maximum depth of beam : 1200 mm
- (c) Minimum cover distance to centroid of tendons: 100 mm
- (d) Maximum average concrete stress : 6 MPa.

Assume furthermore that prestressing losses are negligible so that the prestressing force is constant throughout.

Assume Weight of Concrete = 25 kN/m^3

[20 marks]

4.



/It is proposed ...

4. (Continued)

It is proposed to build a prestressed concrete floor spanning 12 metres with an additional 4 metre cantilever. Pretensioned double-T units of the uniform cross-section shown above are to be used. These are to be designed according to CP 110 as Class 3 members, using the minimum prestressing force and providing additional untensioned reinforcement where necessary.

The floor is required to carry an imposed loading of 10 kN/m^2 over any part.

Prestressing is to be accomplished using straight horizontal tendons only.

Determine the following:-

- (a) The minimum prestressing force required and its eccentricity. (Consider only the support points and midspan, neglecting the slightly higher moments just to the left of midspan).
- (b) The area of additional untensioned reinforcement required at midspan using either prestressing wire or high yield reinforcing steel.

Comment on the merits and demerits of the resulting design.

Necessary data:

Use Concrete Grade 50 (i.e. $f_{cu} = 50 \text{ MPa}$)

Permissible compressive stress for serviceability limit state: $16,7 \text{ MPa}$
 Permissible hypothetical tensile stress for serviceability limit state (including depth factor): $5,8 \text{ MPa}$.

Weight of concrete = 25 kN/m^3

Minimum cover distance to centroid of prestressing tendons: 80 mm

Factors of Safety for Ultimate Limit State: Dead Load: $1,4$
 Imposed Load: $1,6$

Characteristic strength of prestressing wire: $f_{pu} = 1550 \text{ MPa}$

Residual prestress (after losses): $0,6 f_{pu}$

Characteristic strength of high yield steel: $f_y = 460 \text{ MPa}$

Cost of untensioned prestressing wire: $\text{R}700/\text{ton}$

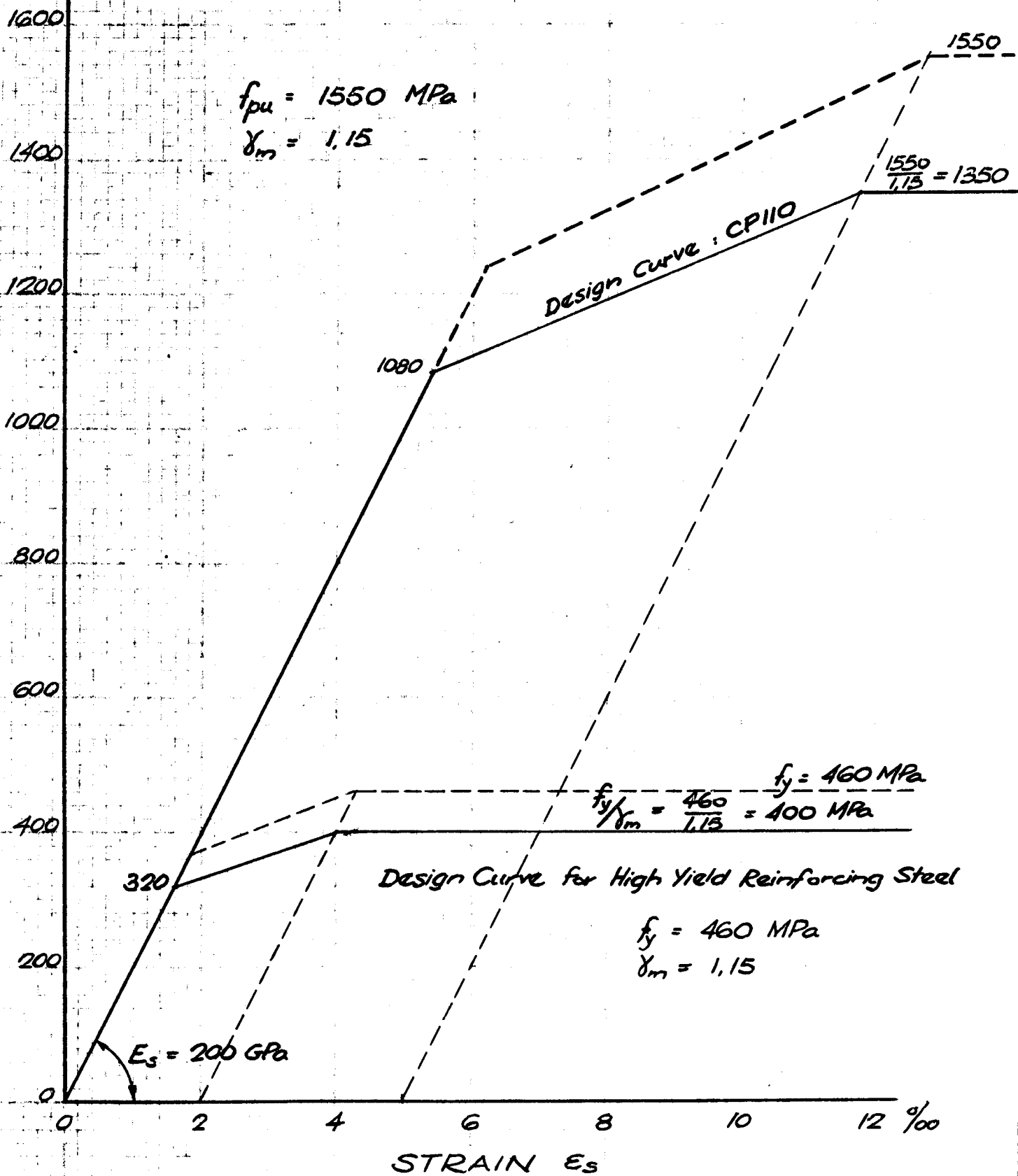
Cost of high yield reinforcing steel: $\text{R}350/\text{ton}$

Modulus of Elasticity for steel: 200 GPa

Design curves for prestressing wire and high yield steel are attached.

[40 marks]

STRESS σ_s IN MPa



UNIVERSITY OF CAPE TOWN

DEPARTMENT OF ACCOUNTING

JUNE 1975 EXAMINATION

INTRODUCTION TO MANAGEMENT ACCOUNTING

INVENTORY COSTING

In a 'perpetual inventory' system of accounting for inventory the debit balance on the 'finished goods inventory' account should represent the cost of inventory on hand. There are various methods of determining cost.

YOU ARE REQUIRED TO

Name and explain briefly an alternative to each of the methods given below.

1.0 With regard to the cost of goods manufactured (debits to the inventory account):

1.1 DIRECT COSTING

An alternative is

which means that :

1.2 'ACTUAL' COSTING

An alternative is

which means that :

1.3 JOB COSTING

An alternative is

which means that :

1.4 JOINT COSTS SPLIT ACCORDING TO SOME MEASURE OF SALES REVENUE

An alternative is

which means that :

2.0 With regard to the cost of goods sold (credits to the inventory account):

2.1 WEIGHTED AVERAGE COST

An alternative is

which means that :

ITMA 1975/FINAL/2

SCORE:



OUT OF 5 MARKS

INVENTORY VALUATION

In placing a valuation on inventory for the purpose of the annual financial statements one has to consider not only the cost of the inventory.

YOU ARE REQUIRED TO

1. State what basis of valuation other than cost might be appropriate.
2. State with which statute and/or convention one would be complying.

PROCESS COSTING

Accounting A and Accountant B have been asked to cost a month's production of the same process. Part of their respective calculations are given below.

YOU ARE REQUIRED TO

Answer the questions on the following page.
(You may assume that there are no arithmetical errors)

ACCOUNTANT A'S SCHEDULE

	<u>UNITS</u>
INPUTS	
a Beginning w i p ($\frac{1}{2}$ converted)	2 000
b Started	<u>18 000</u>
c	<u>20 000</u>
OUTPUTS	
d Completed	
- from beginning w i p	2 000
- started and finished	13 000
e Normal loss	1 500
f Ending w i p ($\frac{4}{5}$ converted)	<u>3 500</u>
g	<u>20 000</u>

<u>MATERIALS</u>	<u>CONVERSION</u>
COSTS	
R 1 800	R 4 325
<u>18 000</u>	<u>34 600</u>
<u>R19 800</u>	<u>R38 925</u>
EQUIVALENT UNITS	
-	1 000
13 000	13 000
1 500	500
<u>3 500</u>	<u>2 800</u>
<u>18 000</u>	<u>17 500</u>

ACCOUNTANTS B'S SCHEDULE

	<u>UNITS</u>
INPUTS	
a Beginning w i p ($\frac{1}{2}$ converted)	2 000
b Started	<u>18 000</u>
c	<u>20 000</u>
OUTPUTS	
d Completed	15 000
e Normal loss	1 500
f Ending w i p ($\frac{4}{5}$ converted)	<u>3 500</u>
g	<u>20 000</u>

<u>MATERIALS</u>	<u>CONVERSION</u>
COSTS	
R 1 800	R 4 325
<u>18 000</u>	<u>34 600</u>
<u>19 800</u>	<u>38 925</u>
EQUIVALENT UNITS	
15 000	15 000
1 500	500
<u>3 500</u>	<u>2 800</u>
<u>20 000</u>	<u>18 300</u>

Please refer to the previous page and answer the following questions:

1. Explain why they have arrived at different equivalent units.
Which is correct and why ? 2
2. Explain why they have both used the same costs. 2
3. Give a probable explanation for the computation of equivalent units in respect of normal loss. 2
4. Using Accountant A's schedule, show (as far as the information allows) for all ledger accounts involved, the balances and the entries required to record the month's production.

CAPITAL INVESTMENT APPRAISAL AND BREAK-EVEN

A small company manufactures a single product with one machine (Model A) which was purchased exactly two years ago for R40 000. The economic life of model A was (and is) estimated to be 10 years, after which it will have a scrap value of Rnil. Model A can be sold now for R12 000.

At present there is a fully automatic model B on offer for R50 000 delivered and installed. Model B has an estimated economic life of 8 years after which its estimated scrap value will be R3 000. Both machines qualify for an annual income tax depreciation allowance at the rate of 10% per annum on cost. Assume: that the company has a large taxable income; that the tax rate is 40%; that tax for any year is paid at the end of that year; that all cash flows occur at the end of the year.

The company's required earnings rate is 10% after tax. The present values of R1 at 10% are as follows:

Year 1	0,9
2	0,8
3	0,7
4	0,7
5	0,6
6	0,6
7	0,5
8	0,5
9	0,4
10	0,4

The following data apply to each machine respectively.

(All figures in thousands)

	<u>Model A</u>	<u>Model B</u>
Production and sales	30 units	30 units
Sales Revenue	<u>R210</u>	<u>R210</u>
Variable cost	<u>R135</u>	<u>R120</u>
Fixed costs excluding depreciation	<u>60</u>	<u>60</u>
	<u>195</u>	<u>180</u>
Net income before depreciation	<u>15</u>	<u>30</u>

YOU ARE REQUIRED TO

1. Advise whether model A should be replaced by Model B, giving reasons.
2. If model A were to be replaced by model B show how the break even units and revenue would be affected.

Please use the worksheet on the following page.

STANDARD COSTING

YOU ARE REQUIRED TO

Show all variances that can be determined from the following data :

(all figures in thousands)	Original Budget	Actual Performance
Production	240 units	270 units
Direct material usage	96 kg	100 kg
Direct labour usage	60 hrs	60 hrs
Sales	240 units	250 units
Sales revenue	<u>R1 200</u>	<u>R1 235</u>
Direct materials	R 480	R 543
Direct labour	120	132
Indirect variable	120	<u>135</u>
Total		810
Stock increase	—	<u>60</u>
Factory V.C. of sales	720	750
Selling variable	<u>60</u>	<u>65</u>
Total V.C. of Sales	<u>R780</u>	<u>R815</u>
Contribution	R420	R420
Fixed expense	<u>220</u>	<u>222</u>
Net income	<u>R200</u>	<u>R198</u>